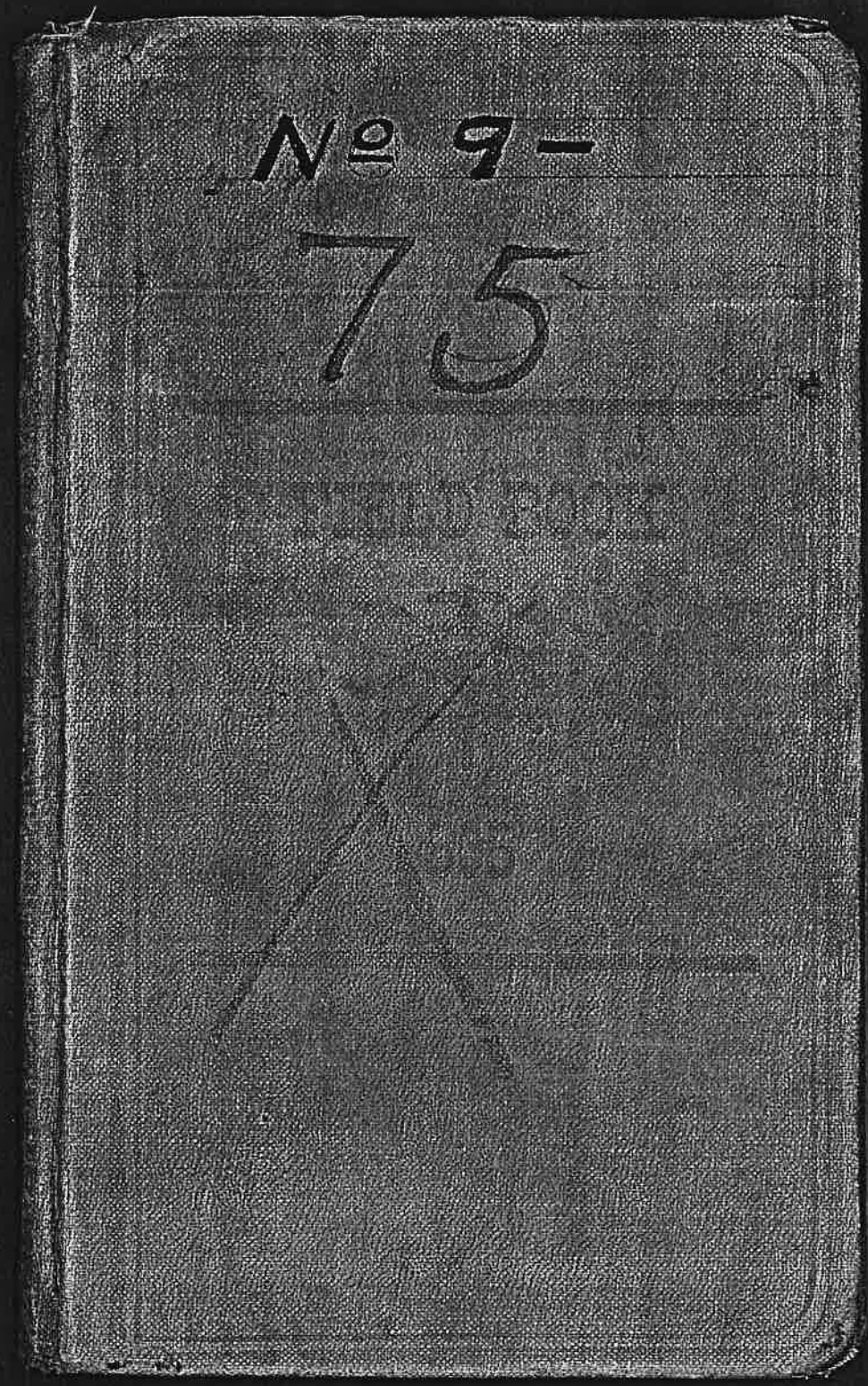
# Field Book #75


No 9-
75

1

S. on W. bdy of T23-8 R4W

26.30 Fir 24" dia

40.00 set qr post

A fir 18" b N85E 39 lks

B Oak 12 b S 37W 18"

71.50 Canon

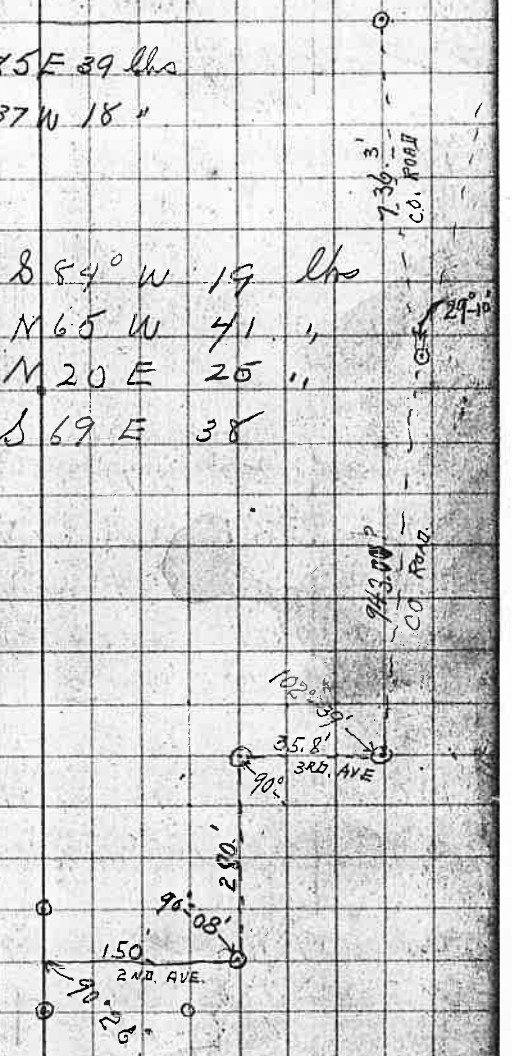
74.79 over Canon

80.00 " post A Redwood 8" S 54° W 15 lks

" Fir 12 N65W 41 "

" 12 N20E 26 "

" 12 S69E 38




LOCUST

Levels & Grades on 2nd Ave. Oakland, Or. June 14 1915

East Side

Burt Schell

Clyde Hennger

| Sta. | R.R. | Elev. | Grade | C. & F. |
|---|---|---|---|---|
| | 1.28 | 478.20 | | |
| | | | 476.92 | |
| 0+17½ | 6.35 | 471.85 | 471.20 | .65 |
| +40 | 3.28 | 474.92 | 472.70 | 2.22 |
| +20 | 2.06 | 476.14 | 475.20 | .94 |
| +35 | 1.46 | 476.74 | 476.61 | +.13 |
| 0+30 | 1.75 | 476.45 | | |

N. end of pavement Locust St inter. E Side
S prop line of Locust ST
N " " " Park "
Hub set 15' South of N Prop line of Park ST
E. prop Line of 2nd Ave

W. Side

| | | | | |
|---|---|---|---|---|
| 0+17½ | 6.58 | 471.62 | 471.12 | .5 |
| 0+17½ | 5.81 | 472.39 | 471.90 | .49 |
| 0+40 | 4.05 | 474.15 | 472.60 | 1.55 |
| 1+20 | 2.76 | 475.44 | 475.10 | .34 |
| 1+62½ | 2.00 | 476.20 | | |
| A | | 478.13 | | |
| B 0+30 | | 478.25 | 476.93 | 1.32 |

N. end of Concrete Curb R.C. N.
S " " " " R.C. S.
S prop line of Locust ST
N " " " Park
End of pavement S. in line with 1435 E. Side
Hub set S. 45' of N. Prop line of Park ST.
E. Prop line of 2nd Ave.

2 Oakland 2nd ave.

| STA. | ROD | H.I. | Center line ELE. | Cut to grade |
|---|---|---|---|---|
| 0. | | 479.97 | 471.57 | 471.15 |
| 0.+17.5 | | | 472.47 | 472.38 |
| 0.+35 | | | 473.37 | 472.83 |
| 0+51 | | | 474.87 | 473.27 |
| 1+01 | | | 475.57 | 474.61 |
| 1+51 | | | 476.77 | 475.95 |
| 1+67 | | | 477.17 | 477.40 |
| 1+84½ | | | 477.87 | 477.40 |
| | 10.88 | | | 7.01 |

BM 476.92 on Tee head on center line of Locust St.

Pt 17½ N. of ℄ of Locust ℄ of Locust

0+00
+17½
+35
0+51
+01
+37½
1+51
+67

0+15 on Park St
0+36

Park St

476.92 10.88 467.80 1.01 466.79

80 37½ 137½ 46862

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 15 8.1 | 11½ 8.2 | 7½ 8.2 | 0 8.40 | 7½ 8.6 | 11½ 8.8 | 14 8.3 | | |
| 15 6.9 | 11½ 6.9 | 7½ 7.1 | 7.5 | 7½ 7.8 | 11½ 7.8 | 15 7.9 | | |
| 15 6.3 | 11½ 6.4 | 7½ 6.6 | 6.6 | 7½ 7.2 | 14 7.6 | | | |
| 15 5.8 | 11½ 5.6 | 7½ 5.5 | 5.1 | 7½ 5.3 | 11½ 5.5 | 15 5.7 | | |
| 15 4.4 | 11½ 4.5 | 7½ 4.3 | 4.4 | 7½ 4.9 | 11½ 5.6 | 15 5.9 | | |
| 15 3.1 | 11½ 3.0 | 7½ 2.9 | 3.2 | 7½ 3.8 | 11½ 4.1 | 15 4.4 | | |
| 15 2.0 | 11½ 2.1 | 7½ 2.7 | 2.8 | 7½ 2.9 | 11½ 3.9 | 15 4.3 | | |
| 15 1.6 | 11½ 1.3 | 7½ 1.8 | 2.1 | 7½ 2.12 | 11½ 2.8 | 15 3.4 | | |

14 on curb
15 on pavement
477

E Lt
W Rt

2.3 479.2 476.9

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 13 7.0 | 12.5 7.5 | 7½ 7.6 | 0 7.2 | 7½ 7.5 | 14 7.2 | 14 7.5 | on ℄ | |
| 13 6.0 | 12.5 7.1 | 7½ 7.0 | 0.0 6.9 | 7½ 6.8 | 14 6.7 | | | |
| 13 5.0 | 12.5 6.5 | 7½ 6.1 | 0.0 5.9 | | 14 6.2 | 14 7.1 | 15 5.4 | 66 on ℄ |
| 13 4.8 | 12.5 5.6 | 7½ 5.6 | 0.0 5.7 | 7½ 6 | 11½ 6.5 | 12½ 4.7 | | |
| 13 3.5 | 12.5 4.5 | 7½ 4.8 | 0.0 4.9 | 7½ 5.4 | 11½ 5.5 | 12½ 4.8 | | |
| 13 3.2 | 12.5 4.1 | 7½ 4.3 | 0.0 4.3 | 7½ 4.3 | 11½ 5.2 | 12½ 4.0 | | |

4.3 481.2 476.9

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 15 4.2 | 14 5.0 | 10 5.0 | 0.0 5.1 | 5 5.1 | 10 5.1 | 11 5.8 | | |
| 3.3 | 13 4.3 | 0.0 4.3 | 7½ 4.1 | | | | | |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 16 4.7 | 15 5.0 | 11 5.0 | 0.0 5.1 | 4.1 | 8.0 5.1 | 12 5.2 | 15 | |
| 12 3.0 | 11½ 4.7 | 7½ 4.7 | 0.0 4.3 | 7½ 5.1 | 11½ 5.1 | 12½ 4.3 | | |

3 Park — Oakland St. bet. 2nd and 3rd Ave.

| | Rod | H.I. | Ele. curb line | Subgrade | B.M. 476.92 (Sand Lime 2nd Story, 1') | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| B.M. | 6.65 | 483.57 | | | | 17½ 6.8 | 11½ 6.4 | 7½ 5.9 | 5.6 | 7½ 5.6 | 11½ 5.6 | 17½ 5.4 |
| 0+00 | | | | | | | | | | | | |
| 0+15 | | | 478.0 | 479.80 | | 17½ 5.8 | 11½ 4.9 | 7½ 4.5 | 4.7 | 7½ 4.4 | 11½ 3.8 | 17½ 4.1 |
| 0+65 | | | 478.9 | 479.14 | | | | | | | | |
| 1+15 | | | 482.2 | 479.49 | | 17½ 3.5 | 11½ 2.4 | 7½ 2.1 | 1.4 | 7½ 1.3 | 11½ 1.2 | 17½ .7 |
| T.P. | 1.21 | | | | | | | | | | | |
| B.S. | 6.54 | 488.90 | | | | | | | | | | |
| 1+65 | | | 483.8 | 481.84 | | 17½ 7.7 | 11½ 7.2 | 7½ 6.3 | 5.1 | 7½ 4.9 | 11½ 4.9 | 17½ 5.6 |
| 2+15 | | | 483.7 | 482.19 | | 17½ 8.3 | 11½ 7.2 | 7½ 6.3 | 5.2 | 7½ 5.1 | 11½ 5.0 | 17½ 4.9 |
| 2+65 | | | 481.8 | 483.54 | | 17½ 9.5 | 11½ 9.1 | 7½ 8.7 | 7.1 | 7½ 5.3 | 11½ 4.6 | 17½ 4.6 |
| 2+80 | | | 480.8 | 483.95 | ℄ of 2nd Ave | 17½ 9.2 | 11½ 9.0 | 7½ 8.1 | 8.1 | 7½ 7.2 | 11½ 6.5 | 17½ 4.3 |
| 2+97½ | | | 481.4 | 483.95 | | 17½ 9.1 | 11½ 8.4 | 7½ 8.0 | 7.1 | 7½ 6.5 | 11½ 6.4 | 17½ 5.5 |
| | | 5th Ave. | | | | | | | | | | |
| 0.00 | | | | | | 17½ 5.2 | 11½ 5.4 | 7½ 5.0 | 4.7 | 7½ 4.4 | 11½ 4.4 | 17½ 4.6 |
| 0+17½ | | 488.95 | 484.5 | 484.41 | | | | | | 7½ 3.8 | 11½ 4.0 | 17½ 4.3 |
| 0+35.8 | | | 485.3 | 484.87 | | 17½ 3.3 | 11½ 3.3 | 7½ 3.4 | 3.6 | | | |
| 0+53.3 | | | 488.0 | 484.87 | | 17½ 1.8 | 11½ 1.3 | 7½ 1.0 | 0.9 | 7½ 0.6 | 11½ 0.1 | 17½ .00 |
| T.P. | 3.63 | | | | | | | | | | | |
| B.S. | 2.23 | 487.50 | | | | | | | | | | |

4 Oakland Co. Road

| | | H.I | Center line Elev | Finish grade | Left 17½ | Left 11½ | Left 7½ | Cut | Right 7½ | Right 11½ | Right 17½ |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0+00 | | | | | 3.1 | 2.3 | 2.1 | 1.7 | 1.4 | 1.2 | 0 |
| 0+17½ | | 487.50 | 485.8 | 485.08 | 2.1 | 1.6 | 1.5 | 1.4 | 0.8 | 0.7 | 3,— |
| 0+67½ | | | 486.1 | 484.78 | 1.2 | 1.4 | 1.4 | 1.3 | 1.0 | 1.3 | .8— |
| 1+17½ | | | 486.2 | 483.38 | 6.1 | 6.2 | 6.2 | 6.3 | 6.4 | 6.1 | 4.2 |
| 1+67½ | | | 481.2 | 481.74 | 12.2 | 11.6 | 9.4 | 9.4 | 9.2 | 9.6 | 5.5 |
| 2+17½ | | | 478.1 | 480.48 | 13.8 | 13.2 | 12.1 | 11.3 | 11.3 | 12.4 | 10.9 |
| 2+67½ | | | 476.2 | 480.02 | 12.6 | 12 | 10.6 | 10.4 | 12.6 | 13.0 | 10.9 |
| 3+17½ | | | 477.1 | 480.83 | 6.8 | 7.5 | 6.4 | 6.4 | 7.0 | 8.1 | 7.3 |
| 3+67½ | | | 481.1 | 482.31 | 2.2 | 2.2 | 0.9 | 0.8 | 0.6 | 1.2 | 0.0 |
| 4+17½ | | | 486.7 | 484.16 | | | | | | | |
| T.P. | 0.62 | | | | | | | | | | |
| B.S | 12.35 | 499.23 | | | | | | | | | |
| 4+67½ | | | 490.2 | 486.11 | 7.6 | 10.1 | 9.4 | 9.0 | 9.6 | 10.8 | 11.2 |
| 5+17½ | | | 491.6 | 487.97 | 6.7 | 9.3 | 7.5 | 7.6 | 9.3 | 10.0 | 11.1 |
| 5+67½ | | | 493.0 | 489.83 | 5.3 | 6.7 | 6.0 | 6.2 | 8.0 | 8.7 | 10.1 |
| 6+17½ | | | 496.0 | 491.68 | 7.4 | 6.8 | 6.0 | 3.2 | 3.1 | 3.4 | 2.0 |
| 6+67½ | | | 496.9 | 493.54 | 6.3 | 6.3 | 5.0 | 2.3 | 2.2 | 2.1 | 2.4 |
| 7+17½ | | | 496.9 | 495.40 | 6.8 | 6.3 | 5.8 | 2.3 | 2.4 | 2.2 | 0.7 |
| 7+67½ | | | 495.7 | 497.26 | 7.2 | 6.0 | 5.4 | 3.5 | 3.4 | 4.4 | 5.3 |
| 8+17½ | | | 497.2 | 499.12 | 3.6 | 3.2 | 2.7 | 2.0 | 2.1 | 3.9 | 4.0 |
| T.P. | 0.00 | | | | | | | | | | |
| B.S | 9.85 | 509.08 | | | | | | | | | |
| 8+67½ | | | 501.8 | 500.98 | 5.1 | 4.8 | 6.9 | 7.3 | 7.3 | 7.9 | 7.0 |
| 9+17½ | | | 506.7 | 502.84 | 0.8 | 1.7 | 2.0 | 2.4 | 2.4 | 1.6 | 2.0 |
| 9+43 | | | 508.0 | 503.54 | 1.— | 11 | 1.8 | 1.6 | 1.6 | 1.7 | 0.6 |

5

| | | H.I. | Elevation | Subgrade | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | 16 | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 0+50 | | 509.08 | 504.7 | 500.70 | | 3.2 | 5.6 | 5.5 | 4.4 | 3.8 | 4.3 | 3.2 |
| | | | | | | 17 | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 1+00 | | | 500.5 | 497.84 | | 9.4 | 10.6 | 10.0 | 8.6 | 8.6 | 9.2 | 9.2 |
| T.P. | 12.93 | | | | | | | | | | | |
| B.S. | 0.26 | 496.41 | | | | | | | | | | |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 1.50 | | | 495.9 | 494.99 | | 2.0 | 1.6 | 1.0 | 0.5 | 0.5 | 1.3 | 1.7 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 2+00 | | | 491.4 | 492.12 | | 6.0 | 7.3 | 6.3 | 5.0 | 5.0 | 6.3 | 6.2 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 2+50 | | | 488.9 | 489.58 | | 9.6 | 10.3 | 8.9 | 7.5 | 7.9 | 9.6 | 10.0 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 3+00 | | | 487.0 | 487.78 | | 10.7 | 11.9 | 10.6 | 9.4 | 9.7 | 11.0 | 11.8 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 3+50 | | | 485.7 | 486.58 | 3+60 crack | 11.9 | 12.7 | 10.8 | 10.7 | 10.7 | 11.8 | 12.3 |
| T.P. | 10.70 | | | | | | | | | | | |
| B.S. | 4.68 | 490.39 | | | | | | | | | | |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 4+00 | | | 485.7 | 486.02 | | 5.4 | 6.2 | 5.4 | 4.7 | 4.7 | 5.0 | 5.6 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 4+50 | | | 485.6 | 486.38 | | 5.5 | 6.3 | 5.6 | 4.8 | 4.9 | 5.4 | 5.7 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 5+00 | | | 485.4 | 486.91 | | 6.3 | 6.0 | 5.8 | 5.0 | 5.8 | 5.5 | 5.7 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 5+50 | | | 485.9 | 487.66 | | 5.9 | 6.6 | 5.3 | 4.5 | 4.7 | 5.1 | 5.2 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 6+00 | | | 487.5 | 488.41 | | 3.5 | 4.1 | 3.5 | 2.9 | 3.1 | 4.1 | 3.2 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 6+50 | | | 488.1 | 489.16 | | 3.1 | 3.1 | 3.1 | 2.3 | 2.9 | 3.0 | 2.5 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 7+00 | | | 488.4 | 489.91 | | 2.7 | 2.5 | 2.5 | 2.0 | 2.6 | 2.9 | 2.5 |
| | | | | | | 17½ | 11½ | 7½ | | 7½ | 11½ | 17½ |
| 7+36.3 | | | 489.3 | 490.38 | | 1.3 | 1.5 | 1.4 | 1.1 | 1.7 | 1.7 | 1.2 |
| | 1.05 | | 489.84 | Nail in Power pole | | | | | | | | |

1952.86

Second Ave

| | | | |
|---|---|---|---|
| 388.1 | sq yds @ | 1.12 | 434.67 |
| 320.0 | lin ft of St Curb (wood) @ | .06 | 19.20 |
| 31.4 | " " " Curb " @ | .10 | 3.14 |
| 126.8 | Cu yd excavation @ | .55 | 69.74 |
| 6.0 | " " fill @ | .20 | 1.20 |
| 1 | wood culvert @ | 5.00 | 5.00 |
| | Total | | 532.95 |

| | | | |
|---|---|---|---|
| 492.0 | sq yds of pavement @ 1.12 | | 551.04 |
| 590.0 | lin ft of St wood curb @ 0.6 | | 35.40 |
| 244.1 | Cu yds of cut | @ .50 | 122.05 |
| 108.1 | Cu yds of fill | @ .20 | 21.62 |
| | | | 730.11 |

7

Third Ave. Survey

Oakland Ore.

