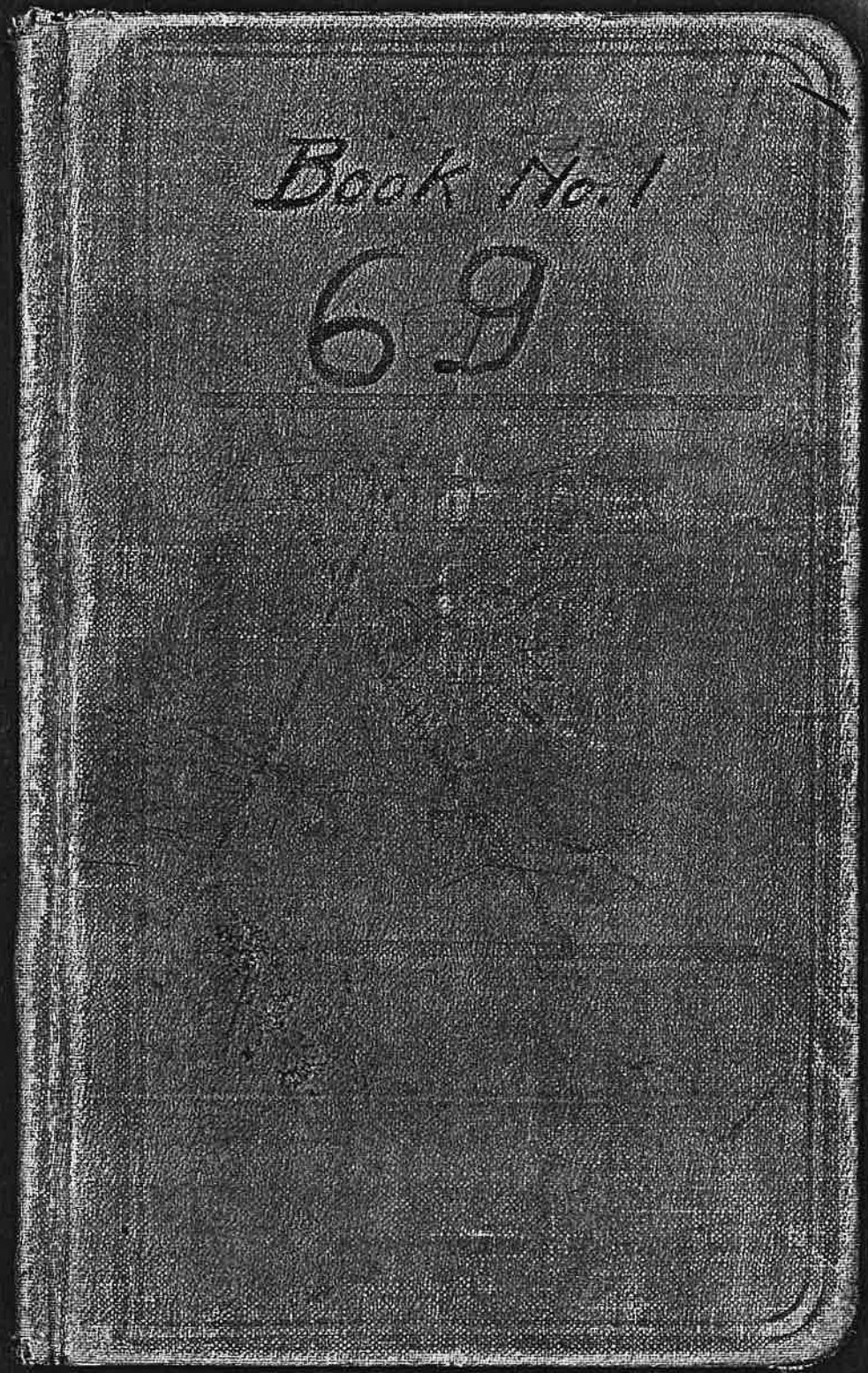
Field Book #69


Book No. 1
69

1111

1250
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1320

HANNA BLUE PRINT PAPER CO.
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SEATTLE, WASH.

Indexed Complete

Index of Transit Notes

Sta.	to	Sta.	Page
76+97.6	—	80+50	22
80+50	—	82+36.9	23
82+36.9	—	84+50.6	24
84+50.6	—	87+00	25
87+00	—	90+50	26
60+51.6	—	64+00	27
64+00	—	76+97.6	28 to 32
0+00	—	60+51.6	33 to 49

Sta.	to	Sta	Page to Page
0+00	to	60+51.6	33 to 49
60+51.6	to	76+97.6	27 to 32
76+97.6	to	90+50	22 to 26

Cross-section of Canyon Creek Road

Sta	E	G	C	F	L	R	-
0+00	1166.30	1166.30					
+50	1171.3	1168.4	2.9				
+98.5	1172.41	1170.5	1.9				
1+50	1175.70	1172.60	3.10				
1+70.3	1177.7	1174.9	2.8				
P	1185.5	1174.7	10.8				
P+50	1185.4	1176.80	8.6				
3	1183.1	1178.9	4.2				
+50	1183.1	1181.00	2.1				
4	1185.66	1183.10	2.5				
+50	1184.56	1185.20		0.8			
+75 ⊗	1186.16	1186.30					
	1187.37			(0.0)			
5	1184.66	1187.37		2.71			
	1189.62			(0.0)			
+50	1185.46	1189.62		4.16			
	1191.87			(0.0)			
6	1186.16	1191.87		5.71			
	1194.12			(0.0)			
+50	1188.26	1194.12		5.86			
	1196.37			(0.0)			
7	1188.77	1196.37		7.60			
	1198.62			(0.0)			
+50	1193.47	1198.62		5.15			
	1203.38						
8	1199.18	1200.87	(2.4)	1.69			
+50	1201.62	1203.12		1.50			
	1207.62						
9	1204.92	1205.37	(2.3)	.45			
+50	1204.74	1207.62		2.88			
	1207.97			(1.9)			
10	1202.72	1209.87		7.15			
	1212.17			0.0			
+50	1208.2	1212.12		3.9			

L			R		
			1/1	+5.4	
				13.4	
0.0			3½/1	+17.5	
3.0				21.2	
0.0			3½/1	26.8	
2.2				28.0	
0.0			3½/1	21.0	
2.0				23.7	
0.0				15.3	
4.0				19.5	
0.0				12.5	
11.0				3.2	
0.0				2.2	
5.0				13.5	
0.0				18.2	
5.0				17.1	
0.0				12.1	
4.0				14.1	
0.0				6.2	
4.5	+	69 (73.51)		11.1	+ 38.75 (43.0)
			0.0	4.4	
	+	49.1 (53.06)	5	10.2	14.8
				6.0	
	+	177		17.0	+ 24.6
				6.8	
	+	237		11.4	+ 27.2
				5.7	
	+	462		10.8	+ 22.8
				4.8	
	+	38.8		10.4	+ 19.2
				4.0	
	+	32.5		10.0	+ 16.8
				3.9	
	+	29.2		9.0	+ 15.6
				4.0	
	+	29.2		10.0	+ 16.0
0.0				5.7	
8.0	+	57.0		10.8	+ 45.6
				2.4	
	+	5.1 (4.268)		9.2	+ 9.6 (5.0)
				4.5	
1.0				10.2	
8.5	+	49.1 (53.1)		1.7	+ 43.5
				8.8	
	+	46.5 (49.21)		2.6	+ 6.8 (2.0)
			0.0	9.3	
	(762)	12.03	8.2	7.7	+ 6.24
	+	3.425		11.8	+ 30.8

C.Yds (-24.07)

(-3333)

(-5277)

(-3888)

C.Yds

End Area

Sta	E	G	C	F
	1214.37			(0.0)
11	1214.09	1214.37		0.28
+ 50	1217.09	1216.62	0.47	
	1218.87			(0.6)
12	1217.17	1218.87		1.70
	1221.12			(0.0)
+ 50	1218.40	1221.12		2.72
	1223.37			(0.0)
13	1220.50	1223.37		2.87
	1224.62			(0.9)
+ 50	1222.00	1225.62		3.62
14	1228.99	1227.87	(1.1)	5.37
+ 50	1230.12	1230.12		(0.0) 5.83
15	1232.37	1232.37		(0.0) 3.15
+ 50	1234.52	1234.62		0.10
16	1234.72	1236.87		2.2
+ 50	1239.22	1239.12	0.10	
17	1238.95	1241.37		3.42
+ 50	1241.75	1243.62		1.87
18	1243.55	1245.87		2.32
+ 50	1248.16	1248.12	0.04	
19+00.8	1252.16	1250.37	1.79°	
+ 50	1250.87	1252.62		2.35
20	1250.37	1254.87		4.50
+ 50	1258.27	1257.12	1.15	
21	1258.47	1259.37		0.90
+ 50	1262.30	1261.62	(0.7)	0.93
22	1263.87	1263.87		(0.0) 2.88
+ 50	1266.12	1266.12		(0.0) 4.13
23	1268.37	1268.37		(0.0) 4.00

C.Yds (-52.77)

(-60.18)

(4679)

-(52.77)

-(6481)

-(67.59)

-(80.55)

L

00/20

00/1.5

C.Yds	R	End Area
	+ 9.0	
6185	12.5	+ 36.0
	+ 8.7	
6555	12.3	+ 34.8
	+ 9.4	
6703	12.7	+ 37.6
	+ 7.2	
6148	11.6	+ 28.8
	+ 6.8	
5185	11.4	+ 27.2
	-0.0+ 7.3	
4546	2.0 11.6	+ 21.9
	+ 4.9	
4296	10.2	+ 24.5
	+ 8.2	
5379	12.2	+ 33.1
	+ 7.7	
5962	11.8	+ 30.8
	+ 8.5	
6000	12.2	+ 34.0
	+ 9.7	
6740 (56.18)	12.8	+ 388 (27.0)
	+ 8.3	
6666 (55.74)	12.1	+ 332
	+ 2.7	
4074 (35.37)	9.3	+ 108 (5.0)
	+ 9.2	
4+07 (29.67)	12.6	+ 36.8
	+ 9.8	
7037 (49.07)	12.9	+ 37.2 (26.0)
	+ 7.8	
6518 (84.42)	11.9	+ 31.2
	+ 11.6	
7185 83.51)	13.8	+ 464 (59.0)
	+ 13.0	
9111 (90.74)	14.5	+ 520 (39.0)
	+ 2.1	
5592 (38.80)	9.1	+ 84 (3.0)
	+ 13.0	
6495 (59.95)	14.5	+ 61.75
	+ 10.1	
9425	13.1	+ 40.0
	+ 8.5	
6855	12.2	+ 34.0
	+ 9.2	
6555	12.6	+ 36.8
	+ 8.1	
6407	12.1	+ 32.4
	+ 7.8	
5888	11.9	+ 31.2

Sta	E	G	C	F
+ 50	1271.02	1270.62	0.40	
24	1275.02	1272.87	2.15	
+ 50	1278.63	1275.12	3.51	
25 + 02	1271.23	1277.37		6.14
+ 50	1282.23	1279.62	2.61	
26	1284.39	1281.87	2.52	
+ 50	1286.19	1284.57	1.62	
27	1288.49	1287.27	1.22	
+ 50	1295.17	1289.97	5.20	
27 + 75	1297.57	1294.07	6.30	
28	1297.07	1292.67	4.40	
+ 50	1297.01	1295.37	1.64	
29	1297.81	1298.07		0.26
+ 50	1300.17	1300.77		0.66
30	1301.89	1303.47		1.58
+ 20			0.5	
+ 50	1304.20	1305.87		1.67
+ 83	1311.62	1307.07	3.5	
31	1313.07	1308.27	4.80	
+ 50	1312.57	1310.67	1.90	
32	1313.28	1313.07	0.2	
+ 50	1315.68	1315.47	0.21	
33	1318.18	1317.87	0.3	
+ 50	1318.98	1320.27		1.29
34	1322.54	1322.67		.13
+ 50	1326.04	1325.07	.97	
35	1329.24	1327.47	1.77	



{112.87
112.87}

-(60.18)

-(26.66)

(43.5)

L	C.Yds.	R		
		+ 5.1		
	47.77	10.6	+	20.4
		+ 9.7		
	54.81 (73.51)	12.8	+	38.8 (59.0)
+00		+ 7.1		
7.5	86.87 (105.55)	11.6	+	55.02
−11.3	+ 50	−0.8		
18.3	− 50.94	7.8	−	12.1.9
+00		+8.6		
5.5	+ 53.75	12.3	+	58.05
		+9.6		
	89.30 (103.74)	12.8	+	38.4 (54.0)
		+8.8		
	68.14 (93.51)	12.4	+	35.7 (47.0)
		+8.9		
	65.55 (83.33)	12.4	+	35.6 (43.0)
00		+12.5		
7.3	121.48 (128.33)	14.2	+	95.6
+1.6		+14.9		
8.8	109.07	15.2	+	140.0
+00	110.55	15.5	+	198.8
8.8		+11.8		
+ 0.0	146.11	13.9	+	59.0
2.0		+10.6		
	93.88	13.3	+	42.1
		+9.0		
	72.59	12.5	+	36.0 *
		+18.2		
	100.74 (91.66)	17.1	+	72.8 (63.0)
		+18.0		
	53.62 (43.19)	17.0	+	72.0
		+7.2		
	56.00 (52.77)	11.6	+	28.8 (23.0)
+0.0	56.71 (56.83)	+9.6 12.8	+	64.0 (74.0)
5.5	48.16 (50.0)	+4.9 13.7	+	89.0
+0.0		+9.7		
6.4	131.80	12.8	+	53.35
+00		+8.0		
3.0	79.02	12.0	+	33.0
		+9.5		
	64.81	13.7	+	38.0
		+10.0		
	72.22	13.0	+	40.0
		+7.8		
	65.92 (57.4)	11.9	+	31.2 (22.0
		+9.6		
	64.44 (55.92)	12.8	+	38.4
		+9.8		
	71.85 (81.85)	12.9	+	39.2 (50.0)
+00		+11.5		
2.0	89.53 (99.53)	13.7	+	57.6

Sta	E	G	C	F
+50	1330.14	1329.87	.24	
36	1331.54	1332.27		.73
+50	1333.94	1334.67		.73
37	1337.89	1337.07	.82	
+50	1340.88	1339.47	1.41	
38	1341.49	1341.87		.38
+50	1346.92	1344.27	2.65	
39	1346.42	1346.67		.25
+50	1345.36	1349.07		3.71
40	1349.96	1351.47		1.51
+50	1355.28	1353.87	1.41	
41	1355.88	1356.27		.39
+50	1347.98	1358.67		10.69
42	1359.71	1361.07		1.36
+50	1367.32	1363.47	3.85	
43	1366.62	1365.87	.75	
+50	1369.82	1368.27	1.55	
44	1374.47	1370.67	3.80	
+50	1374.77	1373.05	1.72	
45	1372.57	1375.47		2.90
+50	1375.95	1377.87		1.92
46	1386.95	1380.27	6.68	
+20	1389.80	1381.27	8.5	
+50	1384.60	1382.67	6.9	
+72				
47	1378.50	1385.07		6.6
+20	1385.97	1386.17		
+50	1388.63	1387.47	1.16	