559
46
3357
3805
3689 4

N 1/8 E 5

N. 01. 5 E 5

180'

60'

200'

Third Ave

S 27 1/4 E

60'

90° 14'

60'

8

X. Sect. Notes on Third Ave. Oakland Orc.

12.62 493.41 480.79

| | Lt E | | | Rt W | |
|---|---|---|---|---|---|
| 0+00 | 30 11 3 | 12 12 1 | 00 12.62 | 12 11 8 | 30 11 5 |
| | 482.1 | 481.3 | 480.4 | 481.6 | 481.9 |
| +12 | 12 9 7 | 12 11 0 | 00 10 7 | 12 9 5 | 30 9 3 |
| | 483.7 | 482.4 | 482.7 | 483.9 | 484.1 |
| +30 | 30 7 9 | 12 8 5 | 00 8 4 | 12 8 4 | 30 8 9 |
| | 485.5 | 484.9 | 485.0 | 484.6 | 484.5 |
| +60 | 30 4 1 | 12 5 4 | 00 5 3 | 12 4 0 | 30 4 0 |
| | 489.3 | 488.0 | 488.1 | 489.4 | 489.4 |
| +90 | 30 (-0 2) | 12 6 5 | 00 1 3 | 12 0 8 | 30 0 2 |
| | 493.6 | 492.9 | 492.1 | 492.6 | 492.7 |
| T.P. | 11.72 | 504.53 | | 0.60 | 492.81 |
| 1+20 | 30 8 3 | 12 8 4 | 00 8 9 | 12 8 8 | 30 8 9 |
| | 496.2 | 496.1 | 495.6 | 495.7 | 495.6 |
| +50 | 30 6 4 | 12 6 4 | 00 5 2 | 12 5 4 | 30 5 5 |
| | 498.1 | 498.1 | 498.8 | 499.1 | 499.0 |
| +90 | 30 0 7 | 12 1 5 | 00 1 6 | 12 1 3 | 30 1 6 |
| | 503.8 | 503.0 | 502.7 | 503.2 | 502.9 |
| T.P. | 12.78 | 516.97 | | 0.34 | 504.19 |
| 2+30 | 30 9 4 | 12 10 6 | 00 10 4 | 12 10 2 | 30 10 0 |
| | 507.6 | 506.5 | 506.6 | 506.8 | 507.0 |

8.12 on hub
485.29

517

9

517

# Third Ave (Cont)

516.97

| | | Lt E | | | Rt W | | |
|---|---|---|---|---|---|---|---|
| 2+70 | | 30 / 5.5 | 12 / 5.5 | 00 / 6.4 | 12 / 6.5 | 30 / 7.4 | |
| | | 511.5 | 511.5 | 510.6 | 510.5 | 509.6 | |
| 3+10 | | 30 / 2.3 | 12 / 2.7 | 00 / 3.5 | 12 / 4.1 | 30 / 6.4 | |
| | | 514.7 | 514.3 | 513.5 | 512.9 | 510.6 | |
| +50 | | 30 / 6.0 | 12 / 1.5 | 00 / 3.1 | 12 / 4.1 | 30 / 6.9 | |
| | | 517.0 | 515.5 | 513.3 | 512.3 | 510.1 | |
| +80 | | 30 / (1.9) | 12 / 2.2 | 00 / 3.8 | 12 / 5.2 | 30 / 7.0 | |
| | | 518.4 | 514.8 | 513.2 | 511.8 | 510.0 | |
| 4+10 | | 30 / (1.4) | 12 / 2.2 | 00 / 3.2 | 12 / 4.8 | 30 / 5.8 | |
| | | 518.7 | 514.8 | 513.3 | 512.2 | 511.2 | |
| +35 | | 30 / (0.9) | 12 / 2.4 | 00 / 3.3 | 12 / 4.4 | 30 / 4.3 | |
| | | 517.9 | 514.6 | 513.7 | 512.6 | 512.7 | |
| +60 | | 30 / 0.0 | 12 / 1.7 | 00 / 1.6 | 12 / 2.2 | 30 / 1.3 | |
| | | 517.0 | 515.3 | 515.4 | 514.8 | 515.7 | |

16.0

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| B.M. | 10.63 | 487.57 | | | 476.92 | | |
| T.P. | | | | 6.88 | 480.69 | | |
| T.P | 11.61 | 498.42 | | 0.76 | 486.84 | | |
| 6+30 | 11.69 | 509.69 | 0.50 | 0.50 | 497.92 | 497.93 | S. Prop Line of Maple St. |
| 0+60 | | | 7.29 | | 502.32 | 500.62 | 1.70 |
| +90 | | | 4.27 | | 505.34 | 503.31 | |
| 1+10 | | | 2.30 | | 507.31 | 505.11 | |
| +30 | | | 0.30 | | 509.31 | 506.86 | 2.45 |
| | | | | 0.27 | 509.34 | | |

10

Nov 17 1914

## Grade Notes on Spring St.

### Original Notes

| | Lt. | Cen. | Rt. |
|---|---|---|---|
| 0+23 66 | | | |
| 0+36 47 | out +13 3 | 655 8 | out −12 4 |
| 0+50 | +12 3 | 657 6 | −14 0 |
| 0+57 | +12 0 | 658 5 | −16 0 |
| 0+64 5 | −12 5 | 659 6 | −22 3 |
| +78 | +12 5 | 661 4 | −23 5 |
| +91 | −18 4 | 663 1 | −17 0 |
| 1+00 | −23 1 | 664 3 | −15 0 |
| −14 | −18 0 | 666 2 | −12 3 |
| +26 | +12 5 | 667 8 | +12 4 |
| +50 | +14 4 | 671.00 | +14 0 |
| +75 | +14 4 | 674.5 | +13 0 |

### Recheck X Section Notes

9.85 — 663.65 — H.B.M. 653.80

12.65 — 651.00

Lt East — Rt. West

656.25 — 656.62 — 655.35 — 654.65

12/7.4 — 10/8.03 — 10/8.3 — 12/9.0 T.

657.25 — 657.47 — 657.45 — 656.45 — 655.95

12/6.4 — 00/6.18 — 10/6.2 — 14/7.1 — 15°/8.2

658.25 — 658.46 — 658.35 — 657.85 — 654.95

12/5.4 — 00/5.19 — 10/5.3 — 12/5.8 — 15/8.7

658.95 — 659.38 — 659.45 — 658.45 — 657.95 — 651.85

12/4.7 — 00/4.27 — 4/4.2 — 11/5.2 — 12/5.7 — 23/11.8

660.76 — 660.88 — 660.45 — 659.45 — 654.45

12/2.81 — 00/2.7 — 9/3.2 — 12/4.0 — 22/7.2

659.66 — 660.85 — 662.05 — 662.57 — 662.25 — 660.55

23/13.6 — 16/2.8 — 12/1.6 — 1.08 — 12/1.4 — 15/3.1

T.P. 9.79 — 673.26 — 663.90 — 663.56 — 0.18 — 663.47

24/17° — 24/13° — 12/9.36 — 9/9.7 — 15°/9.8 — 669.46

25/12.2 — 20/9.2 — 12/8.4 — 12/7.2 — 665.6 — 00/7.23 — 666.03 — 12/7.7 — 665.56

12/6.0 — 669.26 — 12/6.4 — 667.16 — 14/6.1 — 667.16

12/2.2 — 670.56 — 12/2.7 — 670.56 — 00/2.6 — 670.96 — 12/2.8 — 670.76 — 13/1.2 — 672.06

T.P. 12.94 — 686.07 — 673.87 — 0.13 — 673.73

17/11.67 — 12/12.2 — 00/11.88 — 12/12.4 — 673.69 — 15/12.2 — 673.87

11

## Grade Notes (Cont'd.)

| | | Lt | Cen | Rt |
|---|---|---|---|---|
| 2 | | | | |
| 2 + 00 | | +12 | 678.00 | -14 |
| + 25 | | -14 | 681.50 | -16 |
| 2 + 50 | 1490 | -13 | 685.00 | -21 |
| + 65 | | -14 | 687.10 | -23 |
| 2 + 75 | ◎ | | 688.50 | -17 |
| + 88.81 | Δ = 10°10½' D.C. 4°30' Rt | | 690.47 | |
| 3 + 00 | | | 692.06 | |
| 3 + 13.81 | | | 694.03 | |
| 3 + 38.81 | | | 697.59 | |
| 3 + 63.81 | 1424 ℄ | | 701.15 | |
| + 88.81 | | | 704.71 | |
| 4 + 13.81 | | | 708.27 | |

## Recheck X. Sect. Cont.

Lt. East — Rt. West

686.67 — 697.94 — 709.78

12

Grade Notes (Cont)

| | | |
|---|---|---|
| 4+38 86 | | 718.83 |
| +63 86 | ⓒ | 715.40 |
| +88 86 | | 719.06 |
| 5+14 97 | E.C. 4°30' R | 722.89 |
| +41 97 | | 726.84 |
| +50 | | 728.02 |
| +75 | | 731.68 |
| 6+00 | 14.65 | 735.34 |
| +25 | | 739.01 |
| +34 54 | Δ = 8°50' BC 4°20' Lt | |
| +50 | | 742.67 |
| +75 | | 746.33 |
| 7+00 | | 750.00 |
| +25 | | 753.90 |

Rocker X. Sect.

L

716.45 718.45 722.45 711.95 711.86 711.35 710.95 710.35 708.16

718.05 715.15 715.43 714.95 714.25 711.95

719.46 718.85 719.21 718.55 718.45 714.25

12.09 723.28 734.38 723.18 722.68 721.98 722.29

same slope 728.88 726.76 726.87 726.55 726.38 723.28

S slope 729.98 728.08 728.01 727.58 727.25 725.28

same slope 733.38 731.58 731.92 731.38

12.038 736.45 735.05 746.10 735.87 735.25 734.12

S slope 739.85 738.25 737.95 736.79

S slope 743.45 740.05 739.25 739.36 738.85 740.25 738.95

S slope 746.66 741.55 744.52 744.63 740.85 742.05 740.05

S slope 748.47 743.15 743.38 744.84 742.35 743.55 741.95

11.67 757.39 745.72

S slope 750.09 746.89 746.49 746.39 746.59 745.08

750.27 750.59 750.03 750.56 750.39 749.09

753.99 754.50 754.09 753.39 752.29 75+67

754.59 754.39 753.49

2.89

13

## Grade Notes Cont

| | | |
|---|---|---|
| 7+50 | | 757.80 |
| +75 | | 761.70 |
| +88 | 15+13.50 | 762.57 |
| 8+00 | | 765.61 |
| +13 | | 767.64 |
| +25 | | 769.52 |
| +44.79 | ⊙ E.C. 4°20' L | 772.60 |
| +61.5 | | 775.55 |
| +70 | | 777.04 |
| 8+3 | | |
| +95 | 17+50.00 | 781.41 |
| 01 | | |
| 9+20 | | 785.79 |
| +25 | | |
| +45 | | 790.1-6 |
| 9+37 | | |
| +58.99 | ⊙ | 792.60 |

## Reckoning X sect (cont'd)

Lt / Rt

T.P 9.27 766.45 0.21

T 7.85 7.58.07 759.35 749.05

T 7.58.70 764.35 761.95 762.45 761.95 761.75 757.18

T 759.95 763.65 764.15 4.30 764.95 763.95 751.95 748.06

T 759.35 765.05 765.85 2.10 766.07 765.85 765.05 752.35

T 764.13 766.73 0.38 766.07 766.83 766.63 755.95

10.86 764.13 766.73 786.93 766.83 0.38 766.63 756.63

768.33 767.63 8.95 767.98 766.07

768.72 769.93 6.94 769.99 769.03 768.33

768.03 772.13 772.83 3.02 772.43

768.03 775.63 775.63 776.13 776.49

772.6 776.1 777.39 776.1 776.49

T.P 12.94 789.75 0.12 776.81

tie & soil fill

Bench 50.0

Butter

Bench

throat 9.35 798.89 -0.1 789.54

14

Gr. Notes Cont.

9 + 70

+ 95

10 + 20

+ 45 BC

+ 70

+ 95

11 + 20

+ 45

+ 70

+ 95

12 + 20

+ 45

+ 70

+ 84.66

Δ = 31° 03'

BC 13° 00 Lt

EC 13° Lt

794.74

799.59

804.45

809.46

814.15

819.00

824.14

829.28

834.42

839.56

844.70

849.84

854.98

LT Recheck X sec RT

798.85

811.39

0.42 798.47

823.92

0.16 811.23

834.46

0.23 823.69

849.02

0.20 838.26

T.P. 13.02 861.79

6.25 848.77

15

| | Grade | Notes |
|---|---|---|
| 12 + 95 | 0 | 860.12 |
| 13 + 20 | | 865.26 |
| + 45 | | 870.40 |
| + 70 | | 875.54 |
| + 95 | | 884.68 |
| 14 + 20 | | 885.82 |
| + 45 | | 890.96 |
| + 70 | | 896.10 |
| + 95 | | 901.24 |
| 15 + 20 | 10 + 95 = 819. | 906.40 |
| | 15 + 20 = 906.4 | 908.04 |

Earnest Lawrence 87.4 6 hrs
Mark Simpson 14 hrs
Bill Whipple 12 "
Gordon Burnett 4 "

10 + 95 = 819.0
15 + 20 = 906.40
89.03

906.4
860.12
46.28
225
456
280
1225
175

20.56
819
874
820
2409
2112

16-20
10.95
4.25
2750

20.80

20.56
1520
10.95
4.25

1520
1295
225

906.40
860.12
46.28
225

1520
1295
225

20.56
16.48
22.5
20.56

908.3

20.56

LH RH

Reached X 861.79 Sect Notes

12,49 874.16 0.12 861.67

T.P. 1300 886.92 24 873.92

T.P. 1255 899.28 0.19 886.73

T.P. 1201 911.10 10.19 899.09

10.73 921.52 .031 910.79

0.99 920.53

433

20.56

903
866
37
2160
2119

90803
81900
8903

1528
10.95
4.33

16

## Check Levels on Spring St Resurvey — Nov 17 1914

| | | | | | |
|---|---|---|---|---|---|
| | 0.99 | 921.69 | | | 920.70 |
| | 0.21 | 909.22 | | 12.68 | 909.01 |
| 15+20 | | | 1.47 | | 907.75 |
| +95 | | | 6.25 | | 902.97 |
| +70 | | | 11.45 | | 897.77 |
| T.P. | 00.26 | 896.59 | | 12.89 | 896.33 |
| +45 | | | 4.03 | | 892.56 |
| +20 | | | 9.33 | | 887.26 |
| T.P. | 00.32 | 884.48 | | 12.43 | 884.16 |
| 13+95 | | | 2.24 | | 882.24 |
| +70 | | | 7.48 | | 877.40 |
| 13+45 | | | 12.65 | | 871.83 |
| T.P. | 00.14 | 871.97 | | 12.65 | 871.83 |
| +20 | | | 4.93 | | 867.04 |
| 12+95 | | | 10.08 | | 861.89 |
| + | | | 12.07 | | 869.90 |
| T.P. | 0.25 | 869.22 | | 13.00 | 858.97 |
| +70 | | | 2.58 | | 856.64 |
| +45 | | | 8.04 | | 851.18 |
| 12+20 | | | 13.05 | | 846.17 |
| T.P. | 00.21 | 846.38 | | 12.05 | 846.17 |
| +95 | | | 5.54 | | 840.84 |
| +70 | | | 10.89 | | 835.49 |
| T.P. | 00.31 | 834.27 | | 12.42 | 833.96 |

Germond — Level
Whipple — Rod

17

| | | | | | |
|---|---|---|---|---|---|
| | | 834.27 | | | |
| 11.45 | | | 3.78 | | 830 49 |
| +20 | | | 9.00 | | 825 27 |
| F.P | 0.37 | 822.05 | | 12 54 | 821.68 |
| 10+95 | | | 2.03 | | 820.02 |
| +70 | | | 6 97 | | 815.08 |
| 10+45.82 | | | 11.64 | | 810.41 |
| T.P. | 00.20 | 809.49 | | 12.76 | 809.29 |
| +20 | | | 3.69 | | 805.80 |
| 9+95 | | | 8.84 | | 800 65 |
| T.P | 00.26 | 796.94 | | 12.81 | 796.68 |
| +55.99 | | | 2 93 | | 794 01 |
| +45 | | | 5.47 | | 791.47 |
| +20 | | | 10.20 | | 786 74 |
| T.P | 00.28 | 784.47 | | 12.75 | 784 19 |
| 8+95 | | | 2.46 | | 782.01 |
| +70 | | | 6.87 | | 777.60 |
| +44.75 | | | 11.21 | | 773.26 |
| TP | 00 22 | 772.00 | | 12.69 | 771.78 |
| 8+25 | | | 1.50 | | 770 20 |
| +00 | | | 5.72 | | 766 28 |
| +75 | | | 9.65 | | 762 35 |
| T.P. | 0.40 | 759.36 | | 13.04 | 758 96 |
| +50 | | | 1.08 | | 758 28 |
| +25 | | | 4.69 | | 754.67 |
| 7+00 | | | 8.61 | | 750 75 |

18

| | | | | | |
|---|---|---|---|---|---|
| | | 759 36 | | | |
| 6 | | | | | |
| 6 + 75 | | | 12.67 | | 746.69 |
| T.P. | 0039 | 747 08 | | 12.67 | 746.69 |
| +50 | | | 4.05 | | 743.03 |
| BC | | | 5 26 | | 741.82 |
| +25 | | | 7 52 | | 739 56 |
| 6 + 00 | | | 11.07 | 736.01 | 736.01 |
| T.P. | 00.36 | 734 42 | | 13.02 | 734.06 |
| +75 | | | 2.31 | | 732.11 |
| +50 | | | 6.23 | | 728.19 |
| +40 97 | | | 7.37 | | 727.05 |
| EC 5#14 97 | | | 11.05 | | 723.37 |
| T.P | 0.52 | 721.98 | | 12.96 | 721.46 |
| 4 + 88 86 | | | 2.58 | | 719.40 |
| +63 86 | | | 6.36 | | 715.62 |
| +38 86 | | | 9.94 | | 712.04 |
| T.P. | 0.22 | 704 47 | | 12.73 | 709.25 |
| +13 86 | | | 1.00 | | 708 47 |
| 3 + 88 86 | | | 4.48 | | 704 99 |
| +63 86 | | | 7.78 | | 701.69 |
| +36 86 | | | 11.34 | | 698 13 |
| T.P | 00.22 | 796 77 | | 12.92 | 796.55 |
| 3 + 13 86 | | | 2.34 | | 794 43 |
| 3 + 00 | | | 4 50 | | 792.27 |
| + 88 86 | | | 6.07 | | 790.76 |

19

| | | | | | |
|---|---|---|---|---|---|
| | | 796.77 | | | |
| 2+75 | | | 8.13 | | 786.64 |
| +65 | | | 9.80 | | 786.97 |
| 2+50 | | | 11.85 | | 784.92 |
| T.P. | 0.28 | 784.23 | | 12.82 | 783.95 |
| +25 | | | 2.71 | | 781.52 |
| 2+04 | | | 6.24 | | 777.99 |
| +75 | | | 9.86 | | 774.37 |
| +50 | | | 13.03 | | 771.20 |
| T.P. | 0.23 | 771.43 | | 13.03 | 771.20 |
| +25 | | | 3.65 | | 767.78 |
| 1+14 | | | 5.22 | | 766.21 |
| 1+00 | | | 7.35 | | 764.08 |
| 0+91 | | | 8.68 | | 762.75 |
| +78 | | | 10.37 | | 761.06 |
| +64.5 | | | 11.87 | | 759.56 |
| +57 | | | 12.78 | | 758.65 |
| T.P. | 2.45 | 761.10 | | 12.75 | 758.65 |
| +50 | | | 3.41 | | 757.69 |
| | | | 5.26 | | 755.82 |
| | | | 7.10 | | 754.00 |

Hicks B.M. Marked 753.80

Original Est = 2775.7 = Exc

Final " = 2375.6 = "

Borrow " 795.9 = "

Rock " 88.9 = 3260.4 = Total

Levels on Preliminary Survey: Yoncalla Water Supply – Adam's Creek Project

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| B.M. | 0.87 | 386.98 | | | 386.11 | B.M. | Nov. 19, 1914 |
| T.P | 2.58 | 383.34 | 6.22 | | 380.76 | stake | |
| T.P. | 1.32 | 379.99 | 4.67 | | 378.67 | Rock | Clear + Cold |
| T.P | 2.65 | 375.69 | 6.95 | Error of 0.01 | 373.04 | Stump | |
| T.P | 2.31 | 375.97 | 2.03 | | 373.66 | Secondary B.M. on Rot. Stump 300' E of Brd. X Road Cr. | |
| T.P | 5.46 | 377.81 | 3.62 | | 372.35 | Peg | |
| T.P' | 6.46 | 382.40 | 1.87 | | 375.94 | | M.B. Germond – Inst |
| T.P. | 11.81 | 393.69 | 0.52 | | 381.88 | | Jim Hanna – Rodman |
| T.P | 2.76 | 395.56 | 0.89 | | 392.80 | | Gurley's small Transit |
| T.P | 5.23 | 394.01 | 6.78 | | 388.78 | | |
| T.P | 5.53 | 398.57 | 0.97 | | 393.04 | | |
| T.P. | 7.70 | 403.59 | 2.68 | | 395.89 | | |
| T.P | 6.62 | 408.01 | 2.20 | | 401.39 | | |
| T.P | 6.20 | 411.83 | 2.38 | | 405.63 | | |
| B.M. N° 2 | | | 6.88 | | 404.95 | B.M N° 2 on hub on line but Shelly + Finley, S side of Cr | |
| T.P | 8.45 | 417.77 | 2.51 | | 409.32 | | |
| T.P. | 10.06 | 427.23 | 0.60 | | 417.17 | | Foot of hill |
| T.P. | 11.31 | 437.72 | 0.82 | | 426.41 | | |
| T.P. | 12.83 | 449.75 | 0.80 | | 436.92 | | |
| T.P. | 12.80 | 461.68 | 0.88 | | 448.88 | | |
| TP | 12.41 | 473.29 | 0.80 | | 460.88 | | |
| T.P | 12.39 | 484.63 | 1.05 | | 472.24 | | |
| T.P. | 13.00 | 496.63 | 1.00 | | 483.63 | B M N° 3 | |
| T.P | 12.87 | 508.77 | 0.73 | | 495.90 | | |
| | 173.62 | | 57.85 | | | | |

21

## Levels — Continued —

| | | | | | |
|---|---|---|---|---|---|
| | | 508 77 | 13 9 | | |
| T.P. | 12 87 | 521.04 | 060 | 508.17 | Nov. 19 1914 |
| T.P | 12.71 | 532.98 | 0 77 | 520 27 | |
| T.P | 1258 | 544.68 | 0.88 | 532.10 | |
| T.P, | 1283 | 556.84 | 0.67 | 544 01 | |
| T.P, | 1248 | 568 58 | 0 71 | 556,13 | |
| T.P, | 12.83 | 580,70 | 070 | 567.87 | |
| TP | 12.84 | 592.80 | 0 74 | 579.96 | |
| T.P, | 12.71 | 604.74 | 0 77 | 592.03 | |
| T.P. | 12.75 | 616.76 | 0 73 | 604.01 | |
| T.P. | 12.32 | 628.40 | 0.68 | 616.08 | |
| T.P. | 12 78 | 640.75 | 0 43 | 627.97 | |
| T.P | 10 75 | 650.92 | 0,58 | 640.17 | 646 00 Top of 1st Knob |
| T P | 6.63 | 656 57 | 0.98 | 649.94 | |
| B.M N°4 | | | 35.1 | 653.06 | Hub (marked) Top of 2nd Knob |
| T.P, | 12.10 | 667.70 | 0.97 | 655.60 | |
| B.M. N° 5 | 5.68 | 673.80 | 0.58 | 667.12 | Hub " " " 3rd " Extreme Height = 671 00 |
| T.P, | 12.09 | 684.28 | 0.61 | 672.19 | |
| T.P, | 1270 | 696,71 | 0.27 | 684.01 | |
| B.M. #6 | 1.15 | 697.43 | 0.43 | 696.28 | " " " " 4 " " " |
| T.P | 0.93 | 685.42 | 12.94 | 684.49 | 697.6 in level with lower limbs of tree. |
| | | | 12.32 | 673.10 | |
| | 201.69 | | 4087 | | |

201.69
3731
16433
508 77
673.10

201.69
3796
16873
16313

4046
4086
3736

## Levels — continued

| | | | | | | |
|---|---|---|---|---|---|---|
| | | | | | | |
| B.M. #7 | 1.23 | 674.33 | | | 673.10 | 8' N.E. of small Oak tree 2" dia on hill side in front of Davis's |
| T.P. | 1.34 | 663.38 | 12.29 | | 662.04 | |
| T.P. | 0.74 | 651.73 | 12.41 | Error .02 | 650.99 | |
| T.P. | 0.98 | 640.30 | 12.41 | | 639.32 | Nov. 20 1914 Clear & Cold nights |
| T.P. | 0.49 | 628.16 | 12.63 | | 627.67 | |
| T.P. | 0.44 | 615.66 | 12.94 | | 615.22 | Jim Hanna - Rodman |
| T.P. | 0.55 | 603.68 | 12.53 | | 603.13 | M. B. Germond - Inst. |
| T.P. | 0.67 | 592.01 | 12.34 | | 591.34 | Gurley's small Transit |
| T.P. | 0.53 | 579.99 | 12.55 | | 579.46 | |
| BM #8 | | | | 4.85 | 575.14 | B.M. on fence post 550' N.E. of Rock Bin on West side of Road |
| T.P. | 12.23 | 591.86 | 0.36 | | 579.63 | |
| T.P. | 12.39 | 603.13 | 1.12 | | 590.74 | |
| T.P. | 12.48 | 614.95 | 0.66 | | 602.47 | |
| T.P. | 12.78 | 626.74 | 0.99 | | 613.96 | T.P. on stump of small oak tree nailed |
| T.P. | 12.98 | 639.43 | 0.29 | | 626.45 | |
| T.P. | 12.68 | 651.43 | 0.68 | | 638.75 | |
| T.P. | 12.72 | 663.85 | 0.30 | | 651.13 | |
| T.P. | 12.88 | 676.10 | 0.61 | | 663.23 | |
| T.P. | 12.39 | 688.18 | 0.31 | | 675.79 | |
| " | 12.44 | 699.97 | 0.65 | | 687.53 | |
| " | 12.81 | 712.21 | 0.57 | | 699.40 | |
| " | 12.79 | 724.70 | 0.30 | | 711.91 | |
| " | 12.77 | 736.97 | 0.50 | | 724.20 | |
| B.M. #9 | 6.91 | 742.05 | 1.83 | 1.83 | 735.14 | At head of small gulch Turpin's Gap |
| | 178.21 | | 109.88 | | | |

17821
10928
6893
67310
74203

674.33
6.893
743.26

## Levels — Continued.

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 742.05 | | | | |
| | | | | 4.32 | 738.73 | Peg set at extreme low place in gap. |
| T.P. | 0.66 | 730.20 | 12.65 / 12.51 | | 729.54 | |
| T.P. | 0 48 | 718.05 | 12.68 | | 717.57 | |
| T.P. | 0.34 | 705.84 | 12.55 | | 705.50 | Nov. 20 1914 |
| T.P. | 0 34 | 693.50 | 12.68 | | 693.16 | |
| T.P. | 0.21 | 680.95 | 12.76 | | 680.74 | Run levels to 2.30 P.M. |
| T.P. | 0 43 | 668.86 | 12.52 | | 668.43 | |
| T P | 0.19 | 656.36 | 12.69 | | 656.17 | |
| T P | 0.33 | 643.87 | 12.82 | | 643.54 | |
| T P | 0.00 | 631.26 | 12.61 | | 631.26 | |
| T P | 0.15 | 618.58 | 12.83 | | 618.43 | |
| T.P. | 0.18 | 606.02 | 12.74 | | 605.84 | |
| T.P. | 0.44 | 593.84 | 12.62 | | 593.40 | |
| B.M N°10 | | | 10.65 | | 583.19 | B.M. on stone in front of Bassett's House |
| | 3.75 | | 162.61 | | | |
| | | | 3.75 | | | |
| | 742.05 | | 158.86 | | | |
| | 158.86 | | | | | From B.M. N°6 west to C.L. of R.R. by N end of depot = 9922' Slope measure. |
| | 583.19 | | | | | |

24

157.
8462
7284

# Levels on preliminary Survey Yoncalla Water System. Adams Creek

Nov 30 1914

M. B. Germond — Level
Jim. Hanna — Rod

| | | | | | | |
|---|---|---|---|---|---|---|
| T.P. | 0.38 | 583.57 | | | 583.19 | |
| T.P. | 0.14 | 570.78 | 12.93 | | 570.64 | |
| T.P. | 0.35 | 556.52 | 12.61 | | 558.17 | |
| T.P. | 0.57 | 546.52 | 12.57 | | 545.95 | |
| T.P. | 0.54 | 534.42 | 12.64 | | 533.88 | |
| T.P. | 0.21 | 522.17 | 12.46 | | 521.96 | |
| B.M. #11 | 2.19 | | 13.21 | 9.02 | 513.15 | On Cedar stump near F. Apple private Xing of Adams Creek |
| Reading | | | | 13.60? | 508.57 | Butt of Adam's Creek at Xing |
| T.P. | 11.78 | 533.01 | 0.94 | | 521.23 | |
| T.P. | 10.22 | 542.79 | 0.74 | | 532.27 | |
| T.P. | 11.89 | 553.94 | 0.47 | | 542.05 | |
| B.M. | 12.16 | 565.65 | 0.45 | 0.45 | 553.49 | Nail in Fir stump 30" dia 70' Rt of Road at edge of brush |
| T.P. | 12.04 | 577.05 | 0.64 | | 565.01 | |
| T.P. | 11.66 | 588.53 | 1.16 | | 576.87 | |
| T.P. | 2.93 | 590.54 | 0.92 | | 587.61 | |
| T.P. | 6.47 | 590.18 | 6.83 | | 583.71 | |
| T.P. | 9.30 | 596.76 | 2.72 | | 587.46 | |
| T.P. | 5.23 | 595.83 | 6.16 | | 590.60 | |
| B.M. #13 | | | | 2.23 | 593.60 | On root of |
| T.P. | 12.72 | 608.30 | 0.25 | | 595.58 | |
| T.P. | 12.17 | 619.86 | 0.61 | | 607.69 | |
| T.P. | 11.33 | 630.97 | 0.22 | | 619.64 | |
| T.P. | 12.74 | 643.61 | 0.10 | | 630.87 | |
| T.P. | 12.83 | 656.03 | 0.41 | | 643.20 | TP on nail |
| | 157.66 | | 8482 | | | |

## Levels (Cont)

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 1952 65603 | | 70.81 36.35 1952 | | |
| T.P. | 33 12,68 | 668.28 | 0.43 | | 655.60 | |
| B.M. | | | | 263 | 655.65 | On top of stump, on Hill side S. of Mill |
| T.P. | 12,61 | 680.54 | 0,35 | | 667.93 | |
| T.P | 12,56 | 692.85 | 0,25 | | 680 29 | |
| T.P. | 8.17 | 700,61 | 6.41 | | 692.44 | |
| T.P. | 7.00 | 706.50 | 1.11 | | 699.50 | |
| T.P | 11.60 | 716.11 | 1.99 | | 704.51 | |
| | 0.52 | 706.03 | 10.60 | | 705.51 | |
| B M | | | | 3.87 | 702.16 | On root of stump 150' E of old dam |
| | 0.56 | 693.77 | 12.84 | | 693.19 | |
| | 2.02 | 683.15 | 12.64 | | 681.13 | |
| | 2.02 | 672.56 | 12.61 | | 670.54 | |
| B.M | 6.11 | 675.55 | 3.12 | 312 | 669.74 | On top of stump. Big W. Fir 300' above old dam |
| | 75.87 | | 56 35 | | | |

## Levels (Cont)

| | | | | | | |
|---|---|---|---|---|---|---|
| B.M. | 6.89 | 676.33 | | | 669.44 | |
| T.P. | 12.72 | 685.78 | 3.27 | | 673.06 | |
| T.P. | 4.93 | 690.39 | 0.32 | | 685.46 | |
| T.P. | 8.67 | 695.93 | 3.13 | | 687.26 | |
| T.P. | 8.98 | 700.52 | 4.39 | | 691.54 | |
| T.P. | 10.48 | 709.69 | 1.31 | | 699.21 | |
| B.M. | | | | 2.78 | 706.91 | On big Cedar Tree at Fishermans Camp |
| T.P. | 11.39 | 720.90 | 0.18 | | 709.51 | |
| T.P. | 12.15 | 732.40 | 0.65 | | 720.25 | |
| T.P. | 12.48 | 744.55 | 0.28 | | 732.12 | |
| T.P. | 10.69 | 754.55 | 0.69 | | 743.86 | |
| T.P. | 8.39 | 757.45 | 5.49 | | 749.06 | |
| T.P. | 7.58 | 763.28 | 1.75 | | 755.70 | |
| T.P. | 9.12 | 765.64 | 6.76 | | 756.52 | |
| | | | | 10.43 | | On nail that marked Elev of Weir Crest. |
| | | | | 7.92 | 757.72 | B.M. on alder near where Creek was measured |
| TP | 5.8+ | 770.03 | 0.45 | | 765.19 | |
| TP | 12.97 | 782.30 | 1.70 | | 769.33 | |
| T.P. | 9.65 | 790.65 | 1.30 | | 781.00 | |
| | 9.62 | 799.18 | 1.09 | | 789.56 | |
| BM | - | | | 0.78 | 798.40 | On small white fir |
| T.P. | 9.36 | 808.16 | 0.38 | | 798.80 | |
| | 8.62 | 815.29 | 1.49 | | 806.67 | |
| | | | 2.46 | | 812.81 | |
| | 180.48 | | 37.11 | | | |

180.48
37.11
143.37
669.44
812.81

Dec 1st 1917

M. B. Germond – Level
Jim Hanna – Rod
Cold and Frosty

## Levels (Cont)

| | | | | | | |
|---|---|---|---|---|---|---|
| T.P. | 13.00 | 825.81 | | | 812.81 | |
| T.P. | 12.57 | 837.77 | 0.61 | | 825.20 | |
| T.P. | 12.78 | 850.32 | 0.23 | | 837.54 | |
| T.P. | 11.08 | 861.17 | 0.23 | | 850.09 | |
| T.P. | 12.31 | 872.96 | 0.52 | | 860.65 | Nail in Maple tree |
| | 11.82 | 883.98 | 0.80 | | 872.16 | |
| | 11.90 | 895.22 | 0.76 | | 883.22 | |
| | 8.38 | 902.67 | 0.83 | | 894.29 | |
| | 8.19 | 910.32 | 0.54 | | 902.13 | |
| | 102.03 | | | 10.71 | | Crest of Falls |
| | 4.52 | | 4.52 | .07 | 910.25 | B.M. on root of small Maple tree. |
| | 97.51 | | | | | |
| | 812.81 | | | | | |
| | 910.32 | | | | | |

Dec 2 1914

Very rainy

M.B. Germond

Jim. Hanna

Dist changed from B.M. #6

To Weir eight acar more fence = 14.75'

Rough chaining and not accurate

Dec 3 1914

M. B. Germond

Jim Hanna

Reconnaissance and stake Making

28

Plat this on Scale 200 to 1" — 8 3/4 x 10 3/4

# "A" Line Moncolla prc Preliminary Water Survey Dec. 4 1914

## Field Notes

| | Ang. Rt | Ang. Lt. | Bring. | "A" I | Dist |
|---|---|---|---|---|---|
| 0+00 | | | | 800.68 | |
| | 11 | | N 17 50 E | | 80.48 |
| 0+80.48 | | | | | |
| | 19 10 | | N 36° 05 E | | 99.49 |
| 1+79.97 | | | | | |
| | 17° 14' | | N 45 50 E | | 149.43 |
| 3+29.40 | | | | | |
| | 00 28' | | N 45° 15 E | | 111.75 |
| 4+41.15 | | | | | |
| | 11 32' | | N 55-45 E | | 129.50 |
| 5+70.65 | | | | | |
| | 9° 57' | | N 63-20 E | | 96.52 |
| 6+67.17 | | | | | |
| | | 22° 07' | N 44° 00 E | | 128.98 |
| 7+96.15 | | | | | |
| | | 33° 46' | N 10° 15 E | | 170.65 |
| 9+66.80 | | | | | |
| | 18 41 | | N 28 30 E | | 249.68 |
| 12+16.48 | | | | | |
| | | 21° 08 | N 6° 00 E | | 303.37 |
| 15+19.85 | | | | | |
| | 24 07 | | N 32 30 E | | 98.55 |
| 16+18.40 | | | | | |

Brng. of 0+80.48 = N 17° 50' E

Sta. set N 63° 15' E of "H" B.M. Elev 798.40

Var. of needle = 21° 45' E

M.B. Germond - In charge

Jim Hanna - Chman 1

Jim Lee - Axman 1

Geo. Hirshberger - Chman 1/2

"A" Line

Very rainy + snow

0+00 Dam

Under rock bluff near weir sight

| | Ang Rt | Ang Lt | Bring | V. C. | Dist |
|---|---|---|---|---|---|
| | 38° 51' | | N 69 45 E | | 219.90 |
| 18+38 3 | | | | | |
| | | 42° 59' | N 27 00 E | | 417.00 |
| 22+55 3 | | | | | |
| | | 11° 38' | N 15° 30 E | | 242.35 |
| 24+97 65 | | | | | |
| | | 1° 07' | N 13. 05 E | | 227.15 |
| 27+24 80 | | | | | |
| | | 28° 33' | N 14° 00 W | | 182.25 |
| 29+07 05 | | | | | |
| | | 17' 46' | N 31 05 W | | 239.35 |
| 31+46 40 | | | | | |
| | 15° 50 | | N 18 25 W | | 125.50 |
| 32+71 90 | | | | | |
| | 36° 30' | | N 18° 00 E | | 105.00 |
| 33+76 90 | | | | | |
| | 19° 48' | | N 38 20 E | | 306.50 |
| 36+83 40 | | | | | |
| | | 3° 08' | N 35° 45' E | | 404.85 |
| 40+88 25 | | | | | |
| | 1° 36' | | N 37 35 E | | 263.30 |
| 43+51 55 | | | | | |
| | | 33° 30' | N 4 15 E | | 736.45 |
| 50+88 00 | | | | | |
| | | | | | 3249.70 |

"A" Line Cont.