.7

√ Grade

L		C.Yds	R	
			+10.7	
		92.87	13.3	+ 42.8
			+8.8	
		72.22	12.4	+ 35.2
			+7.3	
		59.62	11.6	+ 29.2
			+11.9	
		71.11 (77.03)	13.9	+ 47.6 (54.0)
+0.0			11.6	
2.0		97.77 (103.07)	13.8	+ 58.0
			9.4	
		88.51	12.7	+ 37.0
+0.0			+9.9	
3.0		90.37	12.9	+ 60.0
			+6.4	
		79.25	11.2	+ 25.6
-17.5	C.Yds		-0.0 1.7	
24.5	-101.33 - 117.0	+24.62	6.5 88	
			-0.0 2.9	
	-152.77 - 48.0	+ 6.29	4.0 9.8	+ 5.8
			+10.1	
		42.77 (48.88)	13.0	+ 40.4 (47.0)
			+9.5	
		71.59 (78.70)	12.7	+ 38.0
C.Yds	-28.6		-4.6	
(387.37)	35.6	+ 35.18	11.6	+ 366.36
387.37			+7.4	
(48.14)		+ 27.40 (20.37)	11.7	+ 29.6 (22.0)
0.0			+16.4	
3.5		114.72 (107.68)	16.2	+ 94.3
			+11.8	
		131.01	13.9	+ 47.2
0.0			+13.0	
2.0		103.88	14.5	+ 65.0
0.0			+15.5	
5.0		159.47	15.7	+ 100.75
+0.0			+9.7	
4.0		139.95	12.8	+ 50.4
C.Yds		-0.0	+4.4	
64.81	-70.0	57.87	2.5 10.2	+ 12.1
			+7.4	
-(55.55) (120.37)		38.61 (30.64)	11.7	+ 29.6 (21.0)
+1.6			+15.1	
5.8		164.44 (156.48)	15.6	+ 140.0
+1.6		122.48	+14.3 15.7	+ 182.7
10.2		187.05	+15.1 15.5	+ 154.0
+2.1				
7.7			-9.5	
-15.1		142.59	8.8	
22.1	-157.6	11.86	+8.0 12.0	+ 32.0
Grade C Yds		38.66	+9.4 12.7	+ 37.6
-145.92				
Grade 145.92				

Sta	E	G	C	F	C.Yds	L	C.Yds	R
48	1387.03	1389.87		2.84	-133.33	-144.0	48.70	+ 00 6.0 / 3.0 11.0
+50	1389.33	1392.27		2.94	-(62.03) (195.37)		30.18 (23.14)	+ 4.4 / 10.2
49	1397.57	1394.67	2.90		00 4.3		90.89 (83.86)	+ 13.1 / 14.5
+50	1398.37	1397.07	1.30		00 2.0		131.08	+ 12.2 / 14.1
+77.5	1393.57	1398.57		5.0	C.Yds 84.18 -61.3	-165.3	+31.06	0.8 / 8.6
50	1402.27	1399.47	2.80		84.18 2.3 00 3.0		28.63	12.5 / 14.2
+50	1401.65	1401.87		.22			91.43	+ 7.5 / 11.7
51	1402.15	1404.27		2.12	-27.77 (40.0)	-30.0	49.67	+ 00 8.6 / 2.5 12.3
+50	1406.55	1406.67		.12			66.34	+ 12.0 / 14.0
52	1405.95	1409.07		3.12	-31.48 (37.03)	-34.0	53.71	+ 0.0 5.0 / 4.0 10.5
+50	1410.65	1411.47		.82			40.74	+ 0.0 8.5 / 1.0 12.2
53	1414.87	1413.87	1.0				79.62 (89.81)	+ 13.0 / 14.5
+50	1420.17	1415.27	4.9		00 8.0		154.07 (142.5)	+ 14.3 / 15.2
54	1419.07	1416.67	2.4		00 4.0		161.48	+ 10.0 / 13.0
+50	1416.78	1417.17		0.39			80.37	+ 6.7 / 11.3
55	1418.47	1417.67	.7	1.20			47.03	+ 6.0 / 11.0
+50	1422.67	1418.17	4.5		+ 00 7.5		105.09	+ 10.9 / 13.4
56	1422.27	1418.67	3.6		00 5.5		159.07	+ 12.2 / 14.1
+50	1431.82	1419.17	12.6		2.2 9.1		311.57	+ 19.3 / 17.6
57	1419.63	1419.67	0.0				262.40	7.3 / 11.6
+50	1417.63	1420.17		2.5	-51.85	-56	31.85	+ 00 2.6 / 4.0 9.3
58	1423.33	1420.67	2.7		00 4.0		68.7	+ 11.5 / 13.6
+50	1421.93	1421.67	0.8				98.33 (103.70)	9.0 / 12.5
59	1423.43	1421.67	1.8		00 2.0		83.98 (89.35)	10.7 / 13.3
+50	1420.19	1422.17		2.0	-26.85	-29.0	52.87	00 1.8 / +0 8.9
+78.5	1417.01	1422.17		5.1	-96.95 -19.0	-154.7		8.1
60	1417.91	1422.17		4.2	(119.64) -26.0 35.00 -20.5 27.5	-145.8		- 0.8 7.3

Note: from 56 + 54.7 to 56+50 = 1/2

Sta.	E	G	C	F	C.Yds	L	C.Yds	R	
						+ 1.2		+ 15.0	
+ 50	1428.41	1422.67	5.7			8.6		15.5	+ 133.4
61	1423.47	1423.17	0.3				12351	+ 11.5	
							16611	13.7	+ 46.0
+ 50	1422.97	1423.67		1.4	69.44			0.0 + 6.2	
62	1423.97	1424.17		.8			+ 75.0 + 59.81	2.0 11.2	+ 18.6
								+ 0.0 7.4	
+ 50	1425.17	1424.67	.5				37.77	2.0 11.8	+ 22.2
63	1424.17	1425.17		1.0	-(37.96)			+ 8.0	
							50.18	12.0	+ 32.0
+ 50	1428.99	1425.67	3.3			+ 0.0		+ 6.5	
						4.0	53.70 (49.07)	11.2	+ 26.0 (21)
64	1425.68	1426.17		.5				+ 11.7	
							89.01 (84.44)	13.8	+ 70.2
+ 50	1426.68	1426.67	0.0					+ 7.6	
							93.14	11.8	+ 30.4
65	1426.80	1427.17		.3				+ 7.0	
							54.07	11.5	+ 28.0
+ 50	1429.10	1427.67	1.4					+ 8.4	
							57.03	12.3	+ 33.6
						+ 0.0		+ 11.0	
						3.0	79.25	13.5	+ 52.0
+ 77.5	1421.00	1427.92		6.9	-91.10	- 15.4	-178.9	- 3.7	
66	1425.90	1428.17		2.3	- 104.54	19.0	72.0	3.64 + 0.0 5.7	
								5.0 10.8	+ 8.5
+ 50	1438.17	1429.17	9.0			+ 0.0		+ 12.8	
						8.0	135.27	11.2	+ 137.6
66+66+74						+ 4.0		+ 10.3	
67	1435.77	1429.35	6.4			10.0	249.35	13.3	+ 131.7
67+27=67	1432.17	1429.67	2.5			0.0	93.35	+ 8.8	
+ 50	1433.19	1430.17	3.0			4.5		12.2	+ 55.0
						0.0	51.96	10.2	+ 67.0
				(0.0)		4.0		+ 9.4	
68	1430.67	1430.67		1.4			96.85	12.7	+ 37.6
				(0.0)				+ 10.0	
+ 50	1431.17	1431.17		1.7			71.85	13.0	+ 40.0
				(0.0)				+ 11.3	
69	1431.67	1431.67		2.6			78.88	13.6	+ 45.2
				(0.0)				+ 7.8	
+ 50	1432.17	1432.17		2.8			70.74	11.6	+ 31.2
	14334							+ 8.4	
70	~~1432.79~~	1432.67	08	~~.8~~			60.00	12.2	+ 33.6
						+ 0.0		+ 8.6	
+ 50	1434.19	1433.17	1.0			1.5	68.88	12.3	+ 40.8
								+ 7.8	
71	1432.97	1433.67		0.7			66.66	11.9	+ 31.2
						0.0		+ 2.0	
+ 50	1435.57	1434.17	1.4			2.5	62.87	10.6	+ 36.7
								+ 7.1	
72	1435.40	1434.67	.7				60.27	11.5	+ 28.4
				(0.0)				+ 5.7	
+ 50	1435.17	1435.17	-	2.1			47.40	10.9	+ 27.8

Sta	E	G	C	F	L	+ C.Yds	R		
73	1436.17	1436.17		(0 0) 4.2		48.14	+ 7.3 / 11.6	+	29.2
+ 50	1438.50	1436.17	2.3	(0 0) 0.8	00 / 5.4	74.16	+ 7.6 / 11.8	+	30.9
74	1436.67	1436.67		(0 0) 1.8		71.21	+ 6.5 / 11.2	+	26.0
+ 50	1437.42	1437.17	0.2			51.48	+ 7.4 / 11.7	+	29.6
75	1437.89	1437.17	0.7			47.40	+ 5.4 / 10.7	+	21.6
+ 50	1437.19	1437.67		0.5	- C.Yds	47.03	+ 7.3 / 11.6	+	29.2
76	1431.89	1438.17		6.3	- 18.8 / 25.8 -163.88 -177.0	+27.03	- 1.2 / 8.2		
+ 50	1436.89	1438.67		1.8	(44.44) (208.33)	20.74 (14.62)	+ 5.6 / 10.8	+	22.4 (16.0)
77	1439.29	1439.17	0.1			44.81 (38.88)	+ 6.5 / 11.2	+	26.0
+ 50	1442.79	1439.67	2.1		+ 00 / 5.0	68.00	+ 7.3 / 11.6	+	47.4
78	1440.7 / 1436.15	1440.67		(0 0) 1.5		67.26	+ 6.3 / 11.1	+	25.2
+ 50	(1443.74) / 1439.45	1442.04	(1.7)	2.6		38.88 (47.40)	+ 4.2 / 10.1	+	16.8 (26.0)
79	1443.92 / 1441.05	1443.92		(0 0) 2.9		39.62 (48.14)	+ 6.5 / 11.2	+	26.0
+ 50	1444.95 / 1441.35	1444.95		(0 0) 3.6		55.18	+ 8.4 / 12.2	+	33.6
80	1447.47 / 1445.55	1446.17	(1.3)	.6		59.25 (67.22)	+ 7.6 / 11.8	+	30.4 (39.0)
+ 50	1454.23	1447.57	6.7		+ 0.8 / 8.4	174.44 (182.40)	+ 17.6 / 16.6	+	158.0
+ 88.2	1444.60	1448.54		3.9	- 11.8 / 18.8		00 + 0.7 / 5.0 8.3	C.Yds +19.01	
81	1448.10				- 6154	-87.0	110.62	+	1.0
+ 20.5	1452.53	1449.47	(0 0) 3.0		- 13.6 / 19.6		00 10.0 / 4.0 13.3		

Sta	E.	G	C	F		− Cu. Yds L		+ Cu. Yds. R		
82+80			00					+ 7.3 / 11.6		
83	1457.07	1457.07	00		Grade			+ 7.7 / 11.9		
+50	1461.07 / ~~1458.87~~	1461.07		(0.0) ~~2.2~~				+ 7.5 / 11.7	+	30.8
84	1464.27 / ~~1462.77~~	1465.07		(0.8) 2.3				5624 − 00 / 1.0 6.7 / 11.3	+	30.0
+50	1469.75	1469.07	.6			49.07	−53.0	4944	−	23.4
85	1472.87 / 1472.85	1473.07		.2				+ 9.5 / 12.7		
+50	1476.37 / 1476.31	1477.07		.7				5685	+	38.0
86	1486.19	1481.07	5.1		Wrong			+ 5.2 / 10.6		
+50	1488.29	1485.07	3.2					5444	+	20.8
87	1488.69	1489.09		.4				+ 6.1 / 11.1		
+50	~~1494.62~~	1493.07	1.6					4185	+	24.4
88	1498.54	1497.07	1.5					+ 13.5 / 14.7		
+50	1502.60	1501.07	1.6					12611	+	11.8
89	1505.07	1505.07		(0.0) 1.7				+ 6.7 / 11.3		
+50	1509.07	1509.07		(0.0) 3.4				14898	−	49.1
90	1514.27	1513.07	(1.2)	4.5				+ 5.7 / 9.4		
+50	1515.87	1517.07		(1.2) 6.8				6657	+	22.8
91	1521.07	1521.07		(0.0) 4.0				+ 8.0 / 12.0		
								5814	+	40.0
								+ 10.1 / 13.1		
								8627	+	53.1
								+ 6.3 / 9.4		
								8285	+	36.3
								+ 6.2 / 9.5		
								5657	+	24.8
								7.4 / 11.7		
								5037	−	29.6
								+ 8.5 / 12.2		
								6675	+	42.5
								+ 00 / 2.0 5.8 / 10.9		
						−66.66	−72.0	5546	+	7.4
								7.4 / 11.7		
								4351	−	29.6

Sta	E	G	C	F	-Cu yds	L	C. yds	R		
						00		+ 6.9 ✓		
+50	1527.07	1525.07	(2.0)			2.5	60.92 (6325)	11.4	+	36.2 (39.9)
								+ 5.0 ✓		
92	1528.42	1529.07		.6			57.03 (5463)	10.5	+	20.0
				(00)				+ 7.0 ✓		
+50	1533.07	1533.07		3.8			44.44	11.5	+	28.0
				(60)				+ 8.9 ✓		
93	1537.07	1537.07		2.8			58.88	12.4	+	35.6
				(00)				+ 9.4 ✓		
+50	1541.07	1541.07		1.4			67.77	12.7	+	37.6
				(00)				+ 7.0 ✓		
94	1545.07	1545.07		1.8			60.74	11.5	+	28.0
				(00)				+ 9.6 ✓		
+50	1549.07	1549.07		+0			61.48	12.8	+	38.4
								+ 6.2 ✓		
95	1552.69	1553.07		.4			58.51	11.1	+	21.8
						00		+ 10.3 ✓		
+50	1558.79	1557.07	1.7			2.5	73.02	13.2	+	54.07
								+ 3.6 ✓		
96	1561.19	1561.07	.1				63.39 ↵	9.8	+	14.4
						00		3.7 ✓		
+50	1563.91	1565.07		1.2	-41.66	3.0	-45.0 20.74	9.6	+	8.0
				(1.2)				+ 2.2 ✓		
97	1569.87	1569.07		2.5	-34.25	2.5	-37.0 13.98	9.1	+	7.1
								+ 6.6 ✓		
+50	1572.86	1573.07		.2			31.01 ↵	11.3	+	26.7
						00		+ 8.5 ✓		
98	1578.37	1577.07	1.3			2.0	6379	12.2	+	42.6
								+ 5.7 ✓		
+50	1581.02	1581.07	00				6046	10.8	+	22.8
+75	1579.40	1583.07		3.6		9.3		+ 2.0		
99	1583.62	1585.07		(9.7)	-35.31	16.3	-76.2 +10.55	8.8		
							12.03	11.2	+	26.0
				(00)				+ 8.9 ✓		
+50	1589.07	1589.07		2.0			57.03	12.4	+	35.6
				(00)				+ 5.7 ✓		
100	1593.07	1593.07		2.6			54.07	10.8	+	22.8
				(00)				+ 6.1 ✓		
+50	1597.07	1597.07		2.1			43.70	11.0	+	24.4
				(3.0)		7.7		00 1.9 ✓		
101	1598.07	1601.07		4.0	-55.55	14.7	-60.0 23.88	6.5 8.5	+	1.4
+25	1598.87	1603.07		4.6	-43.10	8.8 16.0	-93.1	- 1.7 ✓		
+50	1605.07	1605.07		(00) 1.6			12.77	+ 6.9 ✓ 11.4	+	27.6
								+ 2.8 ✓		
102	1609.38	1609.07	0.3				3592	9.4	+	11.2
								+ 6.3 ✓		
+50	1613.73	1613.07	0.7				33.70	11.2	+	25.2
						7.1		00 3.1		
103	1615.13	1617.07	-	1.9	-38.0 ↵	14.1	-+1.9 29.90	30 9.6	+	7.1
								+ 8.0		
+50	1621.46	1621.07	.4				3620	12.0	+	32.0

Sta	E	G	C	F	- C.Yds	L	+ C.Yds	R	
104	1624.36	1675.07		.7				00 9.7 ✓	
				(00)				1.0 12.8	+ 38.0
+ 50	1629.07	1629.07		1.4				+ 6.6 ✓	
				(00)				59.62 11.3	+ 26.4
105	1633.07	1633.07		1.1				+ 6.3 ✓	
+ 25	1633.61	1635.07		1.4				47.77 11.1	+ 25.2
+ 50	1637.76	1637.07	.7		-21.18	-84 154	-45.78	+11.66 -8.0 ✓	
								11.166 + 6.8 ✓	
106	1637.66	1641.07		3.4		-12.7		11.3	+ 25.2
				(00)	-81.29	19.7	-87.8	00 3.0 ✓	
+ 50	1645.07	1645.07		2.1				26.11 6.0 9.5	+ 3.0
								+ 9.3 ✓	
107	1649.67	1649.07	(0.6)	.8				37.22 12.6	+ 37.2
				(00)				8.0 ✓	
+ 50	1653.07	1653.07		1.6				64.07 12.0	+ 32.0
								+ 11.6 ✓	
108	1658.96	1657.07	1.9					72.59 13.8	+ 46.4
						00 1.0		+ 12.2 ✓	
+ 50	1661.76	1661.07	.7					101.29 14.2	+ 63.0
								+ 9.1 ✓	
109	1667.69	1665.07	2.6					92.03 13.5	+ 36.4
						00 4.5		+ 11.0 ✓	
+ 50	1670.85	1669.07	1.8					97.31 13.5	+ 68.7
						00 1.5		+16.3 ✓	
110	1686.89	1673.07	13.8			1.8 8.9		136.2 16.1	+ 77.42
								+ 24.6 ✓	
+ 50	1674.65	1677.07		2.4				85594 20.3	+ 307.0
								00 12.0 ✓	
111	1683.24	1681.07	2.2					339.81 5.0 4.0	+ 60.0
						00 4.0		+ 9.1 ✓	
+ 50	1689.97	1685.07	4.9					106.11 12.6	+ 54.6
						00 7.0		+ 10.5 ✓	
112	1690.07	1689.07	1.0					13549 13.3	+ 91.73
						00 2.0		+ 9.4 ✓	
+ 50	1695.97	1692.22	3.7			0.9 8.4		128.45 12.7	+ 47.0
								+ 8.2 ✓	
113	1697.67	1695.37	2.3			0.0 4.0		112.31 12.1	+ 74.3
								+ 9.3 ✓	
+ 50	1700.47	1698.52	1.9			00 3.0		12046 12.6	+ 55.8
								+ 5.9 ✓	
P.I.	1701.40	1701.46		00				8499 10.9	+ 36.0
								+ 7.8 ✓	
								6222 12.9	+ 31.2

Change of Line & X Section
from Sta. 0+00 to

Sta	E	G	C	F	L			R		
								+ 2.8	–	
0+00	1166.30	1166.30	0.0				C.Yds.	9.4		+ 11.2
+50	1168.40	1168.40	0.0					+ 9.0	–	
						+	43.7	12.5		+ 36.0
+98.5	1172.41	1170.50	1.9		00			+ 13.3	–	
					3.10	+	101.1	14.07		+ 73.45
1+50	1175.70	1172.60	3.1		00			+ 15.1	–	
					4.00	+	151.6	15.8		+ 90.6
2	1184.00	1174.70	9.3		00			+ 21.0		
					7.0	+	229.7 (269.07)	18.5		+ 157.5 (200.0)
+50	1181.90	1176.80	5.1		00			+ 22.0		
					3.0	+	257.8 (309.44)	19.0		+ 121.0 (145.0)
3	1183.10	1178.90	4.2		00			+ 18.0		
					5.0	+	220.3 (220.3)	17.0		+ 117.0
+50	1181.00	1181.00	0.0					+ 9.1		
						+	14.2	12.6		36.4
4			2.5		Same as old note					

Change of line and X sec"

From Sta 81+20.5 to Sta 88,+00 (82+83 = 83)

Sta	El	Grade						
81+20.5	1452.53	1449.47						253.33
+56.9	1442.39	1450.93	-7.5	29.5 / 36.5	291.75	3.5 / 10.5		293.0
+72.9	1432.01	1451.57	-19.6	29.6 / 36.6	697.13	12.5 / 19.5		705.5
+88.9	1421.21	1452.21	-31.0	59.0 / 66.0	1746.50	21.5 / 28.5		1156.03
82+049	1413.11	1452.85	-39.6	45.6 / 52.6	2155.18	35.0 / 42.0		1273.01
+20.9	1413.71	1453.49	-39.8	39.8 / 46.8	2141.24	39.8 / 46.8		896.90
+ 36.9	1437.69	1454.13	-16.4	40.0 / 47.0	885.83	25.9 / 32.9		350.98
+ 52.9	1445.02	1454.77	-9.8	22.0 / 29.0	298.76	5.4 / 12.4		134.36
+ 60 ✗	—							
+ 68.9	1450.84	1455.5	-4.7	21.2 / 28.2	160.96	1.0 / 8.0		44.71
82+83 = 83			0.0					

16

250
133

050
385
167

Survey of Slashing and Fence Measurement for Geo Kohlhagen
Nov. 16 1915

Course	Feet	Chs/	
Run East	781	11.83	111
N 42° E	79	1.20 ✓	
N 22° E	383	5.80	1
N 16° E	167	253 ✓	
~~W~~ 74° ~~W~~	350	530 ✓	
S 17° W	50	76	
N 70° W	250	379	
S 25 W	300	4.55	
N 81 W	78	1.18	
S 30 W	455	6.89	
	2893	43.73	

Length of wire fence = 5-250' tallies + 220' = 1470' = 89.1 rods

Jan 5 1914

515			
100.		1° R	
+50		1° R	
99		2° R	
+75		2 R	
+50		2 R	
98		2 R	
+50		2 R	
97		2 R	
+50		3 R	
96		2 R	
+50		2 R	
95		2 R	
+50 no change		2 R	
94		2 R	
+50		2 R	
93		2 R	
+50		2 R	
92		3 R	
+50		2 R	
91		2 R	
+50		2 R	
90		2 R	
+50		3 R	
89		R	
+50			

R

+64

6.4
11.2
+ 9.2 N.
11.8
+ 7.5
11.7
- 0.6
8.6
+ 6.6
11.3
+ 9.9
13.9
+ 8.1
12.1
+ 2.6
9.3
+ 4.4
10.2
+ 4.4
10.2
+ 11.5
13.7
+ 8.4
12.2
+ 8.3
12.2
+ 10.5
13.2
+ 11.4
13.4
+ 8.1
12.2
+ 6.1
11.2
+ 7.4
11.7
+ 8.3
12.2
7.0
11.5
8.7
12.4
10.2
13.1
7.8
13.0
8.4
12.2

				E	
90	not changed				
+50				2R	
89				2R	
+50				3R	
88	~~not changed~~ not changed			1R	
+50	"	"			
87	"	"			
+50				2R	
86				2R	
+50				3R	
85				3R	
+50				2R	
84				2R	
+50				2R	
83				3R	
+80				3R	

+8.7
12.4
+10.2
13.1
+7.8
13.4
+8.4
12.8 h.

7.4
11.7
14.4 Brown
12.2
7.5
11.7
6.5
11.2
10.4
13.2
+8.1
12.0
+8.2
12.1
+9.6
12.8
+8.5
12.4 near cliff

20

Notes on Relocation of Canyon Creek Line as Run by Clough and Frank Cain.

The Line Run by Clough will be known as the "O" Line or the original Line and only his Transit Points will be shown in the Relocation.

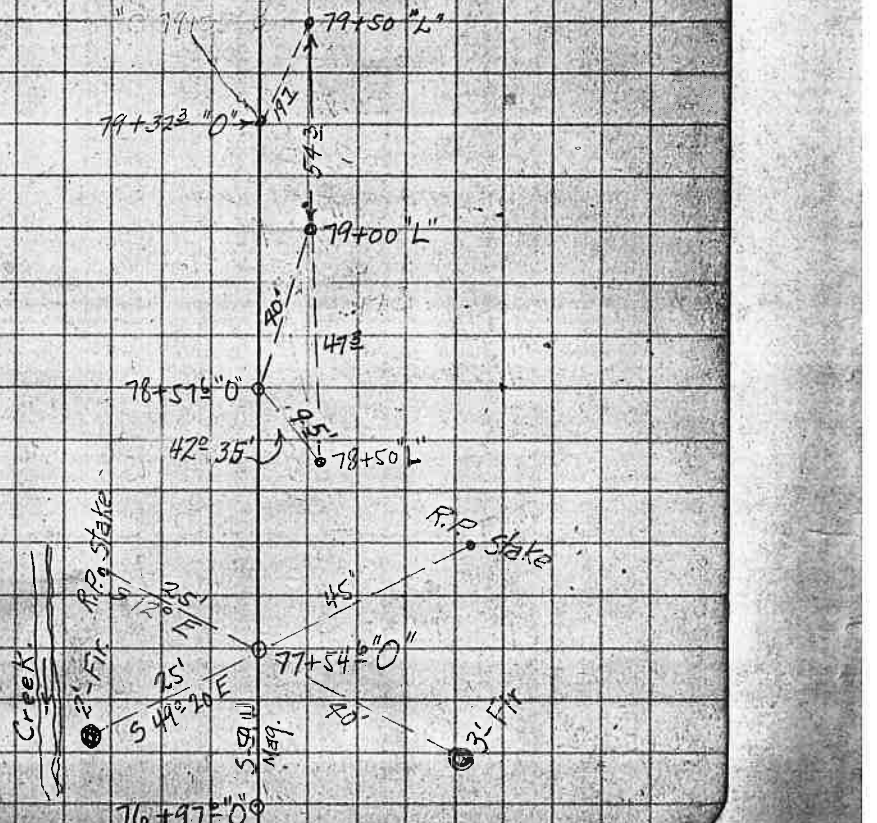
The Line Run by Frank Cain will be known as the "L" Line or Located Line and all points on the "L" Line will be taken from the "O" Line Transit Points where Possible and wherever a point on the "O" Line is the same as one on the "L" Line it will be shown. The Correcked Stationing will also be shown.

All angles are turned Left or Right from the Back Tangent Produced.

1-15-15
Frear - Inst.
W. H. & L. Easley
Snow, Clear.

"O" Line	"L" Line	Dist.	Lt.	Rt.	Mag.	Calc.	Corr. Sta.
80+50 "L" △							
	80+50						
		49±		00°-57'	S88°-50'W.		
1160	80+00						
		48±		01°-39'			
	79+50						
		19±		20°-30'	N72°W		
79+32.3 △							
	79+32.3 "O"						
		36.6	11°-53'		S88°-05'W.		
747	79+00						
		40±	0°-00'		S81°W.		
78+57.6 △							
	78+57.6 "O"						
		9.5		41°-19'	S80°-30'W.		
	78+50						
		51±		45°-07'	S83°-40'W.		
1030	78+00						
		45.4		41°-24	S79°-40W		
77+54.6 △							
		57±			S59°-00'W.		
76+97.6							

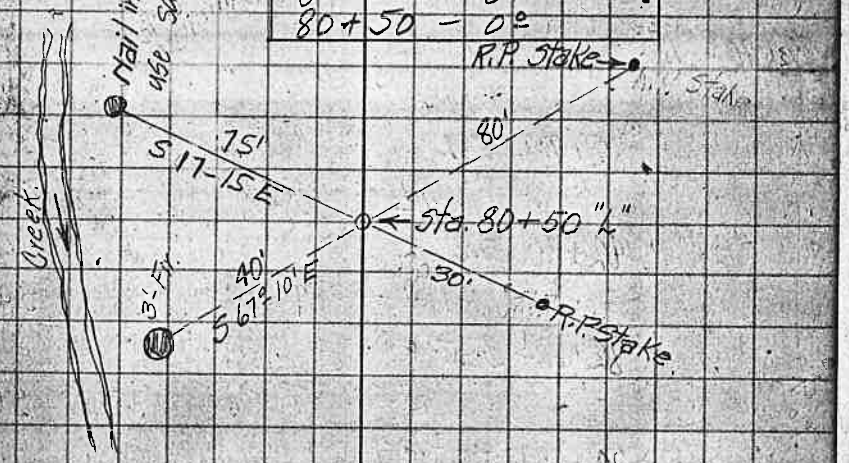
Continued from Page 32



"O" Line	"L" Line	Dist.	Lt.	Rt.	Mag.	Cal.
=	82+36.9	Bent #6				
		18°	75°-35'		S-13-00 W	
=	82+05.2	Hub on Lt. BK. Creek				
		12.6	69°-26'		S-19-35 W	
	Hub	On Rt. BK. Creek				
		7.3	65°-22'		S23-30W	
=	81+85.2 △					
		8.8	63°-09'		S25-45W	
=	81+88.9	Bent #3				
		11.2	60°-17'		S27-45W	
=		Bent #2				
		20.4	57°-02'		S32°W	
=	81+56.9	Bent #1				
		8°	49°-46'		S39-30W	
=	81+48.9 △					
		28.3	47°-08'		S41-50W	
=	81+20.5	E.C. 64°-12'L				
		29°	34°-15'		S54°30'W	
=	80+88.2	P.C.				
		28.8	15°-40'		S73°25'W	
=	80+57.2	P.C.				
		7.2	0°-00'		S89°W	
△ 80+50 "L"						

Correct Position of Stakes on Fill.

Corr. Sta.	
83+00	1.8 Ft. Rt.
82+90.8	-0-
82+80	2.8 ft. Lt.
82+68.9	-0-
82+52.9	-0-
82+36.9	1.2 ft. Rt.
82+05.2	1.2 ft. Lt.
81+85.2	-0-
81+88.9	-0-
81+56.9	1.5 ft. Rt.
81+48.9	-0-
81+20.5	-0-
80+88.2	3° Lt.
80+57.2	-0-
80+50	-0-



1-15-15
Frear Inst.
W.H. & L. Easeley
Snow - Clear.

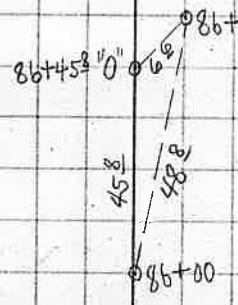
"O" Line	"L" Line	Dist	Lt.	Rt.	Mag.	Calc.	Corr. Sta.
	8						
84+50.6 "O"							
	84+50.6 "O"						
		50.6	84°-44'		S88-55E		
	84+00						
		20.3	80°-08'		S.84-20E		
	83+79.9						
		29.9	78°-39'		S82-50E		
167.8	83+50						
		50.3	75°-57'		S81-05E		
	83+00 Ahead = 83+10 Back.						
		18.0	77°-03'		S81-45E		
82+90.8 "L"							
	82+90.8 End.						
		12.2	93°-07'		S 04-35 E S 03-45 E		
	82+80 E.C.						
		11.7	89°-01'		S 00-45 W.		
169.0 =	82+68.9 Bent #8						
		16.0	85°-56'		S 03-00 W		
=	82+52.9 Bent #7						
		16.2	80°-46'		S 08-15 W		
80+50 "L"	82+36.9						



"O" Line	"L" Line	Dist.	Lt.	Rt.	Mag. Calc.
	87+00				
		48 ±		35°-36'	S 06-45 W
	86+50				
		6 6		69°-53'	S 41-30 W
86+45 8 △					
	⊙ 86+45 8 "O"				
		45 8		26°-00'	S 28-30 E
86+00 L △					
	⊙ 86+00				
46					
		46 °		12°-41'	S 54-35 E
85+53 8 △					
↑					
	⊙ 85+53 8 "O"				
50.31		47		15°-06'	S 67 E
↓	85+50				
	—	45 7		15°-35'	S 66-30 E
85+03 5 △					
↑					
	⊙ 85+03 5 "O"				
52.9		3 5		06°-46'	S 82-30 E
	85+00				
↓		49 4		07°-26'	S 81-45 E
84+50 6 △ "O"					

1-16-15
Frear
W.H. Easley
L. "
Clear.

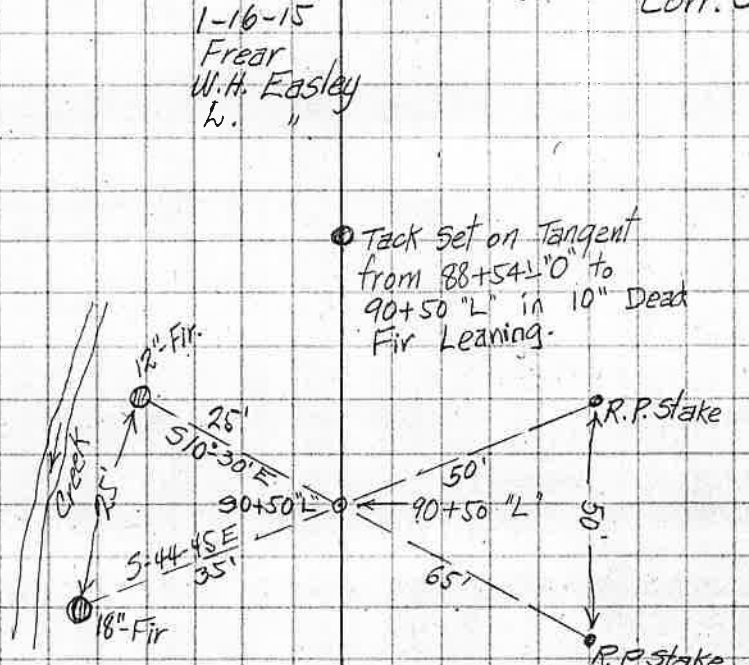
Corr. Dist.