Dec 5 1914

M. B. Germond 2¼ hrs
Geo. Harshberger — 2¼ hrs
Jim Hanna 2¼ "
Jim Lee 1¼ "

Rain + Snow

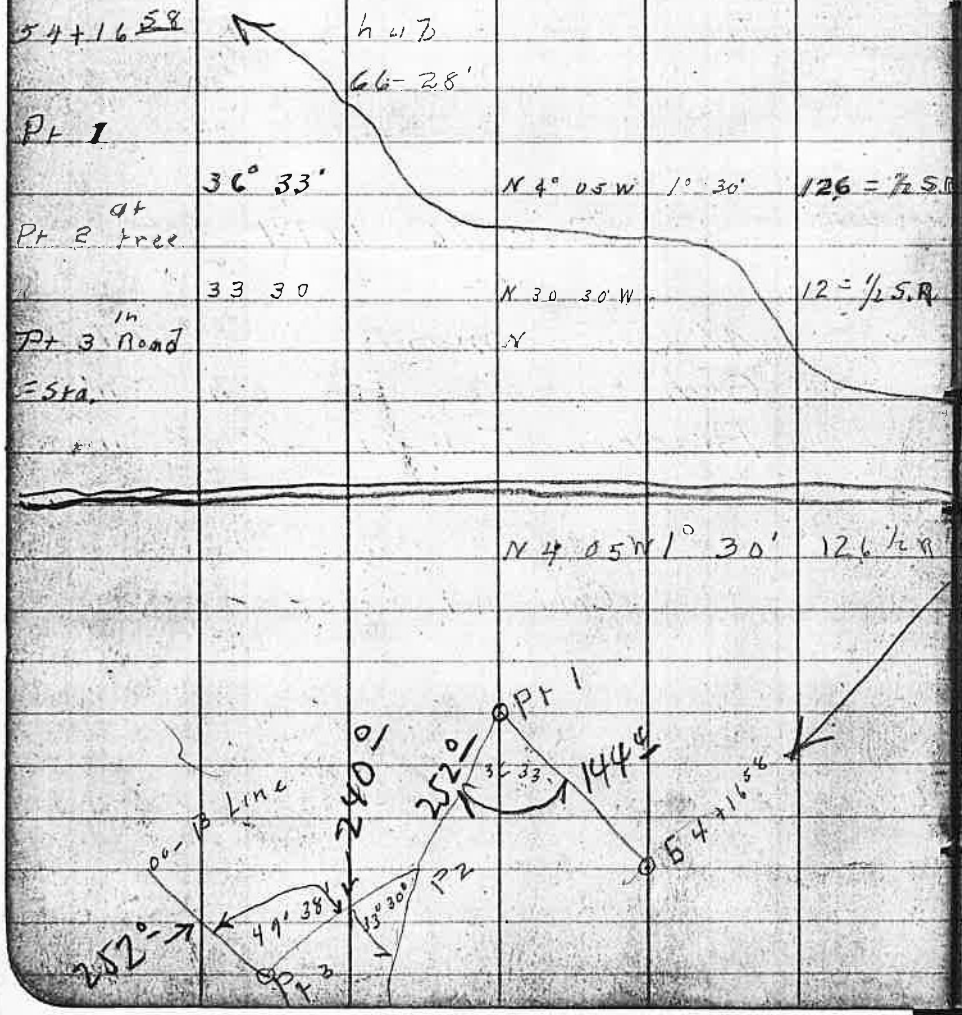
Dec 16 1914

M. B. Germond 1 day
Geo. Harshberger — Ch "
Preston Turpin — Ch "

Cold and Frost

30

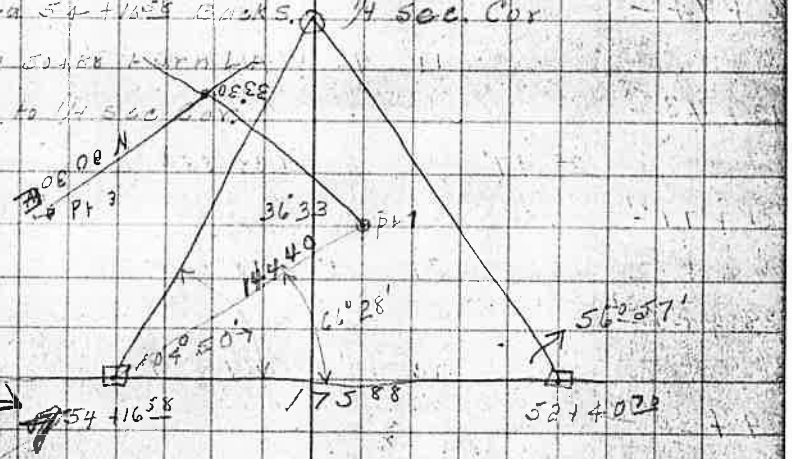
| | Ang Rt | Ang Lt | Bring | V.C. | Dist |
|---|---|---|---|---|---|
| | 23° 59' | | N 25 00 E | | 328.26 |
| 52 + 40 7° | | hub | | | |
| 53 + 12 15 | | hub | | | |
| 54 + 16 58 | | hub | | | |
| | | 66-28' | | | |
| Pt 1 | | | | | |
| | 36° 33' | | N 4° 05 W | 1° 30' | 126 = ½ S.R |
| Pt 2 at tree | | | | | |
| | 33 30 | | N 30 30 W | | 12 = ½ S.R |
| Pt 3 in Road | | | N | | |
| = Sta. | | | | | |
| | | | N 4 05 W | 1° 30' | 126 ½ R |




"A" Line (Cont.)

△ on Sta 52 + 40 7° Sight ahead Turn Rt 56° 57'
To ¼ Corner Bet Secs 32 T 23S -
Fred Applegate's Line

△ on sta 54 + 16 58 Cacks S. ¼ Sec. Cor
On sta 52 + 40 Turn Lt
104° 30' to ¼ Sec Cor.




△ at Sta 54 + 16 58 Sight on Sta 52 + 40 7° Turn Lt
66° 28' to pt 144.40 ft dist

Dec 17 1914

M.B. Germond 1
Preston Turpin — Axman 1
Ray Turpin — " 1
Jim Hanna — Chman 1
Geo. Harshberger — " 1

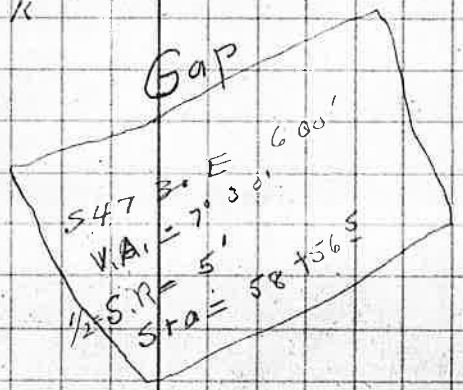
# Field Notes on "B" Line Transit Work. Began near F. Applegate's House

| | Ang Rt | Ang Lt | Bring | V. C. | Dist |
|---|---|---|---|---|---|
| 6 + 00 | | | N 20° 15 W | | |
| | | | | | 373.60 |
| 3 + 73.60 | | | | | |
| | | 2° 05' | N 22° 15 W | | 301.29 |
| 6 + 74.89 | | | | | |
| | | 19° 42 | N 41 30 W | | 668.61 |
| 13 + 43.50 | | | | | |
| | 2° 17' | | N 38 55 W | | 834.11 |
| 21 + 77.61 | | | | | |
| | | 31° 08' | N 70 00 W | | 647.41 |
| 28 + 25.02 | | | | | |
| | | 23° 43' | S 84 50 W | | 595.93 |
| 34 + 20.95 | | | | | |
| | | 40° 25' | S 44 00 W | | 819.85 |
| 42 + 40.80 | | | | | |
| | | 4° 57' | S 41 00 W | | 888.45 |
| 51 + 29.25 | h w b | | | | |
| | | Continue line to | | | 318.45 |
| 54 + 47.70 | | | | | |
| | 18° 51' | | S 58 45 W | | 408.35 |
| 58 + 56.05 | | | | | |
| | 21° 06' | | S 80 30 W | | |
| | | | | | 5856.05 |

2459

Pt in Co. Road 20 ft from Center of the Road

Bridge Xing Adam's Creek




Dec 17 1914

Cold & Frost

Transit at 42 + 40.80 B.S. on 34 - 20.95 turn Lt 100° 02'
to Witness tree N 55° W N. Tree.
Set on 51+29.25 B.S. on 42+40.8 Turn Lt 58° 55'
N 19° 15' W

32

| | | | | | |
|---|---|---|---|---|---|
| 58 56 05 | Ang Rt | | | | |
| 64 + 86 35 | hub | | | | |
| 72 + 67 20 | hub | | | | |
| 75 + 67 50 | hub | | | | |
| 78 + 33 50 | " | | | | |
| 81 + 09 92 | " | | | | |
| 82 + 82 13 | " | | | | |
| 86 + 75 62 | " | | | | |
| 88 + 96 0 | " | | | | |
| | | | | 4043 95 | |
| 96 + 49 10 | " | | | | |
| 99 + 00 | " | | | | |
| 58 56 05 | | | | | |
| 40 43 95 | 7' 03 | | S 88° 15 W | | |
| 106 + 50 | hub | | | | |
| 118 + 50 | " | | | | |

Dec 17 1914

Cold & Frost

Dec 18 1914

M. B. Germond /
Geo. Harshbarger /
Preston Turpin /
Ray Turpin /
Jim Hanna /

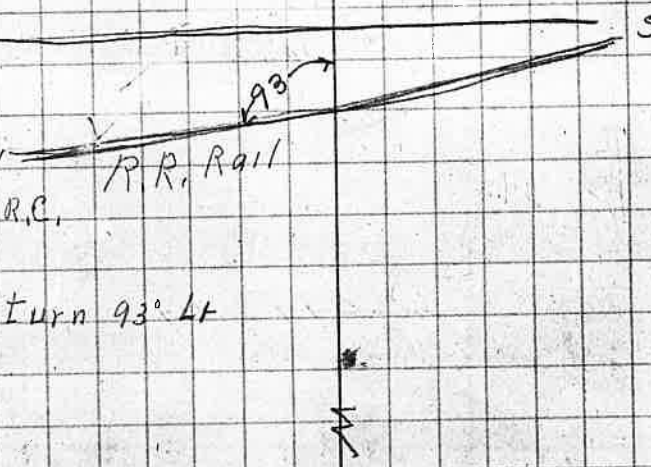
Center of Reservoir

33

| | | |
|---|---|---|
| 127 + 20.89 | hub | 4' west of Findlays E Line |
| 136 + 50 | " | |
| 142 + 50 | " | 9974.3 |
| 168 + 00 | " | |
| 181 + 50 | | |
| 189 + 00 | | |
| 192 + 00 | | |
| 198 + 01.12 | ± Outside of ℄ R.R. Rail | |
| 198 + 74.3 ± | Intersect on R.C. of Curb 1.7' S. of N. end of R.C. | |
| 99.44 / 99 743 | Transit on ℄ S. side of rail B.S. on line and turn 93° Lt | |

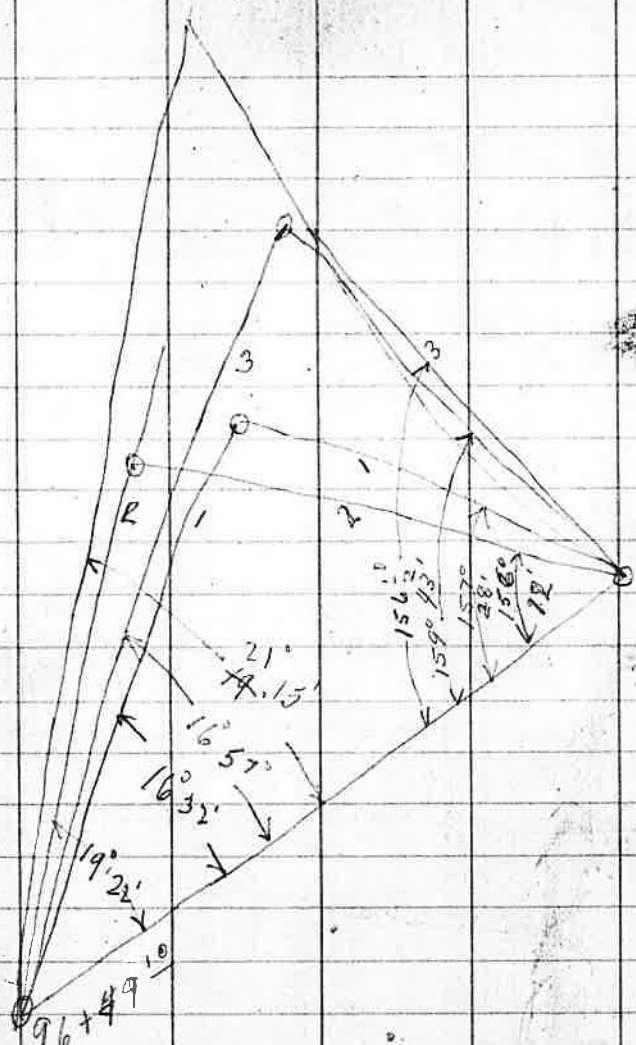
93° 00 1.12
87 00 24.3'

B.T. 2417.5




Dec 19 1914
Geo Harsh Recorder
M. B. Germond
Jim Hanna

34




Very cold + snowy

Dec 19 1914

35

Levels on the "B" Line.

Beginning at Sta. 58+56.05 and running backwards along the line

| | | | | | | |
|---|---|---|---|---|---|---|
| | 324 | 578.38 | | | 575.14 | |
| T.P. | 090 | 566.99 | | 12.24 | 566.09 | |
| 58+56.05 | | 567.0 | 5.73 | | 561.26 | hub |
| +50 | | | 6.1 | | 560.9 | |
| 58 +00 | | | 9.3 | | 57.7 | |
| +50 | | | 12.6 | | 54.4 | |
| 57 | | | 13.6 | | 53.4 | |
| +50 | | | 14.1 | | 52.9 | |
| 56 | | | 14.8 | | 52.2 | |
| +50 | | | 14.4 | | 52.6 | |
| 55 | | | 14.0 | | 53.0 | |
| +50 | | | 11.4 | | 55.6 | |
| +47.20 | | | 11.38 | | 555.61 | hub |
| 54 | | | 11.6 | | 55.4 | |
| +50 | | | 11.8 | | 55.2 | |
| 53 | | | 13.0 | | 54.0 | |
| +50 | | | 12.7 | | 54.3 | |
| 52 | | | 12.4 | | 54.6 | |
| +50 | | | 10.3 | | 56.7 | |
| +29.25 | | | 10.2 | | 56.8 | |
| 51 | | | 11.3 | | 55.7 | |
| | 0.47 | 555.01 | | 12.45 | 554.54 | |
| +50 | | | 1.8 | | 53.2 | |
| 50 | | | 5.3 | | 49.7 | |

M.B. Germond
Jim Hanna - R.O.W
Dec 19

Levels Cont.

B. Line

| | | | | | |
|---|---|---|---|---|---|
| | | 555.01 | | | |
| 49+50 | | | 7.6 | | 547.4 |
| 49 | | | 10.8 | | 44.2 |
| T.P. | 0.68 | 542.61 | | 13.08 | 541.93 |
| +50 | | | 1.5 | | 41.1 |
| 48 | | | 6.6 | | 36.0 |
| +50 | | | 12.3 | | 30.3 |
| 47 | | | 12.0 | | 30.6 |
| +50 | | | 11.6 | | 31.0 |
| T.P. | 0.60 | 520 54 | | 12.67 | 529.94 |
| 46 | | | 1.9 | | 28.6 |
| +50 | | | 2.4 | | 28.1 |
| 45 | | | 4.1 | | 26.4 |
| +50 | | | 6.6 | | 23.9 |
| 44 | | | 7.6 | | 22.9 |
| +50 | | | 8.3 | | 22.2 |
| 43 | | | 8.4 | | 22.1 |
| +50 | | | 10.1 | | 20.4 |
| +40 80 | | | 10.31 | | 20 23 |
| 42 | | | 13.2 | | 17.34 |
| T.P. | 0.12 | 518.12 | | 12.54 | 518.00 |
| +50 | | | 4.3 | | 513.8 |
| 41 | | | 6.3 | | 11.8 |
| +50 | | | 7.6 | | 10 4 |
| 40 | | | 8.3 | | 09.8 |

Levels [Cont]

"B" Line

| | | | | | |
|---|---|---|---|---|---|
| | | 576.12 | | | |
| 39 + 50 | | | 9.1 | | 09.0 |
| 39 | | | 11.5 | | 06.6 |
| T.P. | 0.31 | 566.25 | | 12.18 | 505.94 |
| + 50 | | | 2.6 | | 03.6 |
| 38 | | | 5.9 | | 500.3 |
| + 50 | | | 8.7 | | 497.6 |
| 37 | | | 11.0 | | 95.2 |
| + 50 | | | 13.2 | | 93.0 |
| T.P. | 0.45 | 494.35 | | 12.35 | 493.90 |
| 36 | | | 4.9 | | 89.4 |
| + 50 | | | 7.5 | | 86.8 |
| 35 | | | 9.2 | | 83 2 |
| + 50 | | | 12.3 | | 82.0 |
| + 20.95 | | | 10.70 | | 483.65 H |
| 34 | | | 12.00 | | 82.4 |
| + 50 | | | 12.10 | | 82.2 |
| 33 | | | 12.2 | | 82.2 |
| + 50 | | | 12.8 | | 81.6 |
| 32 | | | 13.2 | | 81.2 |
| | 4.83 | 486.79 | | 12.99 | 481.96 |
| + 50 | | | 6.2 | | 80 6 |
| 31 | | | 8.0 | | 78.6 |
| + 50 | | | 7.8 | | 79.0 |
| 30 | | | 6.4 | | 80.4 |

"B" Line

Levels (Cont)

Dec 19 '44

| | | | | | |
|---|---|---|---|---|---|
| | | 488.79 | | | |
| +50 | | | 3.1 | | 483.7 |
| 29 | | | 1.7 | | 85.1 |
| +50 | | | 4.3 | | 82.5 |
| +25 | | | 5.7 | | 81.1 |
| 28 | | | 5.6 | | 81.2 |
| +50 | | | 3.4 | | 83.4 |
| 27 +50 | | | 4.6 | | 82.2 |
| +50 | | | 6.4 | | 80.4 |
| 26 | | | 7.8 | | 79.0 |
| +50 | | | 7.3 | | 79.5 |
| 25 | | | 7.4 | | 79.4 |
| +50 | | | 8.0 | | 78.8 |
| 24 | | | 8.7 | | 78.1 |
| +50 | | | 6.8 | | 80.0 |
| 23 | | | 6.8 | | 80.0 |
| +50 | | | 4.2 | | 82.6 |
| 22 | | | 1.9 | | 84.9 |
| Hub for T.P. | 9.45 | 493.19 | | 305 | 483.74 |
| +50 | | | 9.3 | | 83.9 |
| 21 | | | 10.1 | | 83.1 |
| +50 | | | 10.9 | | 82.3 |
| 20 | | | 12.0 | | 81.2 |
| +50 | | | 11.1 | | 82.1 |
| 19 | | | 9.1 | | 84.1 |

Levels (Cont.)