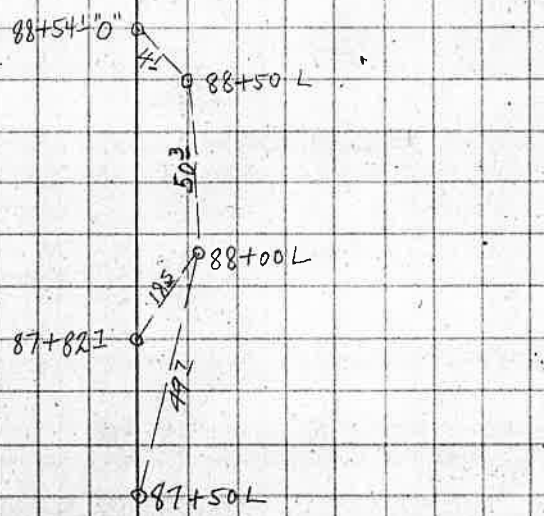


Clear - Cold.

1-16-15
Frear
W.H. Easley
L. "

"O" Line	"L" Line	Dist.	Lt.	Rt.	Mag.	Calc.	Corr. Sta.
Continued on Page.							
△ 90+50 "L"							
	⊙ 90+50						
197		51 3/5		29°-14'	S65-40 W.		
	90+00						
		146 6/10		31°-00'	S66-25W		
88+54± △							
	⊙ 88+54±"O"						
		4±		29°-08'	S36-10W		
72 01	88+50						
		50 3/10		31°-00'	S37°W		
	88+00						
		18 5/10		39°-00'	S45-30 W		
87+82 7/10 "O" △							
	⊙ 87+82 7/10 "O"						
136 2/10		34 0/10		35°-11'	S06-45W		
	87+50						
		48 2/10		35°-10'	S06-45W		
86+45 8/10	87+00						

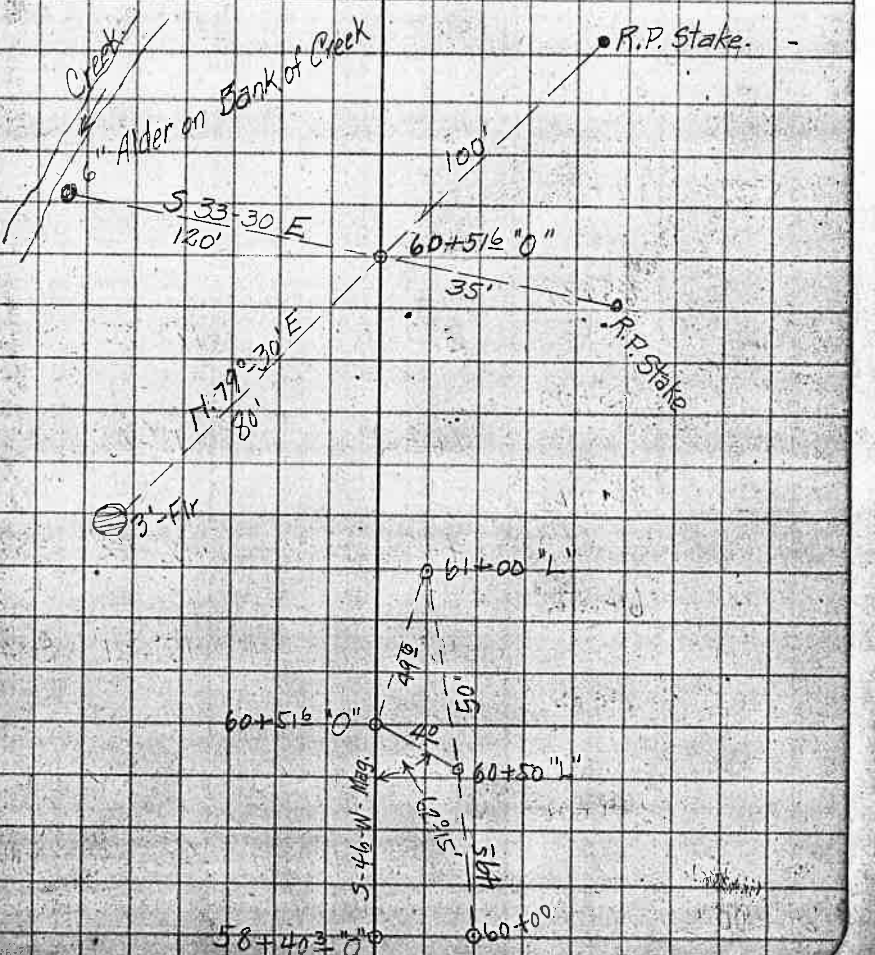




1-19-15 - Clear.
Frear
W.H. Easley
L. "

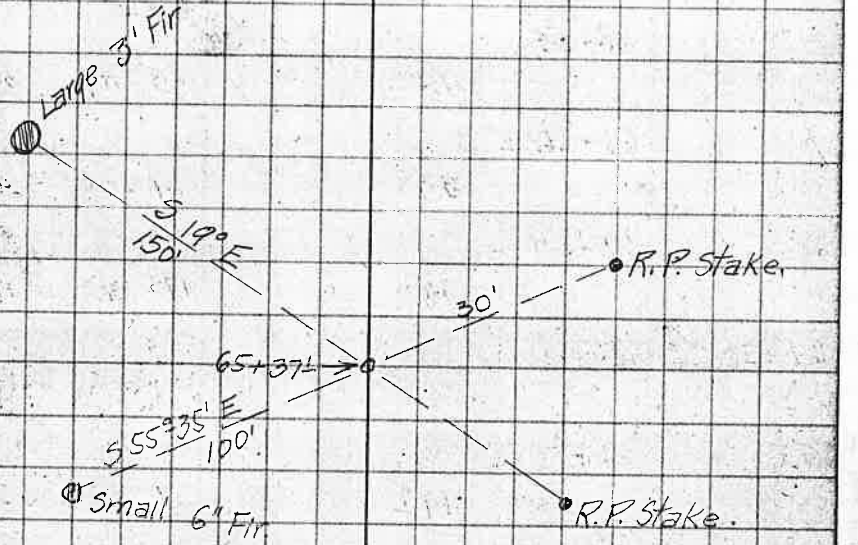
"O" Line	"L" Line	Dist.	Lt.	Rt.	Mag.	Calc.	Corr. Sta.
64+00 △ "L"							
	64+00 ⊙						
		47.5		02°-32'	S 49-00 W.		
	63+50						
		16.0		04°-02'			
	63+33.3 △ "O"						
		33.3		04°-43'	S 51-25 W		
	63+00						
		50.5		05°-01'			
	62+50						
344.0		26.0		05°-46'	S 52 W.		
	62+23.5 △ "O"						
		23.5		06°-25'	S 52-10 W.		
	62+00						
		50.5		06°-00'	S 52° W		
	61+50						
		12.0		06°-44'	S 52°-50' W		
	61+38 △ "O"						
		38.0		07°-57'	S 53-55 W.		
	61+00						
		49.6		07°-57'	S 53-55 W		
60+51.6 △							
					S 46 W.		
58+40.3							

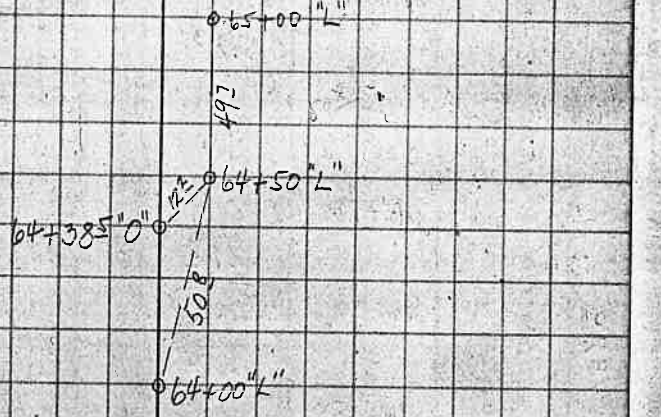
Continued from Page. 49



"O"	"L"	Dist.	Lt.	Rt.	Mag.	Cal.
	66+16	E.C.				
		16°	14°-22'		S 40-20W	
	66+00					
		23°	06°-32'		S 48-15 W.	
	65+86	R.O.C.				
		28 8		07°-08'	S 62 W.	
	65+57					
		8°		19°-13'		
	65+39±	B.C.				
		12°		25°-38'	S 80-45W	
65+37±						
	65+37±					
		36 1		17°-55'	S 55°W	
	65+00					
		6±		15°-08'		
98	64+94±					
		44°		12°-42'	S 49-45 W	
	64+50					
		12±		15°-21'	S 52-45W	
64+38.5± "O"						
	64+38.5± "O"					
		38.5	11°-41'		S 36-50 W.	
64+00 "L"						

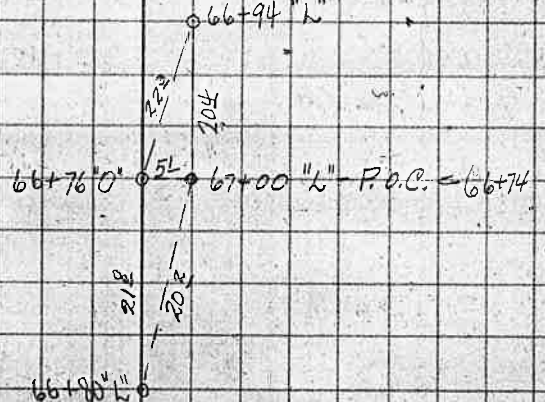
Ref 65+37±



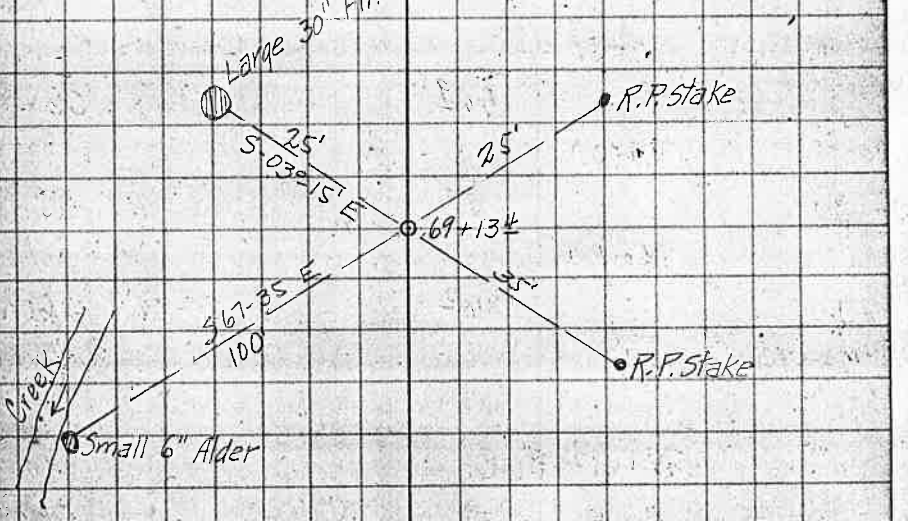


Corr. Sta.

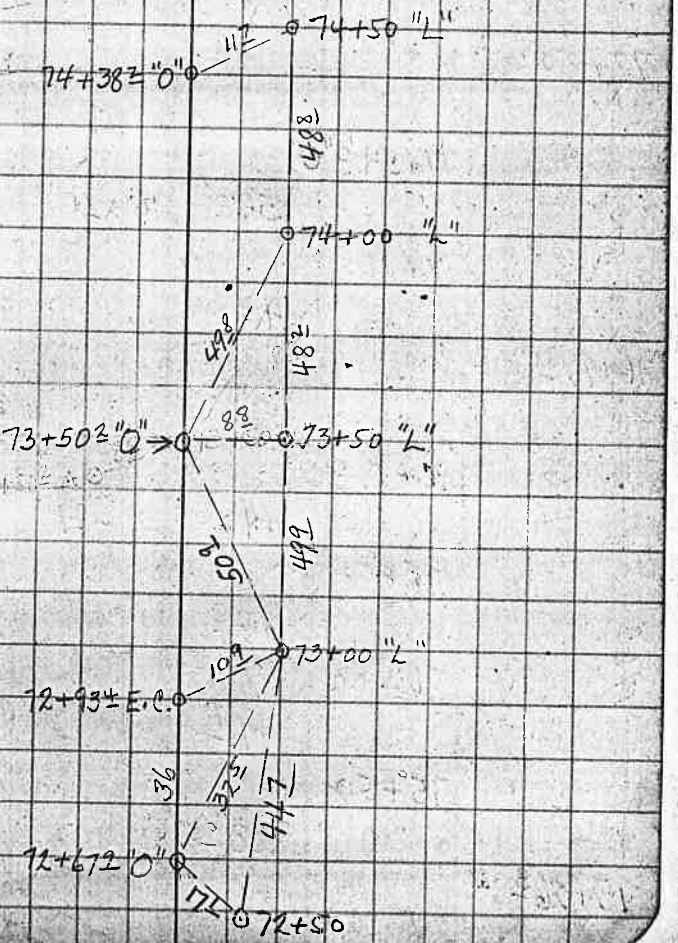
"O"	"L"	Dist.	Lt.	Rt.	Mag.	Cal.	Corr. Sta.
	69+00						
		49 4		09°-20'	S64-05W		
	68+50						
		8°		15°-04'			
	68+43 "O"						
		43 6		14°-25'	S69-45W		
	68+00						
		48 6		17°-30'	S72-25W		
67+50 "L"							
	67+50 "L"						
		49 7		39°-28'	S54-45W		
77 N,	67+27						
		6 8		26°-00'			
	66+94 E.C.						
		22 3		27°-40'	S43-25W		
66+76 "O"							
	66+76 "O"						
		21 8	39°-41'		S-15-30W		
51	66+80	B.C. 12° R.					
137		29 2	35°-03'		S19-45W		
	66+50						
		25 5	24°-51'		S30 W		
65+37	66+16 E.C.						