"B" Line

| | | | | | |
|---|---|---|---|---|---|
| 1 +50 | | 493.19 | 5.4 | | 487.8 |
| 18 | | | 4 0 | | 89.2 |
| +50 | | | 4,1 | | 89.1 |
| 17 | | | 4,8 | | 88,4 |
| +50 | | | 6,0 | | 87,2 |
| 16 | | | 6,5 | | 86.7 |
| +50 | | | 7,1 | | 86.1 |
| 15 | | | 9,2 | | 87.0 |
| +50 | | | 7,8 | | 85.4 |
| 14 | | | 2,4 | | 90,8 |
| T.P. | 2,18 | 494.99 | | 0,38 | 492.81 |
| +50 | | 493 0 | 1,3 | | 93,7 |
| 1478 | | | 1,20 | | 93.8 |
| 13 | | | 2,2 | | 92.8 |
| +50 | | | 4,9 | | 90.1 |
| 12 | | | 2,3 | | 92.7 |
| +50 | | | 4,1 | | 90.9 |
| 11 | | | 6,0 | | 89.0 |
| +50 | | | 6,7 | | 88,3 |
| 10 | | | 7,8 | | 87.2 |
| +50 | | | 9,5 | | 85,5 |
| 9 | | | 11,2 | | 83.8 |
| +50 | | | 13.1 | | 81.9 |
| T.P. | 4.00 | 486,54 | | 12,45 | 482,54 |

Levels Cont

B "Line"

Dec 19 1914

Very Cold + Snowy

| | | | | |
|---|---|---|---|---|
| 8 | 486.54 | 6.3 | | 80.2 |
| +50 | | 7.1 | | 79.4 |
| 7 | | 7.7 | | 78.8 |
| +4 | | 7.87 | | 78.7 |
| +50 | | 7.9 | | 78.6 |
| 6 | | 8.4 | | 78.1 |
| +50 | | 7.7 | | 78.8 |
| 5 | | 7.9 | | 78.6 |
| +50 | | 7.7 | | 78.8 |
| 4 | | 6.9 | | 79.6 |
| +50 | | 6.7 | | 79.8 |
| 3 | | 7.7 | | 78.8 |
| +50 | | 7.2 | | 79.3 |
| 2 | | 8.1 | | 78.4 |
| +50 | | 7.8 | | 78.7 |
| 1+04 | | 6.9 | | 79.6 |
| +50 | | 6.7 | | 79.8 |
| 0+00 | | 4.3 | | 77.2 |

41

Levels on the "A" Line

Beg at Sta 0+00 "A" Line

| | | | | | | |
|---|---|---|---|---|---|---|
| | 0.94 | 799.34 | | | 798,40 | B.M. on W. Fir opposite Sta 0+00 |
| 0+00 | | | 3.15 | | 796,19 | |
| +50 | | | 1.2 | | 98.1 | |
| +80 4.8 | | | 4.5 | | 94.8 | 4.48 M. B. Germond |
| 1+00 | | | 7.8 | | 91.5 | Tim Hanna – Rod |
| +50 | | | 5.9 | | 93.4 | |
| T.P. | 6.20 | 799.92 | 5.62 | 5.62 | 793.72 | 11 |
| 2+00 | | | 8.9 | | 91.0 | |
| +50 | | | 10.2 | | 89.7 | Very Cold & Snow |
| 3+00 | | | 12.5 | | 87.4 | |
| +29 4.0 | | | 17.2 | | 85.7 | 13 B.L. |
| | 1.73 | 789.01 | | 12.64 | 78128 | Dec 20 1914 |
| 3+50 | | | 3.5 | | 85.5 | |
| 4+00 | | | 8.1 | | 80.9 | |
| +41 1.5 | | | 9.51 | | 79.5 | 11 |
| +50 | | | 10.01 | | 79.0 | |
| | 3.35 | 782,22 ✓ | | 10.14 | 778 87 | |
| 5+00 | | | 5.8 | | 76 4 | |
| +50 | | | 4.6 | | 77 6 | |
| +70 6.5 | | | 5.06 | | 77 16 | |
| 6+00 | | | 11.0 | | 71.2 | |
| +50 | | | 7.6 | | 74.6 | |
| +67 11 | | | 5.59 | | 76,03 | 14 |
| 7+00 | | | 8.9 | | 73 3 | |
| | 12.22 | | | 2.48 | | |

42

## Levels

"A" Line

| | | | | | |
|---|---|---|---|---|---|
| | | 782.22 | | | |
| | 068 | 772.05 | | 10.85 | 771.37 |
| 7+50 | | | 4.1 | | 68.0 |
| 7+96.5 | | | 1.90 | | 70.2 |
| 8 | | | 2.00 | | 70.1 |
| +50 | | | 12.2 | | 59.8 |
| 9 | | | 10.2 | | 61.8 |
| +50 | | | 11.5 | | 60.6 |
| 9+66.80 | 277 | 763.43 | | 11.39 | 762.66 |
| 10 | | | 1.4 | | 62.0 |
| +50 | | | 6.1 | | 57.3 |
| 11 | | | 7.8 | | 53.6 |
| +50 | | | 14.5 | | 48.9 |
| 12 | | | 10.5 | | 52.9 |
| 12+16.98 | | | 7.00 | | 56.4 |
| +50 | | | 7.00 | | 56.4 |
| 13 | | | 12.5 | | 50.9 |
| +50 | | | 10.5 | | 53.4 |
| 14 | | | 10.3 | | 53.1 |
| T.P. | 192 | 754.90 | | 12.45 | 750.98 |
| 450 | | | 3.0 | | 49.9 |
| 15 | | | 5.2 | | 47.7 |
| +19.89 | | | 6.32 | | 46.6 |
| +50 | | | 6.5 | | 46.4 |
| 16 | | | 8.6 | | 44.3 |
| | 5.37 | | | 3.469 | |

R.R
13.00 = 8+35 Small Creek From E also wire fence

"A" Line

| | | Levels | | | |
|---|---|---|---|---|---|
| | | 752.90 | | | |
| | 6.19 | 747.01 | | 12.08 | 740.82 |
| 16 + 18 | | | 4.80 | | 42.2 |
| + 50 | | | 9.2 | | 37 8 |
| 17 | | | 14.8 | | 32.2 |
| T.P. | 2.49 | 737.32 | | 12.18 | 734.83 |
| + 50 | | | 11.1 | | 26.2 |
| 18 | | | 12.1 | | 25.2 |
| + 38 3 | | | 6.21 | | 31.1 |
| + 50 | | | 8.3 | | 29.0 |
| | 7.13 | 731.57 | | 12.88 | 72444 |
| 19 | | | 9.4 | | 22.2 |
| + 50 | | | 8.3 | | 23.3 |
| 20 - | | | 12.9 | | 18.77 |
| | 1.45 | 720.82 | | 12.20 | 719.37 |
| + 50 | | | 6.2 | | 14.6 |
| 21 | | | 6.7 | | 12.1 |
| + 50 | | | 13.0 | | 07.8 |
| 22 | | | 15.5 | | 05.3 |
| | 0.50 | 708.52 | | 12.80 | 708.02 |
| + 50 | | | 2.4 | | 06.1 |
| + 55 30 | | | 2.08 | | 06.4 |
| 23 | | | 13.1 | | 95.4 |
| + 50 | | | 11.1 | | 97.4 |

Creek from East Lumber Camp

Levels.

"F1" Line

| | | | | | |
|---|---|---|---|---|---|
| | | 708.52 | | | |
| 24 | | | 13.0 | | 95.5 |
| +50 | | | 11.3 | | 97.2 |
| | 2.26 | 700.28 | | 10.50 | 698.02 |
| +97.66 | | | 4.08 | | 96.2 |
| 25 | | | 4.2 | | 96.1 |
| +50 | | | 8.8 | | 91.5 |
| 26 | | | 11.1 | | 89.2 |
| +50 | | | 11.3 | | 89.0 |
| | 3.44 | 693.07 | | 10.65 | 689.63 |
| 27 | | | 7.5 | | 85.6 |
| +248 | | | 6.5 | | 86.6 |
| +50 | | | 5.3 | | 87.8 |
| 28 | | | 2.2 | | 90.9 |
| +50 | | | 5.5 | | 87.6 |
| | | | | | |
| TP | 7.10 | 699.95 | | 0.22 | 692.85 |
| 29 | | | 9.78 | | 90.1 |
| +50 | | | 9.9 | | 90.0 |
| 30 | | | 12.7 | | 87.2 |
| +50 | | | 5.0 | | 94.9 |
| | 11.63 | 710.80 | | 0.78 | 699.17 |
| 31 | | | 11.0 | | 99.8 |
| +96.40 | | | 12.47 | | 98.3 |
| 50 | | | 11.9 | | 98.9 |

"A" Line

| | | | | | | |
|---|---|---|---|---|---|---|
| | | Levels | | | | |
| | | 710.80 | | | | |
| 32 | | | 10.8 | | 700.0 | |
| +50 | | | 12.7 | | 98.1 | |
| + | | | 13.0 | | 97.8 | H |
| | 682 | 709.87 | | 7.75 | 703.05 | |
| 33 | | | 6.3 | | 03.6 | |
| +50 | | | 4.7 | | 05.2 | |
| +76 9/10 | | | 4.3 | | 05.6 | H |
| 34 | | | 4.5 | | 05.4 | |
| +50 | | | 8.6 | | 01.3 | |
| 35 | | | 14.7 | | 95.2 | |
| +50 | | | 12.5 | | 97.4 | |
| | | | 7.73 | | 702.14 | Check 13 M 702.16 |
| 36 | | | 5.5 | | 04.4 | Opposite old dam |
| | 561 | 714.73 | = | 0.70 | 709.12 | |
| +50 | | | 4.3 | | 10.4 | |
| +83 4/10 | | | 2.86 | | 11.8 | H |
| 37 | | | 3.8 | | 10.9 | |
| +50 | | | 10.9 | | 03.8 | |
| 38 | | | 18.0 | | 96.7 | |
| +50 | | | 19.4 | | 95.3 | |
| 39 | | | 16.0 | | 98.7 | |
| +50 | | | 12.8 | | 01.9 | |
| | 046 | 702.81 | | 12.38 | 702.35 | |
| 40 | | | 4.3 | | 98.5 | |

"A" Line

Levels

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 702.81 | | | | |
| +50 | | | 7.6 | | 95.2 | |
| +88.25 | | | 2.9 | | 95.7 | H |
| 41 | | | 7.5 | | 95.3 | |
| + | 0.25 | 690.28 | | 12.78 | 690.03 | |
| 50 | | | 3.2 | | 87.1 | |
| 42 | | | 12.1 | | 78.2 | |
| | 0.50 | 678.41 | | 12.38 | 677.91 | |
| +50 | | | 5.4 | | 73.0 | |
| 43 | | | 8.4 | | 70.0 | |
| +50 | | | 7.4 | | 71.0 | |
| 43+51.55 | | | 7.43 | | 71.06 | H |
| | 0.07 | 665.89 | | 12.59 | 665.82 | |
| 44 | | | 3.1 | | 62.8 | |
| +50 | 0.35 | 653.82 | | 12.42 | 653.47 | |
| | | | 2.3 | | 51.5 | |
| 45 | | | 13.1 | | 40.7 | |
| | 0.69 | 641.70 | | 12.81 | 641.01 | |
| 50 | | | 11.8 | | 29.9 | |
| T.P. | 0.28 | 629.33 | | 12.65 | 629.05 | |
| 46 | | | 1.2 | | 28.1 | |
| T.P. | 0.08 | 617.12 | | 12.29 | 617.04 | |
| +50 | | | 8.8 | | 08.3 | |
| | 1.60 | 605.55 | | 12.57 | 604.58 | |
| 47 | | | 3.5 | | 02.6 | |

47

Levels

"A" Line

Jim Hanna
M. B. Germond

Cold and Snow

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| | | 605.55 | | | | | |
| +50 | | | 4.3 | | 01.2 | | |
| 48 | | | 7.2 | | 98.3 | | |
| | 0.55 | 594.61 | | 11.49 | 594.06 | | |
| +50 | | | 5.3 | | 89.3 | | |
| 49 | | | 7.2 | | 87.4 | | |
| +50 | | | 4.4 | | 90.2 | | |
| 50 | | | 4.5 | | 90.1 | | |
| +50 | | | 2.4 | | 92.2 | | |
| | 1.88 | 595.48 | 1.01 | 1.01 | 593.60 | Check B.M. | 593.60 |
| +88 | | | 4.82 | | 90.7 | | |
| 51 | | | 4.9 | | 90.6 | | |
| +50 | | | 12.4 | | 83.1 | | |
| | 2.39 | 585.62 | | 12.25 | 583.23 | | |
| 52 | | | 5.3 | | 80.3 | | |
| +45 | | | 5.36 | | 80.2 | H | |
| +50 | | | 5.2 | | 80.4 | | |
| 53 | | | 3.6 | | 82.0 | | |
| +12 15 | | | 2.65 | | 582.97 | H | |

Levels on "B" Line and running ahead along Line from Sta. 58+56.05

Dec 21 1914

| | | | | | |
|---|---|---|---|---|---|
| 58+56.05 | 7.42 | 568.64 | | | 561.26 |
| 59 | | | 10.6 | | 56.1 |
| +50 | | | 15.1 | | 53.6 |
| 60 | | | 7.7 | | 61.0 |
| +50 | | | 4.3 | | 64.4 |
| 61 | | | 4.8 | | 63.9 |
| T.P. | 12.37 | 580.93 | | 0.12 | 568.56 |
| +50 | | | 8.7 | | 72.2 |
| | | | 5.79 | | 575.14 |
| 62 | | | 3.9 | | 77.0 |
| +50 | | | 0.5 | | 80.4 |
| T.P | 12.73 | 593.65 | | 0.01 | 580.92 |
| 63 | | | 9.7 | | 84.0 |
| +50 | | | 6.8 | | 86.8 |
| 64 | | | 3.8 | | 89.8 |
| +50 | | | 0.5 | | 93.2 |
| T.P. | 12.99 | 606.52 | | 0.12 | 593.53 |
| +86.25 | | | 11.37 | | 95.15 |
| 65 | | | 10.5 | | 96.0 |
| +50 | | | 8.1 | | 98.4 |
| 66 | | | 5.9 | | 600.6 |
| +50 | | | 3.9 | | 02.6 |
| 67 | | | 2.4 | | 04.1 |
| +50 | | | 2.2 | | 04.3 |
| | 4.56 | | | .125 | |

"B" Line

Levels

| | | | | | |
|---|---|---|---|---|---|
| | | 606.52 | | | |
| | 12.81 | 618.91 | | 0.72 | 606.10 |
| 68 | | | 11.5 | | 07.4 |
| +50 | | | 8.9 | | 10 0 |
| 69 | | | 15.4 | | 03 5 |
| +50 | | | 6.3 | | 12 6 |
| 70 | | | 1.1 | | 17.8 |
| | 12.37 | 630.76 | | 0.52 | 618.39 |
| +50 | | | 3.8 | | 27.0 |
| 71 | | | 1.8 | | 29.0 |
| | 7.82 | 638.47 | | 0.14 | 630.62 |
| +50 | | | 7.5 | | 30.9 |
| 72 | | | 2.7 | | 35.7 |
| +50 | | | 0.5 | | 37.9 |
| +67.20 | | | 0.98 | | 637.46 |
| 73 | | | 3.1 | | 35 3 |
| +50 | | | 12.5 | | 25.9 |
| T.P. | 5.80 | 632.26 | | 11.98 | 626.46 |
| 74 | | | 16.2 | | 16.1 |
| +50 | | | 13.6 | | 18.7 |
| 75 | | | 1.9 | | 30.4 |
| T.P. | 4.84 | 635.93 | | 1.17 | 631.09 |
| +50 | | | 1.7 | | 34.2 |
| +67.50 | | | 2.01 | | 33.92 |
| 76 | | | 4.5 | | 31.4 |
| | 4.364 | | | 1.423 | |

50

"B" Line

Levels

| | | | | | |
|---|---|---|---|---|---|
| | | 635.93 ✓ | | | |
| 76+50 | | | 12.9 | | 24.0 |
| T.P. | 10.56 | 633.54 | | 12.95 | 622.98 |
| 77 | | | 20.0 | | 613.5 |
| +50 | | | 3.3 | | 630.2 |
| T.P. | 11.56 | 644.68 | | 0.42 | 633.12 |
| T.P | 12.00 | 656.27 | | 0.41 | 644.27 |
| 78 | | | 10.2 | | 46.1 |
| +33.50 | | | 7.58 | | 648.69 H |
| +50 | | | 7.5 | | 48.8 |
| B.M. | | | 12.40 | | 643.87 B.M put on B.O. tree 8" dia 24' Lt sta 78+63 |
| 79 | | | 6.3 | | 50.0 |
| +50 | | | 7.6 | | 48.7 |
| 80 | | | 6.1 | | 50.2 |
| +50 | | | 4.3 | | 52.0 |
| 81 | | | 3.1 | | 53.2 |
| 099° | | | 3.15 | | 653.12 H |
| +56 | | | 6.9 | | 649.37 |
| [illegible] | | | [illegible] | | |
| | 1.07 | 645.32 | | 12.02 | 644.25 |
| 82 | | | 3.0 | | 642.32 |
| +50 | | | 2.7 | | 42.6 |
| +82.13 | | | 5.75 | | 39.6 |
| 83 | | | 10.2 | | 35.1 |
| | 0.25 | 632.59 ✓ | | 12.98 | 632.34 |

5/

Levels

"B" Line

| | | | | | |
|---|---|---|---|---|---|
| | 5 | 632.54 ✓ | | | |
| T.P | 0.37 | 620.42 | | 12.54 | 620.05 |
| 83 + 50 | | | 1.2 | | 619.2 |
| T.P | 0.00 | 607.77 | | 12.65 | 607.77 |
| 84 | | | 5.2 | | 602.6 |
| T.P. | 3.69 | 599.13 | | 12.33 | 595.44 |
| + 50 | | | 13.7 | | 85.4 |
| 85 | | | 1.7 | | 97.4 |
| T.P. | 12.26 | 611.03 | | 0.36 | 598.77 |
| T.P. | 12.66 | 623.47 | | 0.22 | 610.81 |
| + 50 | | | 3.5 | | 620.0 |
| | 11.65 | 634.87 | | 0.25 | 623.22 |
| T.P. | 5.81 | 640.40 | | 0.28 | 634.59 |
| 86 | | | 3.2 | | 37.2 |
| + 50 | | | 2.5 | | 37.9 |
| + 75 62 | | | 3.16 | | 37.24 |
| 87 + 00 | | | 8.8 | | 31.6 |
| T.P. | 5.60 | 633.20 | | 12.80 | 627.60 |
| + 50 | | | 18.0 | | 615.20 |
| T.P. | 12.91 | 645.88 | | 0.23 | 632.97 |
| 88 | | | 1.5 | | 44.4 |
| T.P. | 12.78 | 658.56 | | 0.10 | 645.78 |
| + 50 | | | 1.5 | | 57.1 |
| | 5.98 | 663.68 ✓ | | 0.86 | 657.70 |
| ~~89~~ 88 + 96 00 | | | 2.80 | | 60.9 |

623.19

52

Levels

| | | | | | |
|---|---|---|---|---|---|
| | 30.75 | | | 3955 3870 85 | |
| | | 663.68 ✓ | | | |
| 89 | | | 2.7 | | 61.0 |
| +50 | | | 3.9 | | 59.8 |
| 90 | | | 10.7 | | 53.0 |
| T.P | 0.51 | 651.51 | | 12.68 | 651.00 |
| | 0.17 | 639.60 | | 12.68 | 638.83 |
| +50 | | | 38 | | 35.2 |
| | 6.13 | 632.62 | | 12.51 | 626.49 |
| +95 | | | | | |
| 91+ | | | 15.2 | | 17.4 |
| | 12.99 | 645.47 | | 0.14 | 632.48 |
| +50 | | | 5.1 | | 40.4 |
| | 10.95 | 654.88 43 48 | | 1.54 | 643.93 |
| B.M. | | | 2.35 | | 652.53 |
| 92 | | | 10.4 | | 44.5 |
| +50 | | | 8.6 | | 46.9 |
| 93 | | | 6.0 | | 48.9 |
| +50 | | | 1.8 | | 53.1 |
| | 12.45 | 666.25 | | 1.08 | 653.86 |
| 94 | | | 9.9 | | 56.4 |
| +50 | | | 11.3 | | 55.0 |
| 95 | | | 3.4 | | 62.9 |
| | 12.84 | 678.87 | | 0.22 | 666.03 |
| +50 | | | 2.4 | | 76.5 |
| | 12.48 | 691.35 ✓ | | .20 | 678.67 |

"B" Line

5 ft below sta 91. - bottom gulch

Note Well tree marked incorrect of tree
On Maple tree, To Rt of sta 91+70. On upper side

# Levels

"B" Line

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 691.75 | | | | |
| | 10.62 | 701.07 | | 0.10 | 691.05 | |
| 96 | | | 7.6 | | 93.5 | |
| +49.5 | | | 2.32 | | 98.8 | H |
| +50 | | | 2.4 | | 98.7 | |
| 97 | | | 6.0 | | 95.1 | |
| +50 | | | 11.0 | | 85.1 | |
| +90 | | | | | | 3' below in Elev than Sta 98 |
| 98 | | | 23.0 | | 78.1 | |
| +50 | | | 10.6 | | 90.5 | |
| | 0.26 | 696.57 | | 3.76 | 696.31 | Checked on old B.M. at Reservoir site 696.28 |
| 99 | | | 0.3 | | 96.3 | |
| +50 | | | 5.4 | | 91.2 | |
| 100 | | | 13.0 | | 83.6 | |
| T.P. | 0.23 | 683.86 | | 12.94 | 683.63 | |
| +50 | | | 7.4 | | 76.5 | |
| T.P. | 0.11 | 670.98 | | 12.99 | 670.87 | |
| 101 | | | 0.8 | | 69.2 | |
| B.M. | | | 4.98 | | 666.01 | B.M. on Anchor post S.E. Cor. Brawns fence |
| +50 | | | 5.7 | | 65.18 | |
| 102 | | | 11.4 | | 59.6 | |
| T.P. | 0.18 | 658.59 | | 12.57 | 658.41 | |
| +50 | | | 6.3 | | 52.3 | |
| 103 | | | 18.3 | | 46.3 | |
| T.P. | 0.23 | 646.36 | | 12.46 | 646.13 | |
| | 11.03 | | | 5.32 | | |

54

| | | | | | |
|---|---|---|---|---|---|
| | | 646.26 | | | |
| 103+50 | | | 5.00 | | 41.4 |
| 104 | | | 12.0 | | 34.4 |
| T.P. | 0.58 | 634.53 | | 12.41 | 683.95 |
| +50 | | | 6.5 | | 28.0 |
| 105 | | | 11.5 | | 23.0 |
| T.P. | 0.20 | 621.83 | | 12.90 | 621.63 |
| +50 | | | 2.0 | | 19.8 |
| 106 | | | 7.6 | | 14.2 |
| +50 | | | 13.0 | | 8.8 |
| T.P. | 0.24 | 609.31 | | 12.76 | 609.07 |
| 107 | | | 8.1 | | 601.2 |
| T.P. | 0.25 | 596.97 | | 12.59 | 596.72 |
| +50 | | | 5.9 | | 90.1 |
| T.P. | 0.27 | 584.25 | | 12.99 | 583.98 |
| 108 | | | 3.0 | | 81.3 |
| +50 | | | 12.7 | | 71.6 |
| T.P. | 0.33 | 571.78 | | 12.80 | 571.45 |
| 109 | | | 8.0 | | 63.8 |
| T.P. | 0.33 | 559.37 | | 12.74 | 559.04 |
| +50 | | | 2.0 | | 57.4 |
| T.P. | 0.12 | 546.56 | | 12.93 | 546.44 |
| 110 | | | 0.6 | 10 | 45.8 |
| +50 | | | 10.7 | | 35.9 |
| T.P. | 0.19 | 534.14 | | 12.61 | 533.95 |
| | 2.51 | | | 11.73 | |

H.I = Heights of the Burr Hill tacking 1A-

| | | | | | |
|---|---|---|---|---|---|
| 55 | 63.72<br>1.39<br>62.33 | | 534.14<br>62.33<br>471.81 | | |
| | | 534.14 | | | |
| 111 | | | 7.2 | | 26.9 |
| T.P | 0.27 | 521.74 | | 12.67 | 521.47 |
| 50 | | | 3.9 | | 17.8 |
| 112 | | | 11.1 | | 10.6 |
| +50 | | | 15.1 | | 06.6 |
| 113 | | | 14.9 | | 06.8 |
| | 0.27 | 509.31 | | 12.70 | 509.04 |
| +50 | | | 1.0 | | 506.3 |
| 114 | | | 6.1 | | 503.2 |
| T.P. | 0.18 | 496.50 | | 12.99 | 496.32 |
| +50 | | | 2.8 | | 93.7 |
| 115 | | | 9.8 | | 86.7 |
| | 0.41 | 484.43 | | 12.48 | 484.02 |
| +50 | | | 2.4 | | 82.0 |
| 116 | | | 6.8 | | 77.6 |
| +50 | | | 10.1 | | 74.3 |
| 117 | | | 11.4 | | 73.6 |
| +50 | | | 10.1 | | 74.3 |
| 118 | | | 9.7 | | 74.7 |
| +50 | | | 10.6 | | 74.1 |
| 119 | | | 12.5 | | 71.9 |
| | 0.26 | 471.81 | | 12.88 | 471.55 |
| +50 | | | 3.1 | | 68.7 |
| 120 | | | 7.1 | | 64.7 |
| | 13.4 | | | 63.72 | |

56

| | | | | | |
|---|---|---|---|---|---|
| | | 471.81 | | | |
| 120 +50 | | | 12.1 | | 59.7 |
| | 0.30 | 459.67 | | 12.44 | 459.37 |
| 121 | | | 3.9 | | 55.8 |
| +50 | | | 7.9 | | 51.8 |
| 122 | | | 10.6 | | 49.1 |
| +50 | | | 11.7 | | 48.0 |
| 123 | | | 12.7 | | 47.0 |
| | 0.17 | 447.22 | | 12.62 | 447.05 |
| +50 | | | 2.7 | | 44.5 |
| 124 | | | 5.0 | | 42.2 |
| +50 | | | 7.0 | | 40.2 |
| 125 | | | 9.6 | | 37.6 |
| +50 | | | 12.5 | | 34.7 |
| | 0.37 | 434.74 | | 12.85 | 434.37 |
| 126 | | | 2.3 | | 32.4 |
| +50 | | | 3.8 | | 30.9 |
| 127 | | | 6.3 | | 28.4 |
| +50 | | | 8.6 | | 26.1 |
| 128 | | | 10.8 | | 23.9 |
| +50 | | | 12.0 | | 22.7 |
| T.P. | 1.85 | 424.24 | | 12.35 | 422.39 |
| 129 | | | 2.9 | | 21.3 |
| +50 | | | 4.4 | | 19.8 |
| 130 | | | 5.4 | | 18.8 |
| | 2.69 | | | 50.26 | |

5026
229
47,07

471.81
47.07
424.74

57

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 424.24 ✓ | | | | |
| 130 + 50 | | | 4,8 | | 19.4 | Dec 21 19.14 |
| 131 | | | 4.8 | | 19.4 | |
| + 50 | | | 5,6 | | 18.6 | |
| 132 | | | 6.1 | | 18.1 | |
| + 50 | | | 6,4 | | 17.8 | |
| 133 | | | 6.9 | | 17.3 | |
| + 50 | | | 7.3 | | 16.9 | |
| T.10 | 1.27 | 418.43 | | 7.08 | 417.16 | |
| 134 | | | 2,1 | | 16.3 | |
| + 50 | | | 2,4 | | 16.0 | |
| 135 | | | 3,1 | | 15.3 | |
| + 50 | | | 3,6 | | 14.8 | |
| 136 | | | 4.3 | | 14.1 | |
| + 50 | | | 5 25 | | 13.18 | hub |
| 137 | | | 6,00 | | 12.4 | |
| + 50 | | | 6.9 | | 11.5 | |
| 138 | | | 7.5 | | 10.9 | |
| + 50 | | | 8.5 | | 09.9 | |
| 139 | | | 17,8 | | 400.6 | |
| 139 + 50 | | | 8.9 | | 09.5 | |
| | 1.40 | 412.03 ✓ | | 7.80 | 410.63 | |
| | 2.67 | | | 14-8-8 | | |

58

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 412.03 ✓ | | | | |
| 140 | | | 11.2 | | 400.8 | Dec 22 1914 |
| +50 | | | 2.8 | | 409.2 | |
| 141 | | | 3.1 | | 08.9 | |
| +50 | | | 3.8 | | 08.2 | |
| 142 | | | 4.9 | | 07.1 | |
| | | | 5.00 | | 507.03 | B.M. set on Line at sta 142 +18 line bet |
| +50 | | | 6.1 | | 05.9 | Findlay and Westfall |
| 143 | | | 6.6 | | 05.4 | |
| +50 | | | 7.0 | | 05.0 | |
| 144 | | | 7.6 | | 04.4 | |
| +50 | | | 8.0 | | 04.0 | |
| 145 | | | 8.2 | | 03.8 | |
| T.P | 3.18 | 407.19 ✓ | | 8.02 | 404.01 | |
| +50 | | | 3.0 | | 04.2 | |
| 146 | | | 3.4 | | 03.8 | |
| +50 | | | 3.9 | | 03.3 | |
| 147 | | | 4.0 | | 03.2 | |
| +50 | | | 4.9 | | 02.3 | |
| 148 | | | 6.6 | | 00.6 | |
| +50 | | | 6.6 | | 00.6 | |
| 149 | | | 7.3 | | 399.9 | |
| +50 | | | 8.0 | | 99.2 | |
| 150 | | | 8.7 | | 98.5 | |
| +50 | | | 11.2 | | 96.0 | on dutch |

59

8.21

| | | | | | |
|---|---|---|---|---|---|
| | | 407.19 ✓ | | | |
| 151 | | | 9.0 | | 98.2 |
| | 3.87 | 402.12 | | 8.94 | 398.25 |
| +50 | | | 4.1 | | 98.0 |
| 152 | | | 4.9 | | 97.2 |
| +50 | | | 4.3 | | 97.6 |
| 153 | | | 5.5 | | 96.6 |
| +50 | | | 5.4 | | 96.7 |
| 154 | | | 5.1 | | 96.7 |
| +50 | | | 5.5 | | 96.6 |
| 155 | | | 5.8 | | 96.3 |
| +50 | | | 6.0 | | 96.1 |
| 156 | | | 6.7 | | 95.4 |
| +50 | | | 7.8 | | 95.1 |
| 157 | | | 7.9 | | 94.2 |
| | 4.54 | 395.98 ✓ | | 7.68 | 394.44 |
| +50 | | 399.0 | 5.2 | | 93.8 |
| 158 | | | 5.0 | | 94.0 |
| +50 | | | 4.0 | | 95.0 |
| 159 | | | 3.5 | | 95.5 |
| +50 | | | 4.4 | | 94.6 |
| 160 | | | 5.3 | | 93.7 |
| +50 | | | 5.6 | | 93.4 |
| 161 | | | 5.8 | | 93.2 |
| +50 | | | 5.8 | | 93.2 |
| | 8.41 | | | 16.62 | |

60

18.48
7.88
10.60

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 398.98 ✓ | | | | |
| 162 | | 399.0 | 6.6 | | 92.4 | |
| +50 | | | 5.5 | | 93.0 | |
| 163 | | | 3.1 | | 95.9 | |
| T.P. | 5.21 | 402.29 | | 1.90 | 397.08 | |
| +50 | | | 4.6 | | 97.7 | |
| 164 | | | 4.3 | | 98.0 | |
| +50 | | | 4.2 | | 98.1 | |
| 165 | | | 5.0 | | 97.3 | |
| +50 | | | 5.5 | | 96.8 | |
| 166 | | | 6.4 | | 95.9 | |
| +50 | | | 6.1 | | 96.2 | |
| 167 | | | 4.0 | | 98.3 | |
| +50 | | | 2.9 | | 99.4 | |
| 168 | | | 2.32 | | 400.0 | Hub |
| +50 | | | 3.4 | | 98.9 | |
| 169 | | | 4.6 | | 97.7 | |
| | 0.83 | 398.63 | | 4.49 | 397.80 | |
| +50 | | | 2.8 | | 95.8 | |
| 170 | | | 4.7 | | 93.9 | |
| +50 | | | 5.4 | | 93.2 | |
| 171 | | | 6.0 | | 92.6 | |
| +50 | | | 8.4 | | 90.2 | |
| 172 | | ✓ | 17.7 | | 86.9 | |
| | 1.84 | 388.38 | | 12.09 | 386.54 | |

61

| | | | | | |
|---|---|---|---|---|---|
| | | 384.38 | | | |
| 172+50 | | | 3.8 | | 84.6 |
| 173 | | | 6.3 | | 82.1 |
| +50 | | | 8.4 | | 80.0 |
| 174 | | | 9.2 | | 79.2 |
| +50 | | | 9.9 | | 78.5 |
| 175 | | | 10.3 | | 78.1 |
| +50 | | | 10.5 | | 77.9 |
| 176 | | | 10.8 | | 77.6 |
| +50 | | | 11.4 | | 77.0 |
| T.P. | 1.38 | 378.46 | | 11.30 | 377.08 |
| 177 | | | 1.8 | | 76.7 |
| +50 | | | 2.0 | | 76.5 |
| 178 | | | 2.7 | | 75.8 |
| +50 | | | 3.0 | | 75.5 |
| 179 | | | 3.6 | | 74.9 |
| +50 | | | 4.1 | | 74.4 |
| 180 | | | 5.2 | | 73.3 |
| +50 | | | 5.2 | | 73.3 |
| 181 | | | 4.9 | | 73.6 |
| +50 | | | 5.3 | | 73.2 |
| 182 | | | 5.5 | | 73.0 |
| +50 | | | 5.9 | | 72.6 |
| 183 | | | 6.1 | | 72.4 |
| | 2.97 | 376.01 | | 5.42 | 373.04 |

16 72
435
1237

62

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 376.01 | | | | |
| +50 | | | 3,8 | | 72,2 | |
| 184 | | | 4,2 | | 71,8 | |
| +50 | | | 4.2 | | 71.8 | |
| 185 | | | 4.5 | | 71.5 | |
| +50 | | | 4,7 | | 71,3 | |
| 186 | | | 4,6 | | 71.4 | |
| +50 | | | 4,8 | | 71,2 | |
| 187 | | | 5,2 | | 70.8 | |
| +50 | | | 5,0 | | 71.0 | |
| 188 | | | 5.0 | | 71.0 | |
| +50 | | | 7,2 | | 68,8 | |
| 189 | | | 4,97 | | 71,04 | Hub |
| +50 | | | 5.7 | | 70,3 | |
| 190 | | | 5,5 | | 70,5 | |
| +50 | | | 4,6 | | 71.4 | |
| 191 | | | 9.0 | | 67.0 | on west side of Poodle Creek |
| +50 | | | 5.0 | | 71 0 | |
| 192 | | | 5.32 | | 70.7 | Hub |
| +50 | | | 4,2 | | 71·8 | |
| TP, | 11,63 | 382.97 ✓ | | 4.67 | 371.34 | |
| 193 | | 3830 | 8,7 | | 74.3 | |
| +50 | | | 6,84 | | 76.2 | Hub |
| 194 | | | 6,1 | | 76.9 | |
| +50 | | | 4.3 | | 78.7 | |

63

"B line"

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 382.97 | | | | |
| 195 | | 383.0 | 3.1 | | 79.9 | |
| +50 | | | 3.2 | | 79.8 | |
| 196 | | | 4.5 | | 78.5 | |
| +50 | | | 6.0 | | 77.0 | |
| 197 | | | 7.1 | | 75.9 | |
| +50 | | | 7.6 | | 75.4 | |
| 198 | | | 8.9 | | 74.1 | |
| +50 | | | 4.4 | | 78.6 | |
| +74.3 | | | 3.61 | | 79.4 | |
| | 8.24 | 387.64 | | 3.61 | 379.36 | |
| | | | | 1.28 | 381.36 | On B.M. at S.T.C Hall Store |