"O"	"L"	Dist.	Lt.	Rt.	Mag.
	72+50				
		50 ±	29°-32'		S 32-05 W
	72+00				
		113	29°-53'		
	71+88]				
		39 ±	29°-56'		S 31-45 W
	71+50				
		498	29°-15'		
	71+00				
		199	28°-25'		S 33-45 W
353.4	70+80 ±	"O"			
		29 ±	27°-55'		
	70+50				
		50 9	27°-25'		
	70+00				
		169	24°-13'		S 37-45 W
	69+82]	"O"			
		33 ±	23°-16'		
	69+50				
		36 ±	18°-34'		S 43-05 W
69+13.4 ±	"O"				
156.8	69+13.4 ±	"O"			
		136		07°-18'	S 62-30 W
67+50	"L"	69+00			

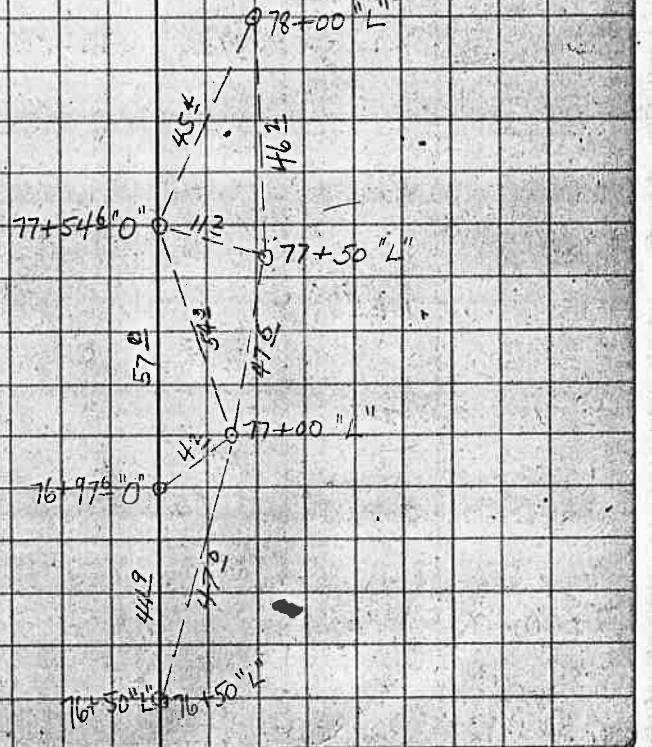


"O"	"L"	Dist.	L.	R.	Mag.
	⊙ 75+26 3				
		26 7		10° 16'	N82-10W.
	75+00				
		50		09° 55'	N82-10W.
74+50 △ "L"					
↑					
	⊙ 74+50				
		11 7		20° 39'	S88-10-W
	74+38 ± △ "O"				
98 8		38 ±		17° 34'	
↓	74+00				
		49 8		21° 13'	S88-45W.
73+50 ± △ "O"					
↑					
	⊙ 73+50 ± △ "O"				
		50 9		35° 08'	S67-30W.
	73+00				
83 6		10 9		45° 33'	S77-35W.
↓	72+93 ± E.C.				
		36 ±		28° 06'	S60 W.
72+67 9 △					
↑					
358 ±	72+67 9 P.O.C.				
		17 ±	29° - 56'		S32° W.
69+13 ± △	72+50				



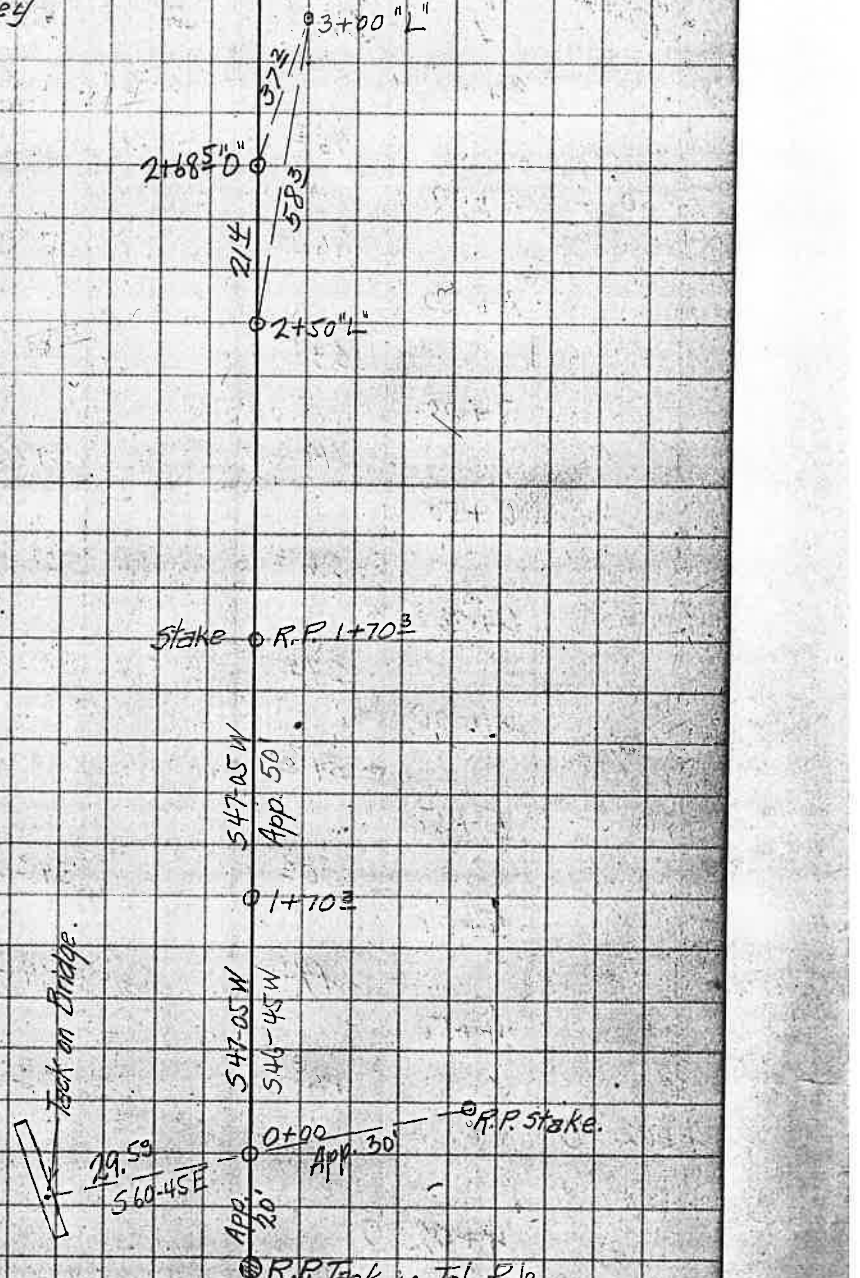
1-19-15 - Clear.
Frear
W.H. Easley
L. "

"O"	"L"	Dist.	Lt.	Rt.	Mag.
	Continued on Page 22				
77+54⅙ △					
	⊙ 77+54⅙ "O"				
57.0'		54⅗	16-21		S 59 W.
	77+00				
		4±		30°-45'	
76+97⅙ △					
	⊙ 76+97⅙ "O"				
		44⅘	23°-19'		S 75° W.
	76+50				
146.0'		49⅕	11°-36'		S 86-50 W.
	76+00				
		49⅘		07°-57'	
	75+50				
		23⅙		12°-46'	N 68-45 W.
75+26⅗ △					

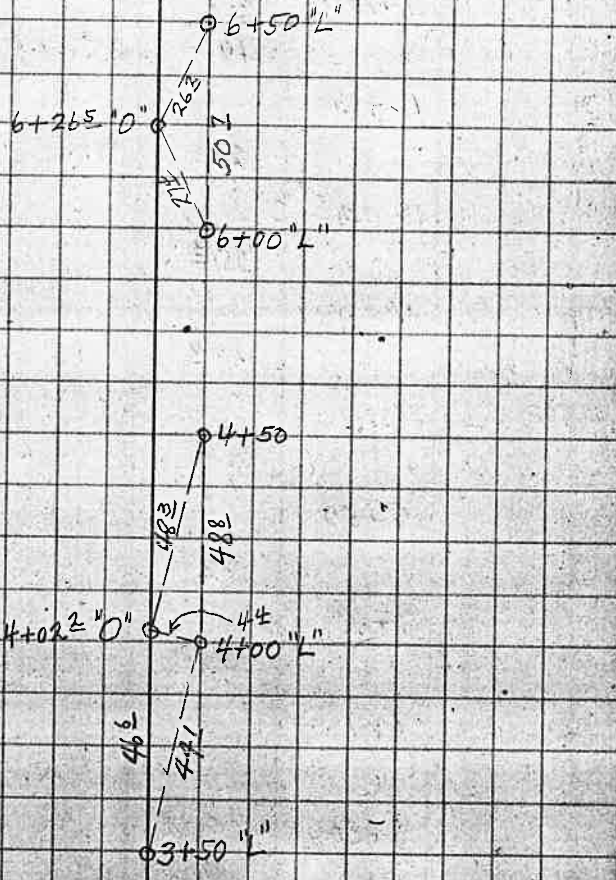


1-21-15 - Foggy.
Frear
W. H. Easley
L. "

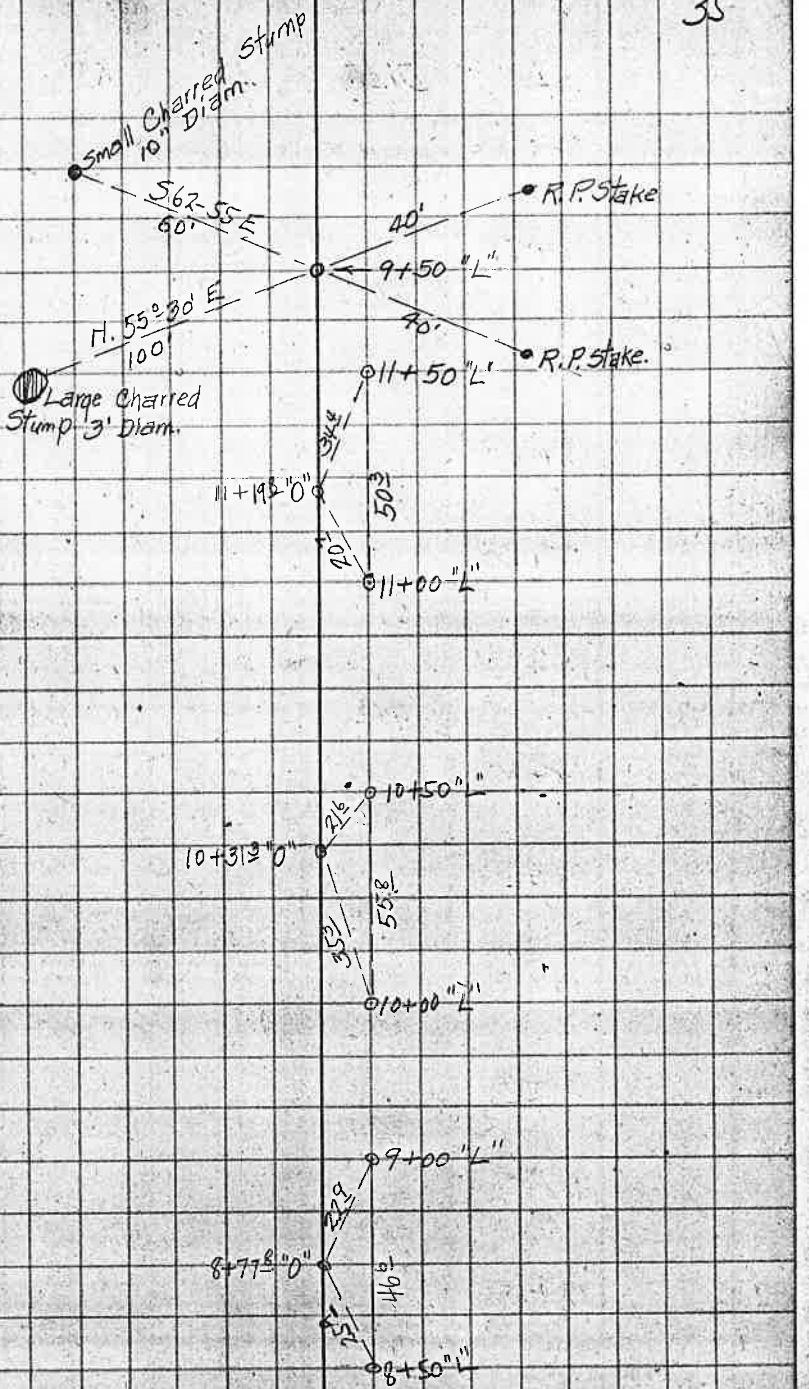
"O"	"L"	Dist.	Lt.	Rt.	Mag.
3+50 △ "L"					
	⊙ 3+50				
		50	46°-31'		S00-35'W
	3+00				
		37½	40°-51'		
	2+68½ △ "O"				
178'		21¼	36°-00'		
	2+50				
		47⅜	35°-54'		
	2+00				
		29⅝	30°-54'		S15-45W
1+70⅜ △					
	⊙ 1+70⅜				
		19⅞		01°-04'	S47-05W
	1+50				
		51⅝		01°-30'	S47-15W
169'	0+98⅝				
		48⅝		03°-57'	S49-40W
	0+50				
		50	0°-00'		S46°-05W
0+00 "O" △					



"O"	"I"	Dist.	Lt.	Rt.	Mag.
	8+00				
		46.5	11°-02'		S 13 W
7+50 △ "L"					
	⊙ 7+50 "L"				
		53.5		30°-15'	S 23-25 W
	7+00				
		49.5		31°-36'	
	6+50				
		26.2		32°-25'	
	6+26.5 △ "O"				
		27.4		30°-45'	S 24-05 W.
	6+00				
		51.6		33°-41'	
	5+50				
		50.3		34°-06'	
	5+00				
		49.1		34°-52'	
	4+50				
		48.3		33°-53'	S 25-05 W
4+02.2 △ "O"					
	⊙ 4+02.2 "O"				
		46.6	07°-03'		S 07° E.
3+50 △ "L"					

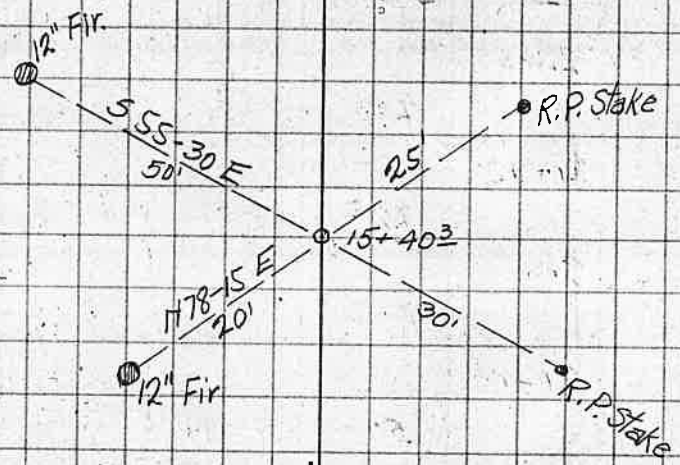


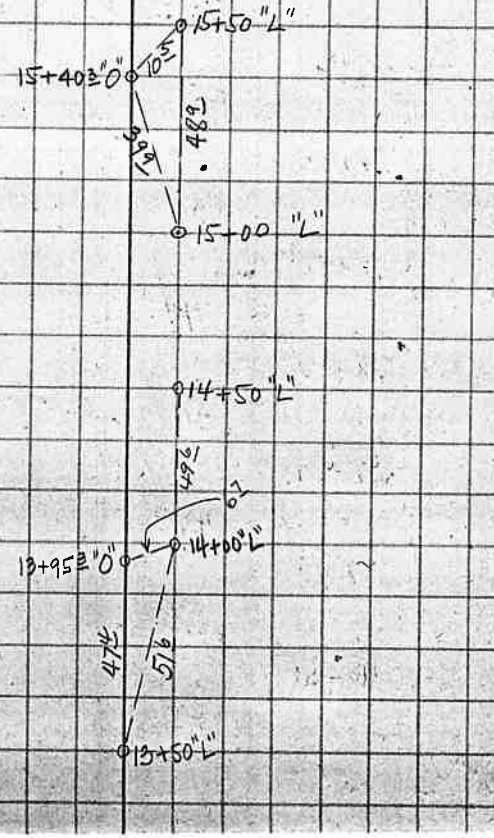
"O"	"L"	Dist.	Lt.	Rt.	Mag.
11+50 "L" △					
	11+50 "L"				
		34.4	25°-34'		S-10-15 E
	11+19.8 △ "O"				
		20.1	29°-18'		
	11+00				
		49.1	25°-43'		S09-40 E
104.1	10+50				
		21.6	21°-51'		
	10+31.3 △ "O"				
		35.3	23°-16'		
	10+00				
		50.8	13°-24'		S 02° W
9+50 △ "L"					
	9+50				
		52.5	08°-22'		S 15-30 W
	9+00				
		22.9	09°-26'		
168	8+77.8 △ "O"				
		25.9	13°-04'		
	8+50				
		52.5	10°-12'		S 13-45 W
7+50 "L"	8+00				