379
691
749

Yoncalla Ore in Sec. 3 - 23-5
¼ Cor bet Sec. 6 + 7 - 23-4

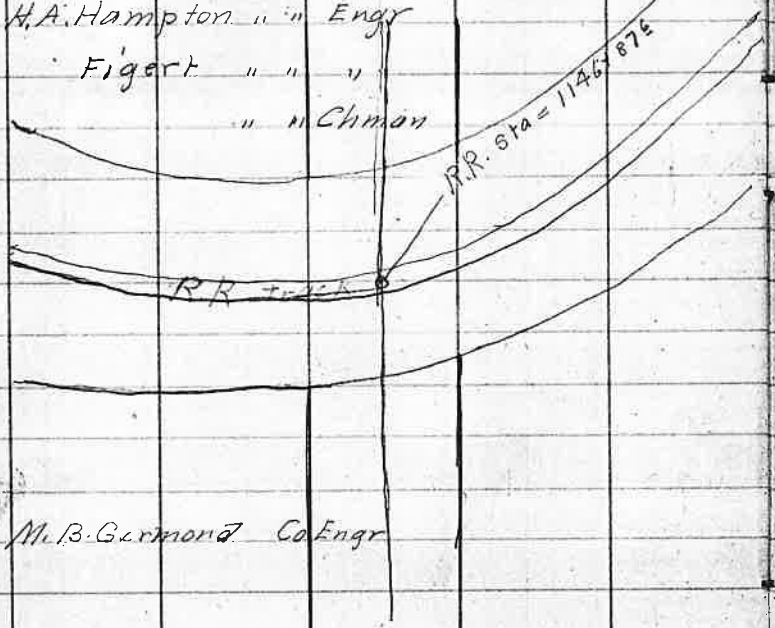
64

Sunshine & squalls - Mar 4th 1915

## Work on R.R. Xing at Myrtle Creek Ore. with R.R. Comm. Engr.

Elev. base of rail at Xing of R.R. =

H.W. Moreland R.R. Com. Engrs.
H.A. Hampton " " Engr
Figert " " "
" " Chiman




M.B. Germond Co Engr

Level readings along ℄ of Co. R.

| | | |
|---|---|---|
| 0+00 W Rail | 0.81 | = Top of lowest rail + 100 |
| 0+30 W | 5.33 | |
| 0+80 " | 8.25 | |
| 1+30 " | 11.13 | |
| 1+58.75 | 10.76 | E. End of Approach |
| 1+94± | 5.39 | ℄ of 1st pier on E Span on Finished floor |
| 0+30 E | 4.42 | |
| 0+80 | 2.07 | |

1149+09 - 4th St intersects R.R.

| W | | | | E | | |
|---|---|---|---|---|---|---|
| 45/8± | 30/14.2 | 9/20 | 0/00 | 9E/-20 | 31/14.2 | 48.0/8.4 |

65

| | | | | |
|---|---|---|---|---|
| 0+00 | | | | Gr = |
| | 25 N | W | 25 S | |
| 0+00 | | 99.9 | | 82 |
| | 93 | | 91 | |
| +30 | 7 0 | W 94.67 | 9 0 | 83.61 |
| | 92.2 | | 90.7 | |
| +80 | 7 8 | W 91.65 | 9 3 | 87 00 |
| | 89.2 | | 87.9 | |
| 1+30 | 10 8 | W 88.87 | 12 1 | 90 30 |
| 1+58 75 | | W 89.24 | | |
| 1+94 6 | | W 94.63 | | |
| 6+30 | 5 3 | E 95.6 | 6 4 | |
| +80 | (-1 0) | E 97 9 | 6 5 | |

5.30 Gives top of floor in 1st Span East

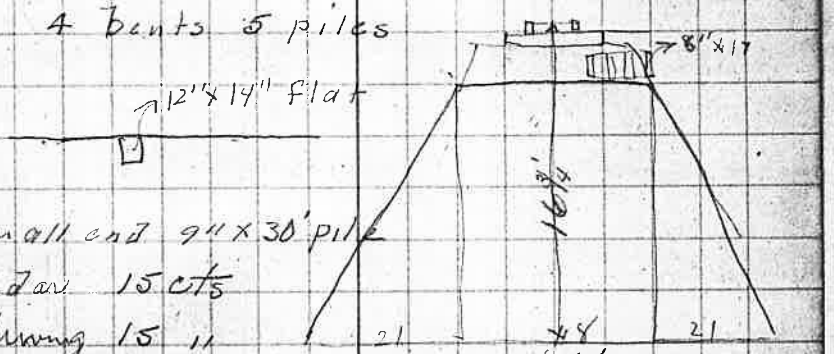
5.5 down from top of flour of Bridge to Kown H.W.

30' down from top of Bridge floor gives L.W.

47620
317
47937
124
47813

47937
112
478.25

13' 6" in clear




18'
60
178
17
546
17
382
346
2

17
20
340

46 Ties

66

Survey for Yoncalla St Pavement. Front St. Jan 28 1915

X-Section Notes from N. City Limits South

Elev. assumed. B.M. on S.P. Tele. pole S.W. of Mile-post 604. B.M. on W. side of Track

Hub. Sta. 0+00 is at intersection of ℄ of Front St and N. City Limits of Yoncalla

M. B. Germond in charge
Geo. Harshberger Chman 1/2
Jim Duniway " 1/2

Fairly clear and warm

| Sta. | East | | | | West | | | |
|---|---|---|---|---|---|---|---|---|
| | 4.39 | 380.10 / 104.39 | | | | 375.71 / 100.00 | | |
| | | | | 374.3 / 5.80 | | | | |
| - 2+00 | | | | 374.9 / 5.2 | | | | |
| - 1+50 | | | | 374.7 / 5.4 | | | | |
| - 1+00 | | | | 374.6 / 5.5 | | | | |
| - 0+50 | 374.1 / 19 6.0 | 374.6 / 14 5.3 | 375.0 / 14 5.1 | 375.2 / 10 4.9 | 375.2 / 8 4.5 | 375.5 / 4 4.6 | 374.8 / 10 5.3 | 374.2 / 15 5.9 | 375.2 / 16 4.9 |
| - 0+00 | | | | 375.72 / 4.38 | | | | |
| + 50 | 374.6 / 20 5.5 | 375.6 / 14 4.5 | 376.4 / 10 3.7 | 377.0 / 8 3.1 | 377.0 / 3.1 | 376.7 / 4 3.4 | 375.2 / 10 4.9 | 374.9 / 14 5.2 | 375.1 / 13 5.0 | 376.3 / 16 3.8 |
| 1 + 00 | 374.5 / 20 5.6 | 375.3 / 14 4.8 | 376.0 / 10 4.1 | 376.6 / 8 3.5 | 376.5 / 3.6 | 376.3 / 4 3.8 | 375.3 / 10 4.8 | 375.0 / 14 5.1 | 376.3 / 15 3.8 |
| + 50 | 374.5 / 20 5.6 | 375.1 / 14 4.7 | 376.1 / 10 4.0 | 376.7 / 7 3.4 | 376.6 / 3.5 | 376.3 / 4 3.8 | 375.2 / 10 4.9 | 374.8 / 14 5.3 | 376.0 / 15 4.1 |
| 2 + 00 | 374.2 / 20 5.9 | 375.0 / 14 5.1 | 376.1 / 10 4.1 | 376.8 / 7 3.3 | 376.4 / 3.7 | 375.1 / 4 3.7 | 375.0 / 10 5.0 | 374.4 / 14 5.1 | 376.1 / 15 4.0 |
| + 50 | 374.3 / 20 5.5 | 374.6 / 14 5.5 | 375.7 / 10 4.4 | 376.1 / 7 4.0 | 376.2 / 3.9 | 375.8 / 4 4.3 | 374.5 / 10 5.6 | 374.1 / 14 6.0 | 375.4 / 16 4.7 |
| 3 + 00 | 373.9 / 20 6.2 | 374.3 / 14 5.8 | 375.3 / 10 4.8 | 375.8 / 7 4.3 | 375.8 / 4.3 | 375.8 / 4 4.3 | 374.7 / 8 5.4 | 374.5 / 10 5.6 | 373.6 / 13 6.5 | 374.0 / 14 6.1 | 373.8 / 15 6.3 | 374.9 / 16 5.2 |
| + 50 | 373.8 / 20 6.3 | 374.4 / 19 6.1 | 374.1 / 14 6.0 | 374.3 / 10 5.8 | 375.6 / 7 4.5 | 375.4 / 4.7 | 375.4 / 4 4.7 | 374.2 / 8 5.9 | 374.1 / 10 6.0 | 374.2 / 13 5.9 | 373.3 / 14 6.8 | 374.7 / 16 5.4 |
| 4 + 00 | 373.5 / 20 6.6 | 373.5 / 19 6.6 | 374.2 / 14 5.9 | 374.9 / 10 5.2 | 375.7 / 7 4.4 | 375.8 / 4.3 | 375.5 / 4 4.3 | 374.7 / 6 5.6 | 374.7 / 9 5.4 | 374.3 / 10 5.2 | 373.4 / 12 5.8 | 375.1 / 14 5.2 | 375.2 / 16 5.2 |

## X-Sect Cont. of Front St Jan-28

| | East | | | | West | | | |
|---|---|---|---|---|---|---|---|---|
| | 73.8 74.5 | 75.0 75.4 75.9 | | | 75.8 74.9 74.6 | 74.6 74.0 73.2 74.9 | | |
| | | 164.39 | | | | 376.04 | | |
| | | 380.11 | | | | | | |
| T.P. | 407 | 104.40 | | 75.9 | 4.06 | 100.33 | | |
| 4+50 | 20/6.3 14/5.6 | 10/5.1 8/4.7 5/4.2 | | 4.2 | 5/4.3 7/5.2 10/5.5 | 12/5.2 14/6.4 15/6.9 16/5.2 | | |
| +77 | 73.8 74.2 74.5 | 74.9 75.5 76.0 | | 76.2 | 76.1 75.1 75.2 74.4 | 73.7 75.2 | | |
| 5+00 | 20/6.3 17/5.9 14/5.6 | 10/5.2 8/4.6 6/4.2 | | 3.9 | 4/4.0 7/5.0 10/4.9 13/5.7 | 14/6.9 16/4.9 | | |
| | 73.3 | 74.2 74.6 75.6 | | 75.5 | 75.3 74.2 74.1 | 74.2 74.8 | | |
| +50 | 20/6.8 | 14/5.9 10/5.5 6/4.5 | | 4.6 | 4/4.8 6/5.9 10/6.0 | 14/5.9 16/5.3 | | |
| | 73.0 | 74.0 74.6 75.5 | | 75.4 | 75.5 74.0 73.7 73.5 | 74.3 | | |
| 6+00 | 20/7.1 | 14/6.1 10/5.5 7/4.2 | | 4.7 | 4/4.9 7/6.1 10/6.4 | 14/6.6 16/5.8 | | |
| | 72.8 | 73.8 74.2 75.1 | | 75.1 | 75.2 73.8 73.4 | 73.2 74.2 | | |
| +50 | 20/7.3 | 14/6.3 10/5.9 6/5.0 | | 5.0 | 4/4.9 8/6.3 10/6.7 | 14/6.9 16/5.9 | | |
| | 72.6 | 73.6 73.9 74.9 | | 74.9 | 74.8 73.7 73.5 | 73.0 74.1 | | |
| 7+00 | 20/7.5 | 14/6.5 10/6.2 6/5.2 | | 5.2 | 4/5.8 8/6.4 10/6.6 | 14/7.1 17/6.0 | | |
| | 72.5 | 72.9 73.7 74.7 | | 74.5 | 74.5 73.6 73.3 | 72.8 73.8 | | |
| +50 | 20/7.6 14/7.2 | 10/6.4 6/5.4 | | 5.6 | 4/5.2 8/6.5 10/6.8 | 14/7.3 17/6.3 | | |
| +84 | 72.7 72.9 | 73.3 73.6 74.8 | | 74.9 | 74.9 73.6 73.1 | 72.9 73.2 | | |
| 8+00 | 20/7.4 14/7.2 | 10/6.8 8/6.5 5/5.3 | | 5.2 | 4/5.2 7/6.5 10/7.0 | 14/7.2 17/6.9 | | |
| | 72.6 72.9 | 73.2 73.5 75.4 | | 75.3 | 75.0 74.7 74.1 | 73.4 73.6 | | |
| +23 | 20/7.5 14/7.2 | 10/6.9 8/6.6 5/4.7 | | 4.8 | 6/5.1 8/5.4 10/6.0 | 14/6.7 17/6.5 | | |
| | 72.8 73.0 | 73.5 73.7 75.3 | | 75.5 | 75.4 75.3 75.2 75.0 74.6 | | | |
| +35 18 | 20/7.3 14/7.1 | 10/6.6 8/6.4 5/4.8 | | 4.6 | 6/4.7 10/4.8 14/4.9 20/5.1 25/5.5 | | | |
| | 73.0 | 73.1 73.8 75.5 | | 75.7 | 75.6 75.4 75.2 | 74.5 | | |
| +44 18 | 20/7.1 | 14/7.0 10/6.3 4/4.6 | | 4.4 | 14/4.5 14/4.7 18/4.9 25/5.6 | | | |
| | 73.1 | 73.2 73.8 75.5 | | 75.7 | 75.5 74.8 | 74.4 74.4 | | |
| 8+50 18 | 20/7.0 14/6.9 | 14/6.3 5/4.4 | | 4.42 | 10/4.6 14/5.3 | 18/5.7 25/5.7 | | |

Wood
Large Culvert across ST.

Wood
Large Culvert

N. Prop Line of 1st St.

Note error in width of pavement in 1+21 St. It should be 18' instead of 12'.

37

376.04
3.17
379.21
7.09
372.12

68

E

X-Sect of Front St. Cont.

W

| | | |

X-Sect of Front ST Cont.

Jan 29 '15

| | | East | | West | | |
|---|---|---|---|---|---|---|
| | 79.7 79.7 79.7 | | 79.7 | 79.5 79.2 | | |
| | 11.68 | 389.41 | | | 377.73 | |
| 0 + 00 | 25/9.7 19/9.7 15/9.7 | | 9.7 | 15/9.9 19/10.2 | | S. Prop Line of 2nd ST |
| | 80.7 | 80.5 80.5 | 80.3 | 80.0 79.9 | 80.4 | |
| 0 + 50 | 25/8.7 19/8.9 15/8.9 | | 9.1 | 15/9.4 19/9.5 | 25/9.0 | Cold in A.M. |
| | 81.3 | 81.5 81.6 | 81.4 | 81.9 82.0 | 82.1 | Warm & Clear P.M. |
| 1 + 00 | 25/8.1 19/7.9 15/7.8 | | 8.0 | 15/8.0 19/7.4 | 25/7.3 | |
| | 84.9 83.4 | 82.8 83.0 | 83.4 | 83.5 84.8 | 86.9 87.3 | Gemmond 8 hrs |
| + 50 | 25/5.0 19/6.2 15/6.4 | | 6.0 | 17/5.9 15/7.4 19/3.0 | 25/2.1 | Hanish Berger 7 " |
| | 86.8 85.6 | 85.5 85.7 | 85.8 | 85.7 87.5 | 89.2 89.1 | Duniway 5 " |
| 2 + 00 | 25/2.6 21/3.4 | 19/3.9 15/3.7 | 3.6 | 17/3.7 15/1.9 | 19/0.4 25/0.3 | |
| | 87.0 86.3 | 86.2 86.4 | 86.6 | 86.5 88.3 | 89.9 89.9 | |
| + 50 | 25/2.4 22/3.1 | 19/3.2 15/3.0 | 2.8 | 17/2.9 15/1.1 | 19/-0.5 25/-0.3 | |
| | 82.3 86.3 85.7 | 85.7 85.7 | 86.6 | 87.7 88.2 | 89.2 90.4 | |
| 3 + 01.7 | 25/3.3 22/3.1 24/3.7 | 19/3.7 15/3.7 | 2.70 | 17/1.7 15/1.2 | 19/-0.2 25/-1.0 | N Prop of Ap Ave |
| | 85.3 84.5 | 84.3 84.4 | 85.9 | 89.3 90.1 | 90.2 | |
| + 29.7 | 25/4.1 23/4.9 | 19/5.1 15/5.0 | 3.5 | 13/0.1 19/0.7 | 25/0.8 | N Curb " " " |
| | 84.9 83.7 83.6 | 83.7 84.4 | 85.3 | 87.7 89.0 | 90.1 90.3 | |
| 3 + 41.7 = 9+00 | 25/4.7 21/5.7 19/5.8 | 15/5.1 10/5.2 | 4.1 | 10/1.7 15/0.4 | 19/-0.7 25/-0.9 | Cen " " " |
| | 83.8 83.3 | 83.1 83.5 | 84.4 | 87.1 88.8 | 89.4 89.4 | |
| 6 + 12.0 | 25/5.6 20/6.1 | 14/6.1 10/5.4 | 5.0 | 10/3.3 15/0.6 | 19/0.0 25/0.0 | S Curb " " " |
| | 81.9 | 81.7 81.7 | 81.7 | 84.4 86.1 | 87.0 88.3 | |
| 9 + 40.0 | level 20/7.5 | 14/7.7 10/7.7 | 7.7 | 10/5.0 14/3.3 | 16/2.4 25/1.1 | S Prop Line of Ap Ave |
| | 79.0 | 79.1 80.3 | 80.4 | 79.9 80.4 | 81.9 83.5 84.6 | |
| 9 + 90 | level 20/10.4 | 14/10.3 10/9.1 | 9.0 | 10/9.5 12/9.0 | 14/7.5 16/8.8 25/7.0 | |

70

X-Sect of Front ST. Cont

Jan 29 '15

| | | |

71

# X-Sect. Front St. (Cont.)

Jan 29

| | | | | | |
|---|---|---|---|---|---|
| 2 + 30 | 75.5 75.5 75.8 77.0 | 77.3 | 77.3 75.8 75.5 7.55 76.2 | level | |
| | 20/7.1 14/7.1 10/6.8 7/5.6 | 5.3 | 3/5.3 6/6.8 10/7.1 14/7.2 15/6.4 | | |
| | 75.1 75.1 75.4 76.6 76.6 | | 76.5 75.8 75.5 75.4 75.2 | | |
| + 80 | 20/7.2 14/7.5 10/7.2 7/6.6 | 6.0 | 4/6.1 7/6.6 10/7.1 14/7.2 18/7.4 | " | |
| | 74.8 74.9 75.1 | 75.6 | 75.5 75.2 75.2 74.6 | | |
| 3 + 31 | 20/7.8 14/7.7 10/7.5 | 7.0 | 5/7.1 10/7.4 4/7.4 19/8.0 | | IV. Prop Line of 4th ST |
| | 75.2 74.8 74.8 | 75.4 | 75.5 75.4 75.6 74.5 74.9 | | |
| + 51 | 25/7.4 15/7.8 10/7.8 | 7.2 | 10/7.1 14/7.2 18/7.1 20/5.3 25/8.4 | | W Curb " " " " |

+ 61
= 0 + 00 Sta. Comes on bridge. Use same sec. as 3+51

Sta 3+61 or 0+00 is S. City Limits. also ℄ of 4th ST, also N. Line Wises Add. also ℄ of RR Cul. 2'

7.51 375.06 Check on old B.M. on W. end of RR Cul.