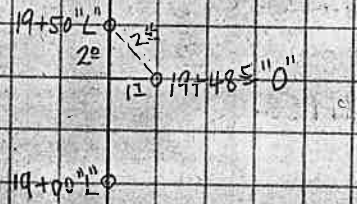
"O"	"I"	Dist.	Lt.	Rt.	Mag.
	16+00				
		48±		19°-05'	S-13-30 W
58±	15+50				
		10 ±		28°-00'	
15+40± "O"					
	15+40± "O"				
		39 ±		04°-32'	S05-35 E
	15+00				
		51 ±		05°-26'	
	14+50				
		49 ±		06°-16'	S04-30 E
	14+00				
		62		06°-25'	
	13+95± "O"				
		47 ±		05°-12'	
386 ±	13+50				
		49 ±		06°-25'	
	13+00				
		48 ±		06°-10'	
	12+50				
		51 ±		04°-46'	
	12+00				
		46 ±		05°-08'	S05-25 E
11+50 "L"					

Ref. 15+40±

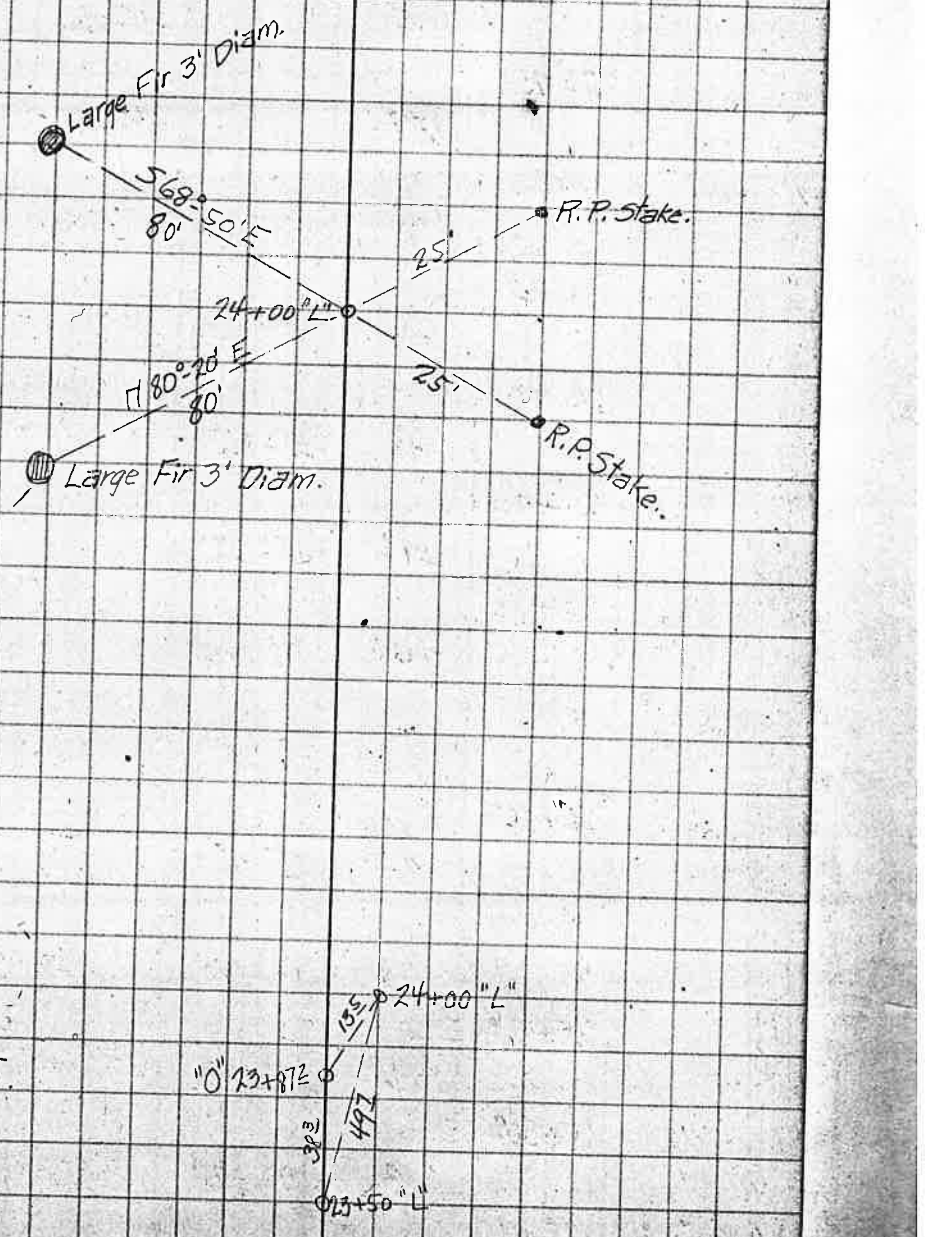




"O"	"I"	Dist.	Lt.	Rt.	Mag.
	21+00				
		27	11°-50'		S05-30W
	20+72.3 △				
		22.5	11°-02'		
	20+50				
		48.9	10°-36'		
	20+00				
		50	07°-49'		S09-30W
	19+50				
		50.2		00°-07'	
19+00 △ "L"					
	19+00				
		50.1		03°-14'	S 16-20W
	18+50				
		49		03°-42'	
	18+00				
		50		04°-55'	
	17+50				
300 ±		49.5		06°-21'	S20-05W
	17+00				
		52°		07°-55'	
	16+50				
		50		06°-36'	S 20-15 W
16+00 △ "L"					



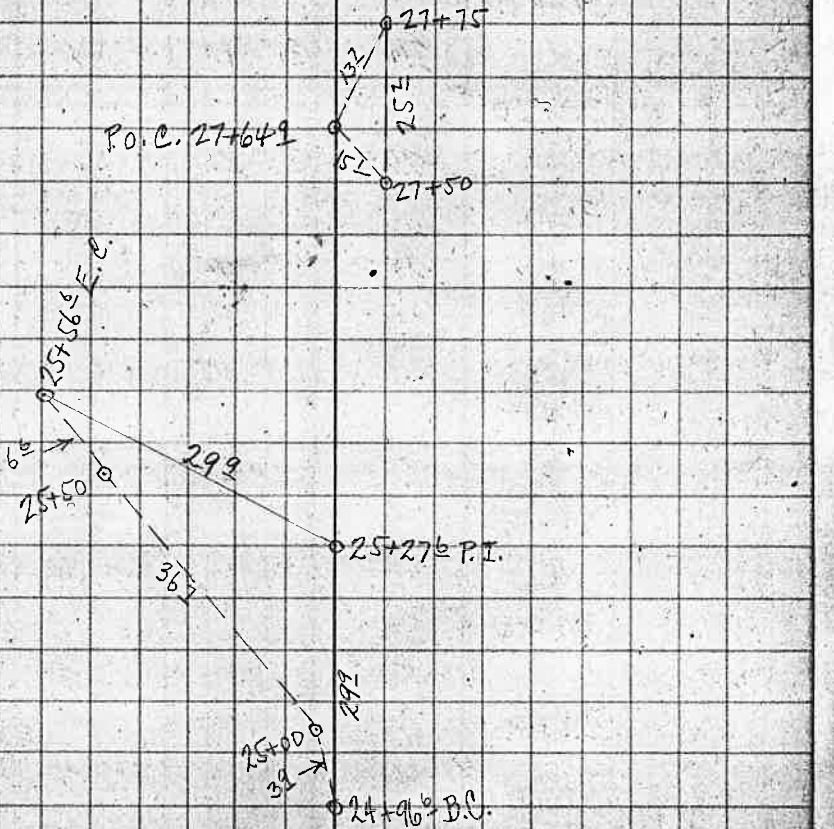
"O"	"L"	Dist.	Lt.	Rt.	Mag.
	25+00				
		39		10°-06'	
	24+96 B.C. 148° L				
		47		09°-25'	
	24+50				
		50		09°-49'	S13-10 W
24+00 "L"					
	24+00				
		13	12°-42'		S04-20 W
	23+87 "O"				
		38	13°-37'		
	23+50				
		50	13°-30'		
	23+00				
		50	12°-54'		
495-3	22+50				
		49	12°-12'		
	22+00				
		33	12°-18'		S04-55 W
	21+65 "O"				
		16	12°-37'		
	21+50				
		50	12°-06'		
19+00 "L"	21+00.				



1-21-15 Frear
Foggy. W.H. Easley
Calc. C. L. "

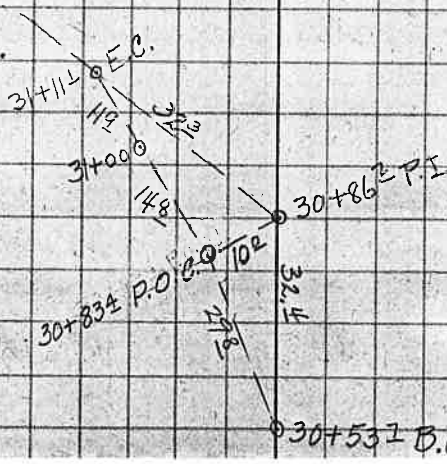
700
164
136

"O"	"I"	Dist.	Lt.	Rt.	Mag.
	28+00				
		21 ±		45°-28'	S20°E.
	27+75				
		137		55°-00'	
27+64 ± △					
	◎27+64 ± P.O.C.				
		15 ±	44°-12'		S65-35 E.
	27+50				
		50	43°-56'		
138'	27+00				
		49 ±	45°-28'		
	26+50				
		24 ±	43°-09'		S64-25 E.
26+25 ± △					
	◎26+25 ±				
		25 ±	25°-54'		S21-30 E.
	26+00				
		44 ±	18°-40'		S14-10 E
165'	25+56 ± E.C.				
		6 ±	02°-46'		
	25+50 ± P.I.				
		36 ±	00°-30'		S03-30 W
24+00 △ "L"	25+00				



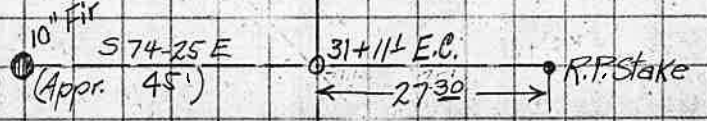
1-22-15 Clear
Frear
L. Easley.

"O"	"I"	Dist.	Lt.	Rt.	Mag.
30+83± P.O.C.					
	P.I.		33°-39'		S 48-30 E
	30+83± P.O.C.				
		29±	29°-51'		S 45-10 E
	30+53± B.C. 119°-30' R.				
		3±	32°-27'		
	30+50				
137±		24	31°-40'		
	30+20				
		26±	31°-32'		
	30+00				
		40	29°-54'		
	29+50				
		17±	19°-30'		S 35-10 E
29+32±	29+50				
	29+32±				
		33±		50°-11'	S-15-20 E
	29+00				
167±		50		50°-53'	S 14-45 E
	28+50				
		49±		49°-50'	
27+64±	28+00				



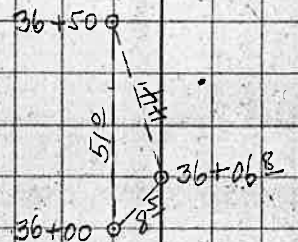
1-22-15
Clear
Frear
L. Easley.

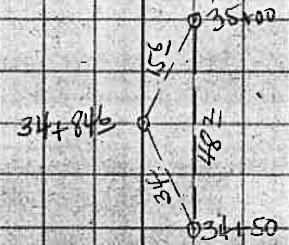
"O"	"L"	Dist.	Lt.	Rt.	Mag.
33+75.9 △					
	⊙ 33+75.9 △				
		25.7		30°-25'	S-29-25 W
	33+50				
		50		31°-14'	
	33+00				
		50		32°-53'	
	32+50				
		24.9		33°-44'	
2229	32+24.8 △				
		25.0		34°-30'	S33-30 W
	32+00				
		49.3		33°-43'	
	31+50				
		22.7		28°-25'	
	31+27.8				
		16.7		15°-15'	
31+11.1 △ E.C.					
	⊙ 31+11.1 E.C.				
		11.9		44°-28'	S01-30 E
41 26	31+00				
		14.6		37°-00'	S08-35 E
30+83.4 △ P.O.C.					



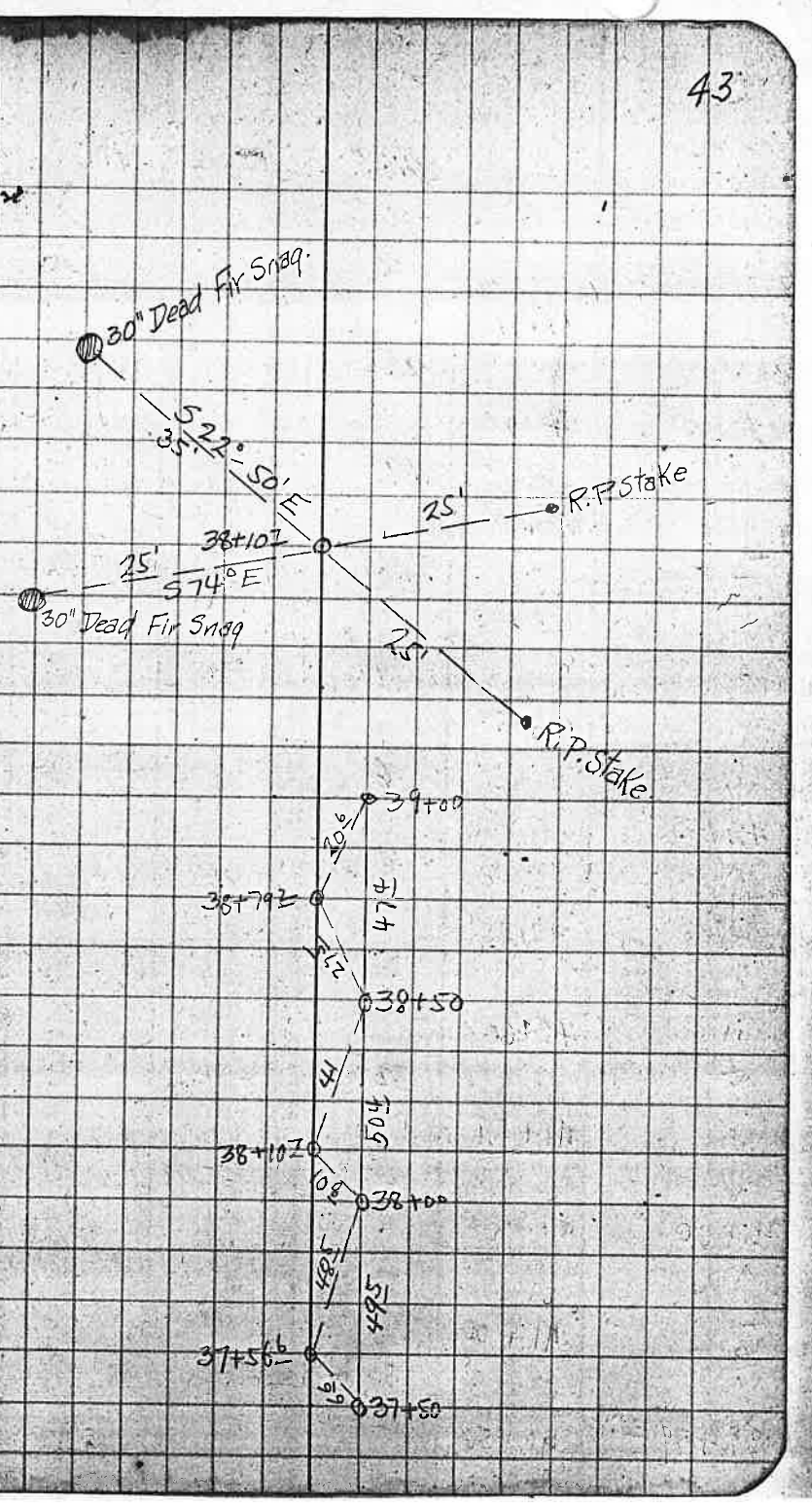
1-23-15
Frear
Germond
L. Easley
Clear

"O"	"L"	Dist.	Lt.	Rt.	Mag.
	37+50				
		48±	14-52		
	37+00				
		50	14-01		
	36+50				
		44	13-21		
36+06.8 △					
↑					
	⊙36+06.8				
		85		16-24	S17-30W
	36+00				
121.9		49.1		14-43	
	35+50				
		49.6		15-56	
↓	35+00				
		15.6		22°-57'	
34+84.6 △					
↑					
	⊙34+84.6				
		34	28-20		S01-50W
108.0	34+50				
		50	25-39		
	34+00				
↓		24±	24-49		
33+75.9 △					

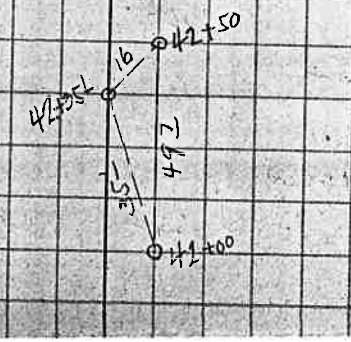




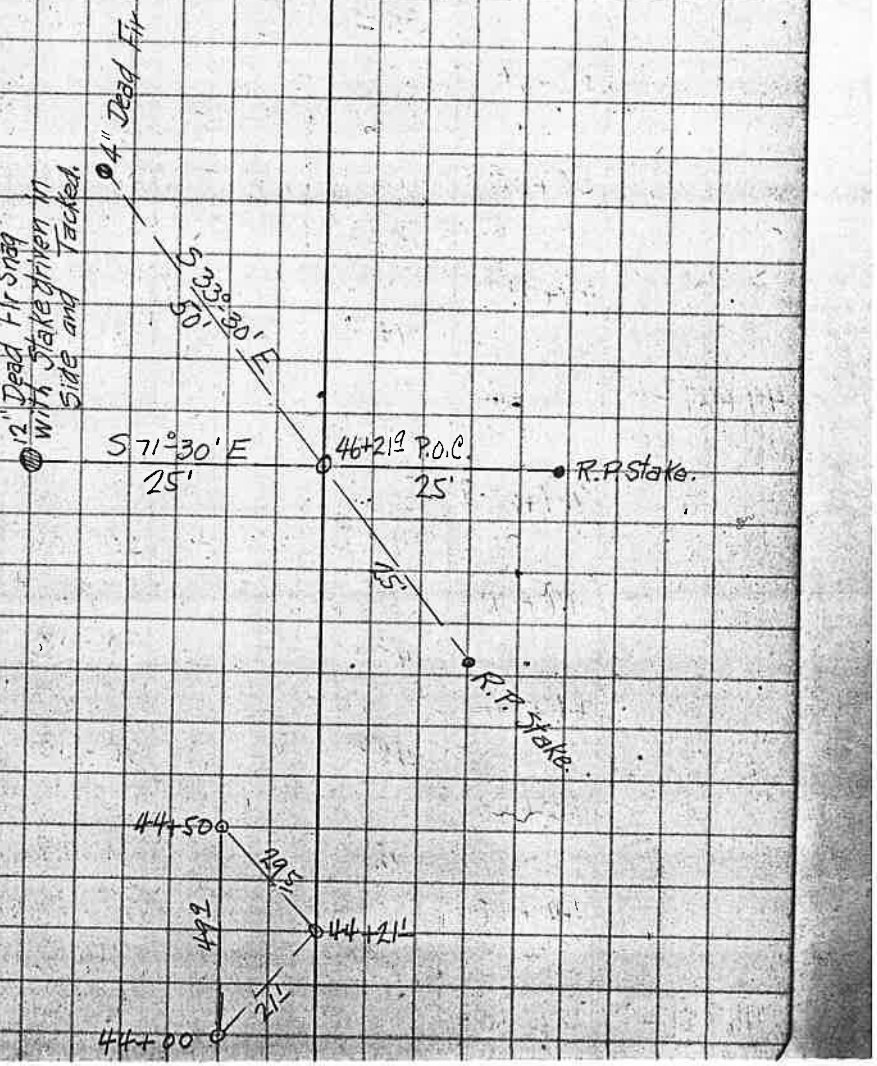
"O"	"L"	Dist.	Lt.	Rt.	Mag.
	40+50				
		48.9		01-32	
	40+00				
		49.2		05-49	
	39+50				
		49.9		14-06	
	39+00				
		20.6		23°-00'	
38+79.2 △					
	⊙ 38+79.2				
		27.5		33-51	S59-55W
684	38+50				
		41		32-31	
38+10.7 △					
	⊙ 38+10.7				
593.1		10.8		24°-42	S25W
	38+00				
		48.5		24-22'	
37+56.6 △					
1457	⊙ 37+56.6				
		6.6	17-17		S04-30W
36+06.8					



"O"	"L"	Dist.	Lt.	Rt.	Mag.
44+21 ⊥ △					
↑ 184	⊙ 44+21				
		21 ⊥	15°-11'		S18-45 E
	44+00				
		49 ±	17-17		
	43+50				
		50	19-29		
	43+00				
		49 ±	18-36		
	42+50				
↓		16	05-42		
42+35 ± △					
↑ 98	⊙ 42+35 ±				
		35 ±	61-34		S04 E
	42+00 P.T.				
		32 ±	44-34		
	41+59 P.O.C.				
↓		43 ±	31-50		
41+00 △					
↑ 215	⊙ 41+00				
		50 ±	01°-17		S58-45 W
↓ 38+79 ± △	40+50				

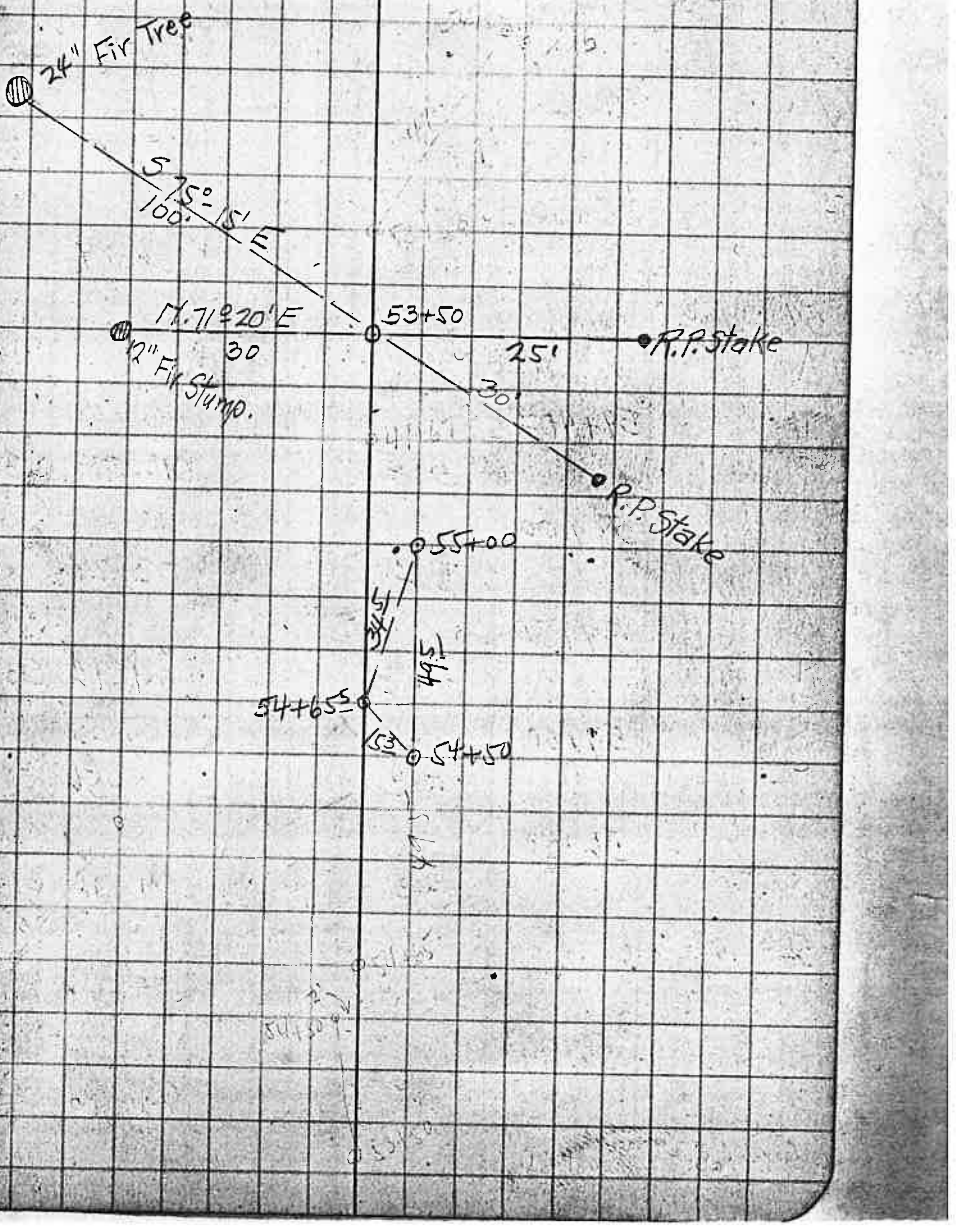


"O"	"L"	Dist.	Lt.	Rt.	Mag.
	47+50				
		30 ±		30-29	
	47+15 ± E.C.				
		32 ±		39°-12'	
	46+81 ± P.O.C.				
		30 ±		49-55	
	46+50				
		3 ±		51-52	
	46+48 ± B.C. 88°-40' L.				
		4 ±		50-56	
	46+43 ± E.C.				
		21 ±		48°-43	
46+21 ± P.O.C.					
	46+21 ± P.O.C.				
		22 ±		20-32	S01-15W
	46+00				
		49 ±		19-18	
198°	45+50				
		50 ±		18-08	
	45+00				
		48 ±		15-48	
	44+50				
		29 ±	01-21		
44+21 ±					

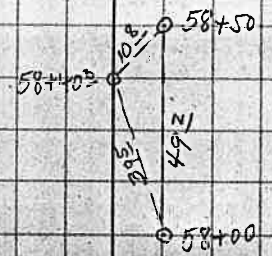


"O"	"L"	Dist.	Lt.	Rt.	Mag.
	51+48 ±				
		48 ±	51-34		S20 E
	51+00				
		51	50-05		
	50+50				
		36 ±	50-51		
	50+11 ± E.C.				
		11 ±	45-12		
	50+00				
		23 ±	42-38		
	49+77				
		11 ±	08-27		
49+67 ± △					
	⊙ 49+67 ±				
		17 ±		30°-04'	S31-50W
	⊙ 49+50				
		49 ±		30°-22'	
	49+00				
34 ± 2		48 ±		30°-13'	
	48+50				
		50		31°-08'	
	48+00				
		60 ±		31-52	
46+21 ± △	47+50				

"O"	"L"	Dist.	Lt.	Rt.	Mag.
	56+00				
		49.2		25-37	
	55+50				
		49.1		21-46	
	55+00				
		34.5		18-28	
54+65.5 △					
	⊙ 54+65.5				
		15.3		25°-33'	S03-50W
112.21	54+50				
		49.5		26°-44'	
	54+00				
		47.1		18°-47'	
53+50 △					
	⊙ 53+50				
		49.8	52°-50'		S20-20E
	53+00				
380.51		49.1	52-39		
	52+50				
		50.5	52-04		
	52+00				
		51.4	51-42		
49+67.1	51+48.4				

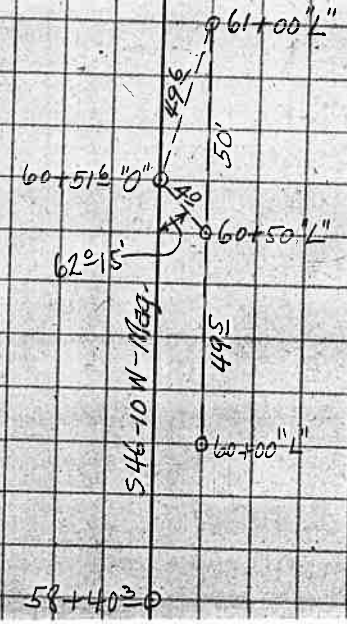


"O"	"L"	Dist.	Lt.	Rt.	Mag.
	59+78.5				
		29 L		18-18	
	59+50				
		49 L		16-34	
	59+00				
		49.2		19-19	S53W
	58+50				
		10.8		26-17	
58+40.3 ▲					
	⊙ 58+40.3				
		39.5		01°-27'	S33W
	58+00				
		51.3		02-28	
	57+50				
195.1		50.2		04-16	S35-35W
	57+00				
		51.4		03-56	
	56+50				
		36		04°-00	
56+44.3 ▲					
177.51	⊙ 56+44.3				
		45		27°-46'	S31-30W
54+65.5	56+00				



1-23-15 Clear.
Frear Inst
Germond
A. Easley

"O"	"L"	Dist.	Lt.	Rt.	Mag.
Continued on Page 27					
60+51.6 △					
	60+51.6	4°		12°-45'	S46-10W
209.51	60+50	49.5		13°-44'	
	60+00	21.2		16°-03'	
58+40.3					



Survey for Riddle Light & Power Project - In T. 30- R-

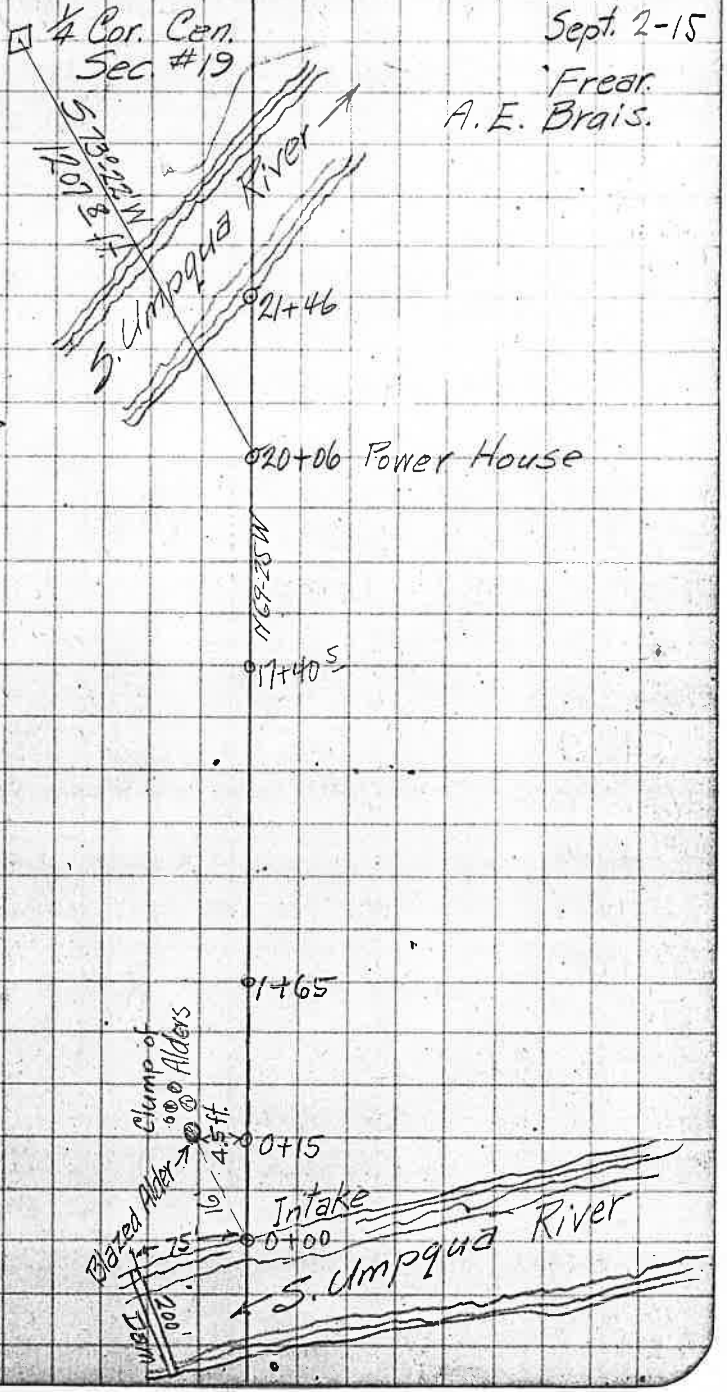
Var. of Needle 21° 30'

Sept. 2-15

Frear.