9.58 373.00 = Bot elev. of R.R. Cul. 2' dia. Corru. Iron

℄ of Front ST =

Bearing of ^ = N 6° 00' W

72

| | East | | | West | | | | |
|---|---|---|---|---|---|---|---|---|
| X-Sect. of County Road | | | | S. of S. City Limits of Yoncalla, Or. | | | Front St. extended South | |
| | 57+ | 380 | 74 | | | 375.00 | | |
| 0+00 | | | | | | | 375.8 | ℄ of 4th Street |
| | 394.7 | 373.2 | 374.6 | 375.0 | 374.7 | 374.5 | 374.9 | 374.9 |
| +10 | 25/6.0 | 14/7.1 | 14/6.1 | 10/5.7 | 6.0 | 10/6.2 | 14/5.8 | 25/5.8 |
| | | 736 | 739 | 745 | 375.0 | 749 | 751 | 74.2 |
| +30 | | 20/7.1 | 12/6.8 | 8/6.2 | 5.7 | 8/5.8 | 12/5.6 | 20/6.5 |
| | | 735 | 735 | 738 | 740 | 74.1 | 748 | 749 |
| +80 | | 20/7.2 | 12/7.2 | 12/6.9 | 8/6.1 | 6.9 | 8/5.9 | 12/5.8 |
| | | 737 | 734 | 745 | 758 | 75.4 | 754 | 753 |
| 1+30 | | 20/7.0 | 12/6.6 | 8/6.2 | 20/5.4 | 5.3 | 8/5.3 | 12/5.4 |
| | | 736 | 741 | 744 | 749 | 75.4 | 751 | 754 |
| +80 | | 20/7.1 | 12/6.6 | 8/6.3 | 4/5.8 | 5.3 | 8/5.6 | 12/5.3 |
| | | 739 | 743 | 746 | 750 | 75.4 | 754 | 752 |
| 2+30 | | 20/6.8 | 12/6.4 | 8/6.1 | 5/5.7 | 5.3 | 8/5.3 | 12/5.2 |
| | | 739 | 742 | 748 | | 759 | 758 | 75.4 |
| +80 | | 20/6.8 | 12/6.5 | 8/5.9 | | 4.8 | 8/4.9 | 12/5.3 |
| 3+30 | | 20/6.7 | 12/6.2 | 8/5.8 | | 4.8 | 8/4.9 | 12/5.2 |
| +80 | | 20/6.5 | 12/6.3 | 8/5.8 | | 4.9 | 8/4.5 | 12/5.2 |
| 4+30 | | 20/6.3 | 12/6.1 | 8/5.8 | | 4.9 | 8/4.6 | 12/5.0 |
| +80 | | 20/6.1 | 12/5.9 | 8/5.6 | | 4.9 | 8/4.8 | 12/5.0 |

Jan 29 '15

S. Prop Line of 4th ST

3763

37661

3766

37692

37723

7772

37754

37785

3778

3730 = N prop. Line of 30' ST on S. side of Wise's Add.

37816

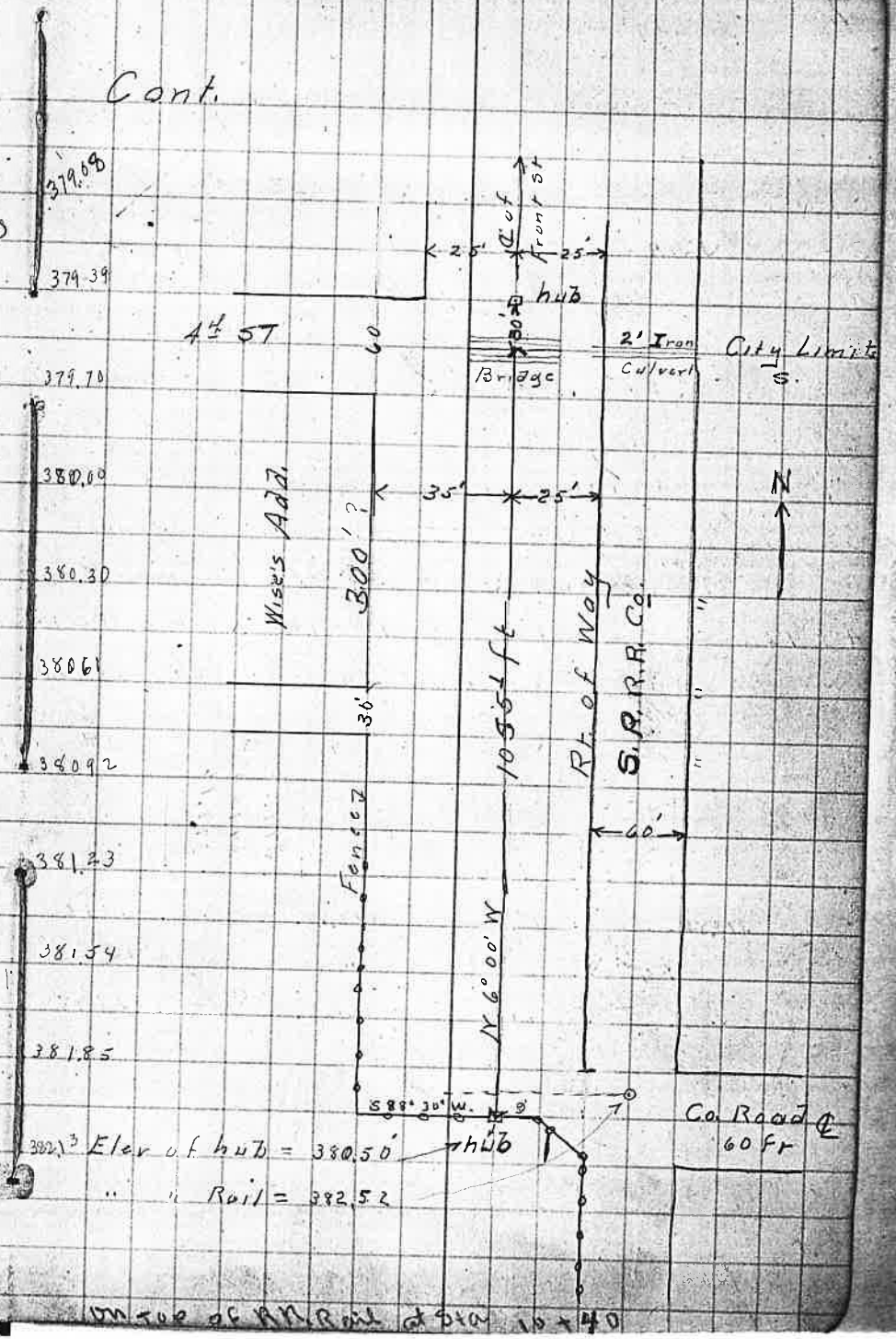
37847

37878

73

# X-Sect of County Road Cont.

| | East | | | | West | | | |
|---|---|---|---|---|---|---|---|---|
| 5+30 | 20/5.8 | 12/5.7 | 8/5.2 | 4.6 | 8/4.4 | 12/4.8 | 20/5.6 | 379.69 |
| T.P | 7.60 | 383.50 | | | 4.54 | 375.90 | | |
| +80 | 20/6.2 | 12/6.0 | 8/5.5 | 0.9 | 8/6.9 | 12/6.9 | 20/7.9 | 379.39 |
| 6+30 | 20/7.- | 12/7.3 | 8/6.8 | 6.1 | 8/6.0 | 12/6.5 | 20/7.2 | 379.70 |
| +80 | 20/7.0 | 12/6.4 | 8/6.2 | 5.5 | 8/5.4 | 12/5.4 | 20/6.3 | 380.00 |
| 7+30 | 20/6.2 | 12/5.8 | 8/5.7 | 5.4 | 8/5.3 | 12/5.3 | 20/6.0 | 380.30 |
| +80 | 20/5.2 | 12/5.1 | 8/5.1 | 4.6 | 8/4.6 | 12/4.8 | 20/5.2 | 380.61 |
| 8+30 | 20/5.0 | 12/4.6 | 8/4.2 | 4.1 | 8/4.0 | 12/4.1 | 20/5.0 | 380.92 |
| | 79.1 | 78.7 | 79.1 | 79.1 | 379.4 | 79.4 | 79.4 | 78.9 |
| +80 | 20/4.1 | 19/4.8 | 12/4.4 | 8/4.3 | 4.1 | 8/4.1 | 12/4.1 | 20/4.6 |
| 9+30 | 20/4.1 | 19/4.8 | 12/4.3 | 8/4.2 | 3.9 | 8/3.9 | 12/4.2 | 20/4.8 |
| | 79.1 | 78.9 | 79.2 | 79.4 | 79.1 | 79.6 | 79.6 | 78.9 |
| +80 | 20/4.4 | 19/4.6 | 12/4.3 | 8/4.1 | 3.8 | 8/3.9 | 12/3.9 | 20/4.6 |
| 10+25 | 50/2.1 | 42/2.4 | 30/3.0 | 33/3.8 | 20/3.9 | 12/3.6 | 8/3.4 | 3.3 |
| +40 | 50/1.- | 36/2.2 | 30/3.0 | 20/3.4 | 12/3.0 | 8/3.4 | | 3.9 |
| 10+95 | 50/1.8 | 42/2.1 | 30/3.0 | 20/2.9 | 12/3.- | | | 3.00 |




Top of RR Rail at Sta 10+40

79

Field Notes Honcalla Pavement on Front St Jan 29 1915

0+00 2 Ft opening at ℄ of 4th St — Concrete or iron
3+31 hub — On N. Prop Line of 4th Street
0+22 1' or 16" opening " pt 22' South of ℄ of 3rd St — Concrete or iron
3+01.7 hub — On N. Prop. Line " Ap. Ave
Note: Soft Rock at Apple Ave.
0+00 Rock Mon. Center of 2nd St
0+00 Old hub " " 1st " . Also some — sta is opposite of R.R. Con. Culvert 30" dia.
0+25 N. of ℄ of 1st St, put in 18" or 2' opening — Elev of Bottom of Culvert is ft
1' opening X 16+ ST to Connect — with opening X Front at sta 0+25
4+77 2' or 30" opening at this sta meas — uring S from N. City Limits. This sta is also
opposite of a 18" x 24" rock Masonry Culvert in the R.R. track. Elev of Bottom of R.R. Cul. = 372.36




375.86 375.86 378.46 378.98 384.46 386.46 380.46 379.25 476.05
375.40
" " " 378.52 384.00 386.00 380.00 379.00 475.80
" " " 378.98 384.46 386.46 380.46 379.25 476.05

373.92
1.42
372.50

Note:— These Gr. points are prop Grade points

C 1.42

373.60
372.70
2.90

376.01
372.70
3.31

375.60
374.60
1.75
372.85
.31
.47

372.26
.31
.69

75

Estimate on proposed Co. R. Improvement
Extending S. from S. City Limits Yoncolla

| | | | |
|---|---|---|---|
| Sq yds of pavement | 1927.1 | @ $1.25 | = $2408.88 |
| " " " gravel | 481.8 | @ .30 | = 144.54 |
| Earth approx ydage | 15000 | @ .25 | = 3750.00 |
| | | Total | $2928.42 |

Mutual Life of N. York
34 yrs
20 pay Life
37.56 on a thousand 3 00 = $112.68
1st cash dividend (annual) $18.63
2nd " " " $21.63

Feb 14 '15 Notes for County Court

Speak about extra Culvert pipe 105+25
" " extra moving of dirt
at Sta. 106+05, 104+00, 101+25,
97+00,
Send out last estimate
About widening of Road

76

Tp 23-4

S 89° 47' E bet 6 & 7

30.30 stream 12 lks wide

39.48 set qr sec post

a fir 30" dia N 47° W 21 lks

" " 18 " S 5° E 18 "

79.48 to Sec Cor.

West on S. bdy of Sec 31 T 22-4

40.00 set qr post

a W Oak 16" dia. N 20° 30' W 10.38

a " " 18 " S 13 00 W 10.07

78.00 Road to Will. to Calif.

80.00 Set post

Cu alder 12" dia S 13 3/4 E 7.45

" " 9 " S 16 1/2 W 7.25

W. Oak 14 " N 80 W 16.53

South on random line on W line of T 22-4

at 5 miles 79.50 chs. intersect 5th Stand Parallel

4.59 lks west of Stand Corner and set post Sec 31 & 36

Cu W Oak 20" dia brs. N 21° W. 10.01

" W " 12" " " N 4° E 14.43

Stand Parallel S

W Oak 12 brs S 2½ W 49

Sec Cor for Secs 5, 6, 7 & 8 23-4

a fir 36" S 50° E 29

" " 10 S 37° W 32

" " 10 N 40° W 26

" " 6 N 17 E 28

bet 7 & 8 23-4

post 4" sq

a fir 30" S 36° E 17 lks

" " 36 S 74° W 42 "

bet 7 & 18 — 23-4

post 4"

a fir 6" S 66° W 16 lks

" " 40 N 35 W 120 "

7-8-17-18 — 23-4

post 6"

a fir 40" N 16° W 75 lks

" " 70" S 34° E 87 "

" " 10 N 78 E 28 "

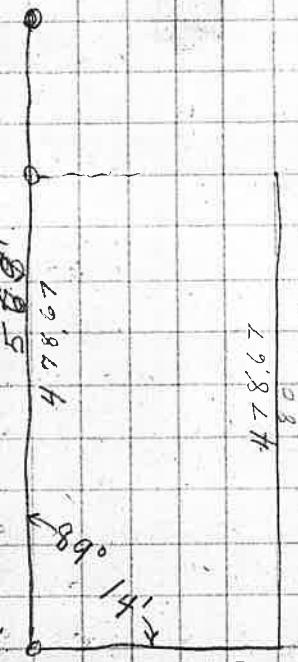
" " 5 S 43° W 13 "

77

Curve Notes on Resurvey of Spring ST Nov 16

| | | | | |
|---|---|---|---|---|
| 2+88 | 00° 15' 02.5" | 6+39 | 00° 13' 34" | 10+45 |
| 3+00 | 3° 33' 45" | +50 | 00° 46' 04" | +70 |
| +23 | 1° 07' 30" | +75 | 1° 18' 34" | +93 |
| +36 | 1° 41' 15" | 7+00 | 1° 51' 04" | 11+20 |
| +63 | 2° 15' 00" | +25 | 2° 23' 34" | +45 |
| +88 | 2° 48' 45" | +50 | 2° 56' 04" | +70 |
| 4+13 | 3° 22' 30" | +75 | 3° 28' 34" | +95 |
| +38 | 3° 56' 15" | 8+00 | 4° 01' 04" | 12+20 |
| +63 | 4° 30' 00" | +25 | 4° 26' 44" | +45 |
| +88 | 5° 05' 15" | +44.73 | | +70 |
| 5+14.97 | | | | +84.66 |

| | |
|---|---|
| 37.18 | |
| 3 21 48 | |
| 4 49 18 | |
| C-24-48 | |
| 8 04-18 | |
| 9 51 48 | |
| 11 19 18 | |
| 12-56-48 | |
| 14 34-18 | |
| 15 [illegible] 30 | |




165) 569 (34
495
740

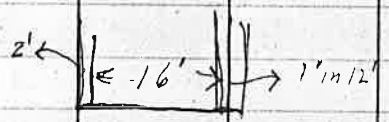
43560
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569) 7405 20 (130.1
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820

357
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2) 1126
563

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862
563
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281
176
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357
533
569
1122
561
74052
361
1795
1683
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1121
100

78




15000, 5700, 1, 100, 1X

15000 / 5700 00 / 45 44 / 120000 / 114000 / 6000

15000 / 10 = 1500 / 1500 = 800 / 11 / 700

758 / 88 / 670

880,00

375 / 320 / 473 / 975 / 975 / 1300 / 140.6 2.5

3260,4 / 1963 / 3456,7

3260,4 / 2775,7 / 484,7

43560 / 15 / 21780 / 217.81

3.72 / 3.5 / 37

96 / 26

600 700 800

10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25

79

JH 25025

Qualtanio Municipal Court

270

37560
37250
310

373.92
372.50
1.42

1.68
142
310
270
40

1
175
270

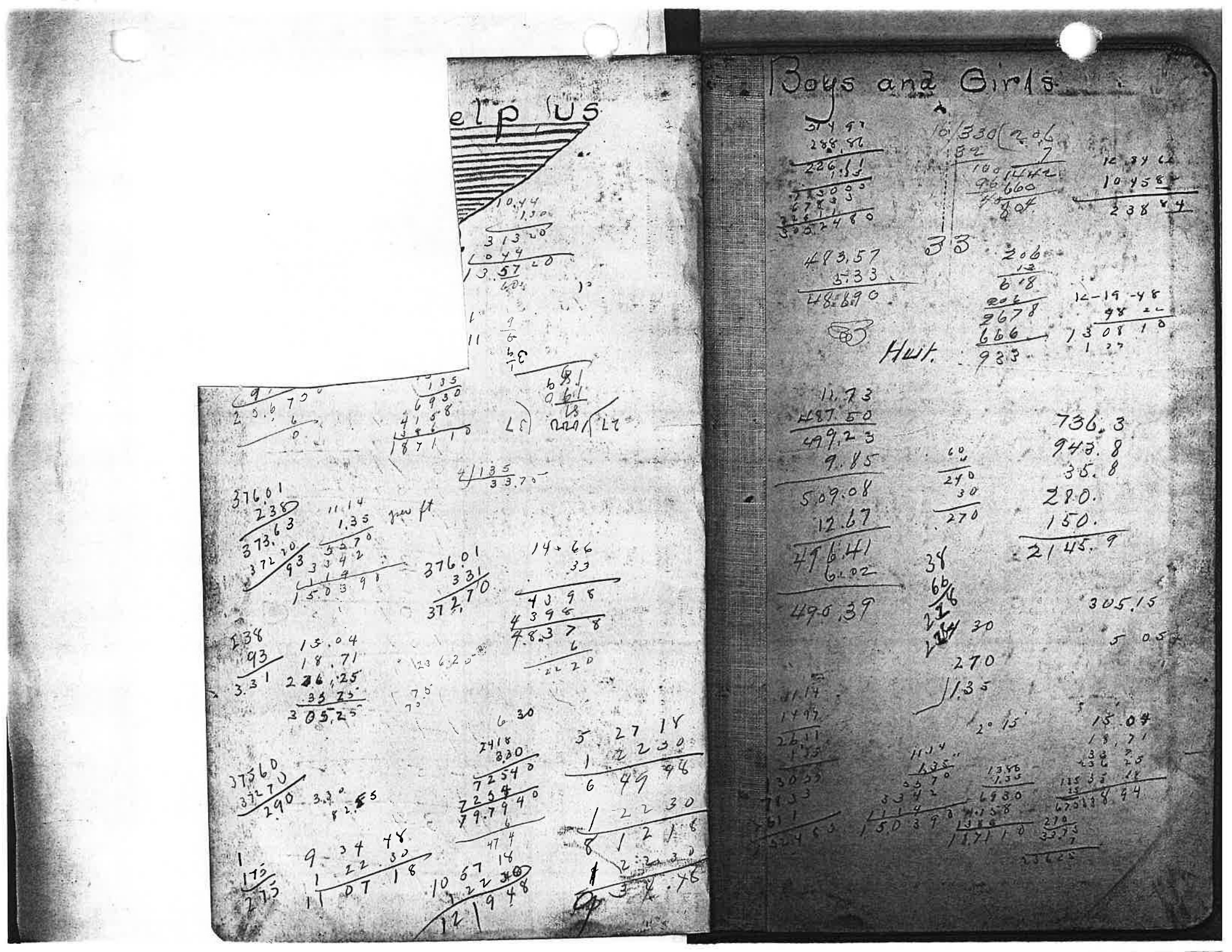
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758
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678

94.5

1 34 48
1 37 30
3 21 48
1 37 30
4 49 18
1 37 30
6 26 48
1 37 30
8 04 18
1 37 30
9 41 48
1 37 30
10 29 18
1 37 30
12 56 48
1 37 30
14 34 18
07 10
1531 28


elp us
Boys and Girls
Hwt.