A. E. Brais.

Sta.	Dist	Lt.	Rt.	Mag.	Calc.
21+46					Waters Edge
	140	18°-00'		N87° W	N87-25 W
20+06 Power House site.					
	265±	11°-53'		N69° W	N69-25 W
17+40±					
	209±		38°-11'	N57-30 W	N57-32 W
15+31±					
	281±		31°-32'	S84° W	S84-17 W
12+50					
	663		11°-05'	S52-55 W	S52-45 W
5+87					
	283±	33°-06'		S41-45 W	S41-40 W
3+03±					
	138±	05°-24'		S74-45 W	S74-46 W
1+65					
	165			S80°-10' W	S80-10 W
0+00					Waters Edge



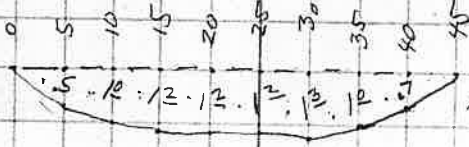
Levels for Riddle Light & Power Project. (Sec. 19- T-30- R-5) Sept. 2-15

Sta.	+	H.I.	−	Rod	Elev.
B.M.	1.81	601.81			600.00
0+00				10.6	591.2
0+25				2.9	598.9
1+00				2.5	599.3
⊙			2.56		599.25
	4.20	603.45			
1+65				4.3	599.2
2+00				4.3	599.2
3+03.2				5.3	598.2
⊙			7.68		595.77
	4.73	600.50			
4+00				4.4	596.1
5+00				4.6	595.9
5+87				5.1	595.4
6+50				4.6	595.9
7+00				6.4	594.1
8+00				5.2	595.3
9+00				4.8	595.2
T.P. ⊙			3.81		596.69
	2.60	599.29			
10+00				3.4	595.9
11+00				5.3	594.0
12+00				6.0	593.3
12+50				5.1	594.2
13+00				4.5	594.9
	13.34		14.05		

On 8" Alder 8' Lt. Sta. 0+20 – Nail in tree.
Water Surface.
Top River Bank

Theoretical H.P. = $\frac{\text{Quan. in sec. ft} \times \text{fall in ft.}}{8.8}$

$\frac{70 \times 17}{8.8} = 136$ – Say 140 H.P.



Area = 40.5

A Float traveled 10 ft. in

1–	9"	5– 7".
2–	5"	6– 6"
3–	6"	7– 6"
4–	4"	8– 5"
		9– 6"
		10– 6"

10 – 62

Ar = 6.2 sec. time to go 10 ft.

$\frac{6.10}{1\frac{4}{6}} = 1\frac{2}{5}$ ft. sec.

Q = a × v

40.5 × 1.5 = 135

40.5
27.0
6 | 7.5 cu. ft. sec. – Q say 70 c.f.s.

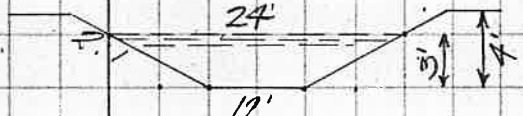
70 c.f.s. – 140 H. Power.

Levels for Riddle Light & Power Project.

Sept. 2-15
Frear
A. E. Brais.

Sta.	+ (13.34)	H. I.	− (14.05)	Rod	Elev.	
14+00		599 29		19	597 4	
			1 28		598 01	On 14+00
	5 24	603 25				
15+00				5 3	598 0	
15+31 3				5 2	598 1	Ft. Bank
15+60				0 9	602 4	top
16+00				1 1	602 2	
T.P.			0 10		603 15	On Top 16+00
	2 45	605 60				
17+00				4 5	601 1	
17+40 5				4 9	600 7	
18+00				5 2	600 4	
19+00				5 3	600 3	
20+06				6 0	599 6	
T.P.			5 05		600 55	
	0 67	601 22				
20+31				7 1	594 1	
T.P.			12 54		588 68	
	0 36	589 04				
20+81				6 1	582 9	
20+81					576 0	Probable Elev tail Race.
21+46				11 0	578 0	Water Surface
	22.06		33.02			

Grd. 0+00 = 593 90
" 20+00 = 592 50
fall per 1000' = 0.25'

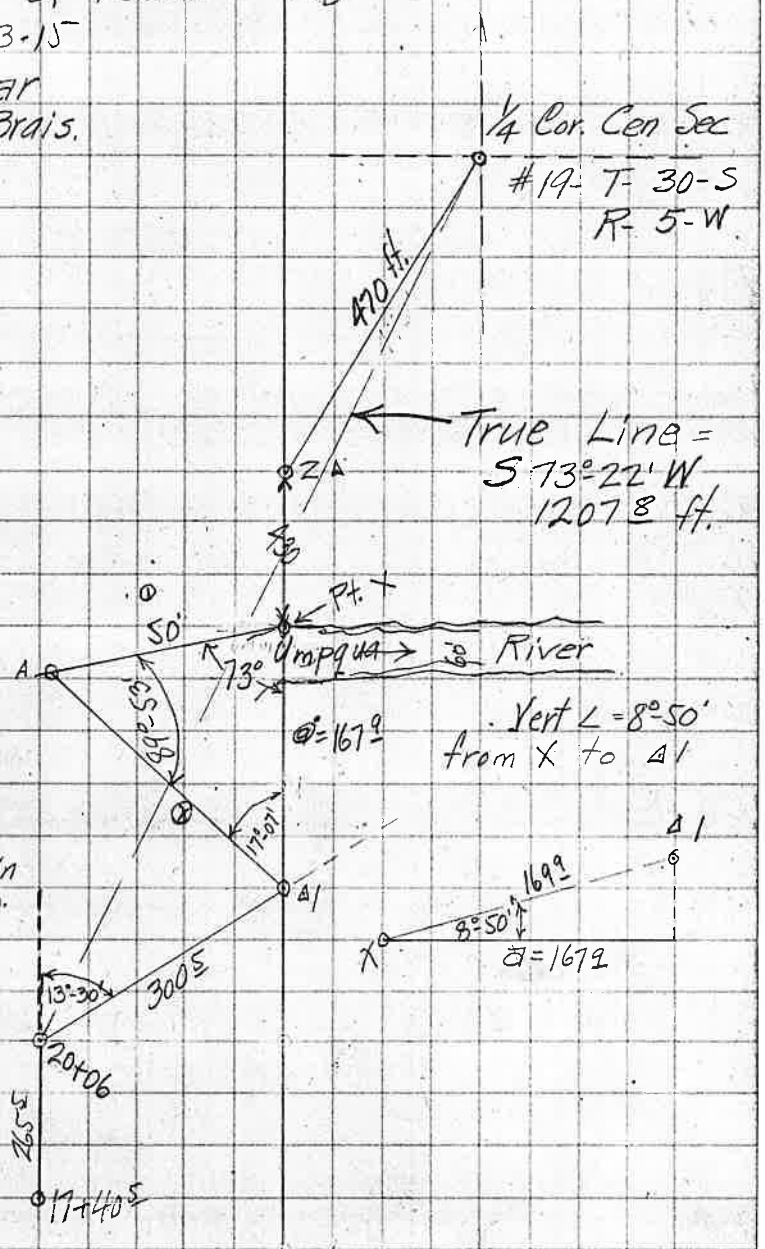


Type of ditch to be used.

Section Line Tie Random Line for Riddle Light & Power Project.

Sept. 3-15
Frear
A.E. Brais.

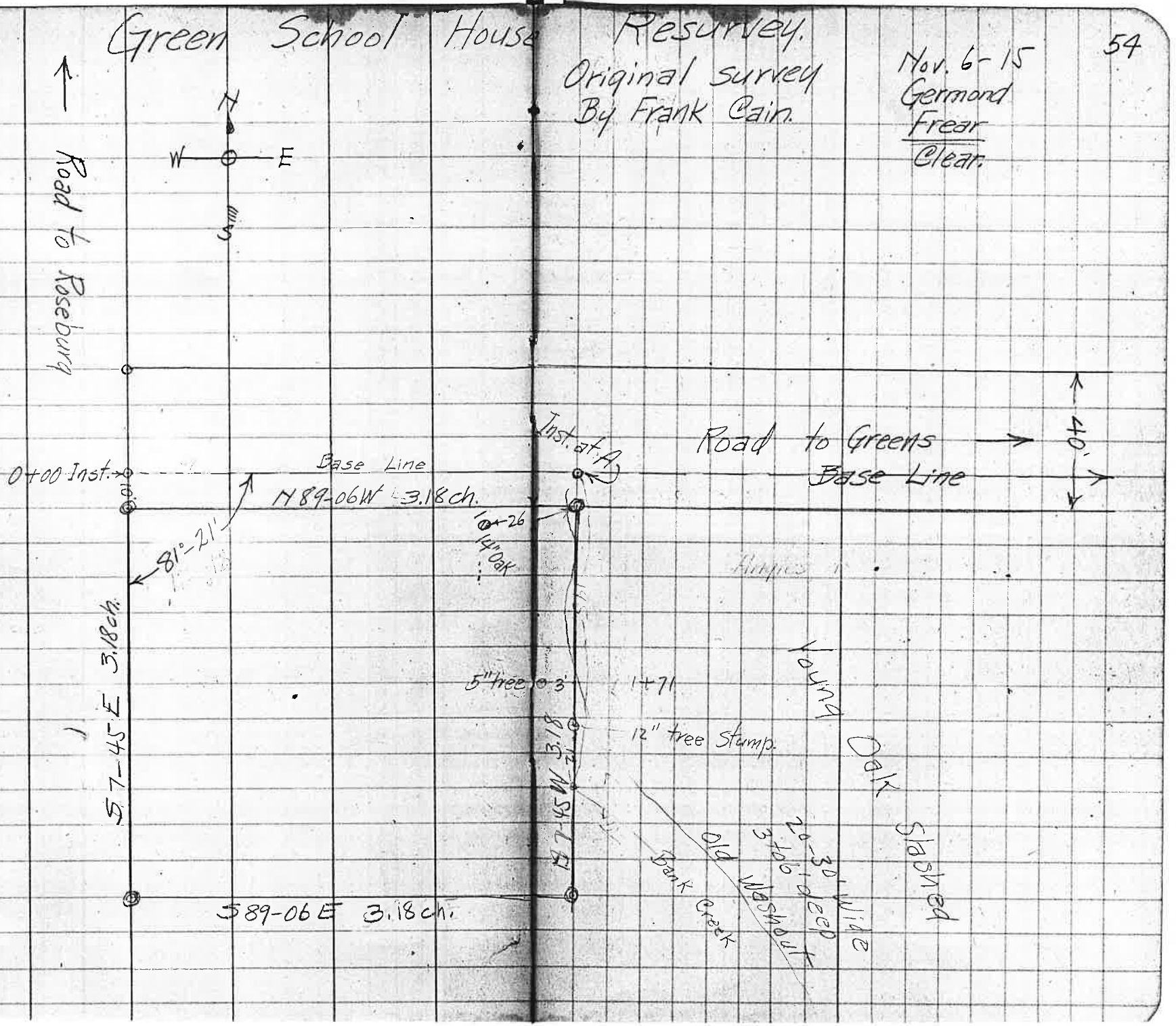
Sta.	Dist.	Lt.	Rt.	Mag.	Calc.
3 Δ = ¼ Cor. Center Sec. 19					
	470 ft.		24°-24'	S 73°-30 W	S 74°-11' W
2 Δ					
	5979	74°-18'		S 50°-30' W	S 49-47 W
1 Δ					
	300 ±		13°-30'	N 55-15 W	N 55-55 W
20+06 Powerhouse Site					
	265 ±			N 69°-15' W	N 69-25 W
17+40 ±					



Green School House Resurvey.

Original survey By Frank Cain.

Nov. 6-15
Germond
Frear
Clear.



Instrument at "A"

Point No	Dist. to Point	Angle Lt.	
5			
	61 8	102°-38'	12" Oak Stump. 2 Oaks 5' apart on Each Side
4			
	76 8	96°-39'	12" Oak Stump.
3			
	131 8	82°-00	30" Oak Stump.
2			
	171 8	81°-12	6" Stump. 3 ft. West.
1			
	183 8	81°-12	12" Stump

Inst at A. Limb at Zero on Base Line.

5			
	80 8	22-22	Oak Stump 40' in Diam.
4			
	128 8	42-03	Oak Stump 5ft. in Diam.
3			
	350 8	23-36	Creek 50' Wide
2			
	345 8	19°-30'	Creek 50' Wide
1			
	225 8	2°-20'	Creek 80' Wide.

Inst. at 0+00 Limb at Zero on base line.

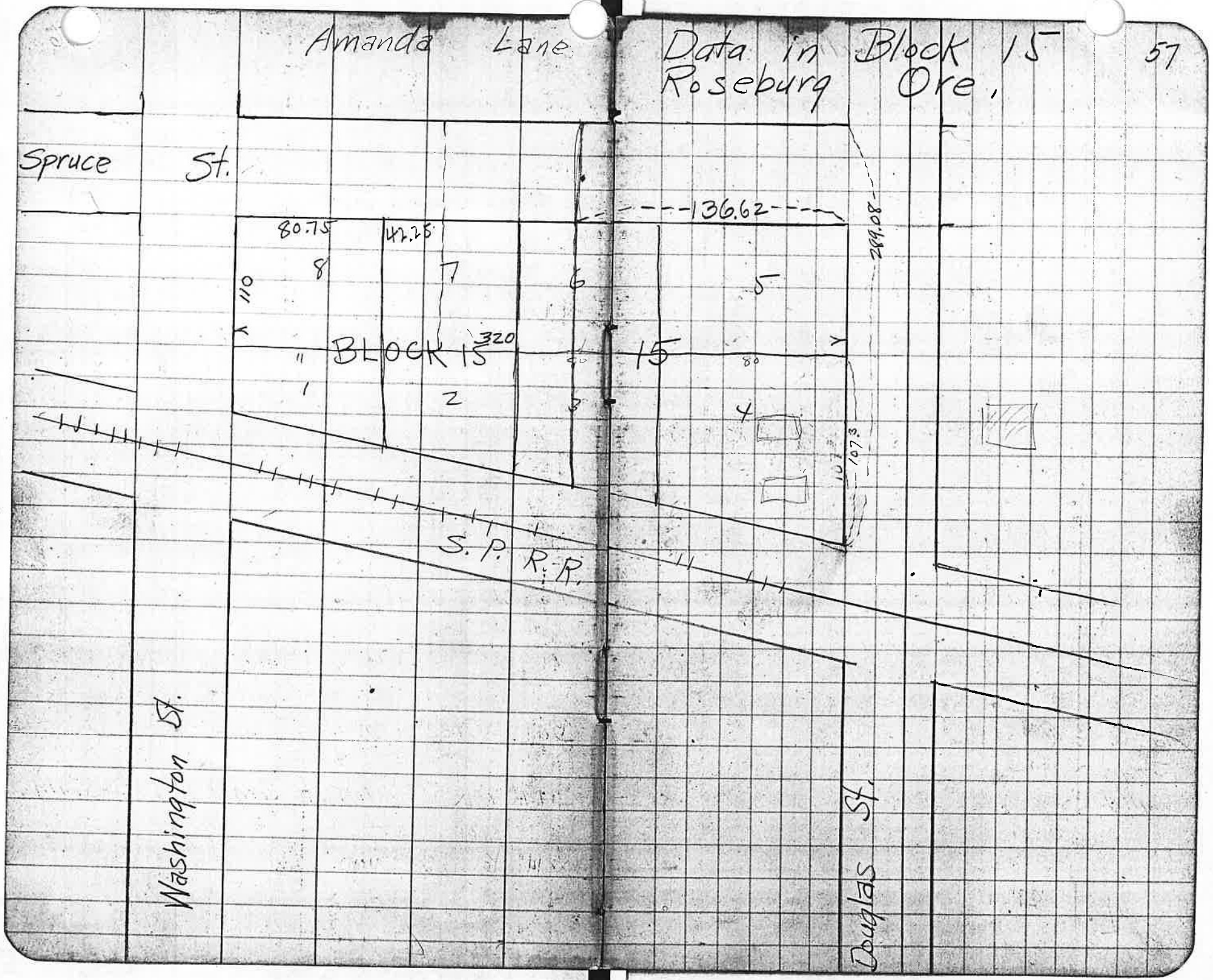
Inst. at "A" Limb at Zero on Base Line.

Const of Instrument 0.8 ft.

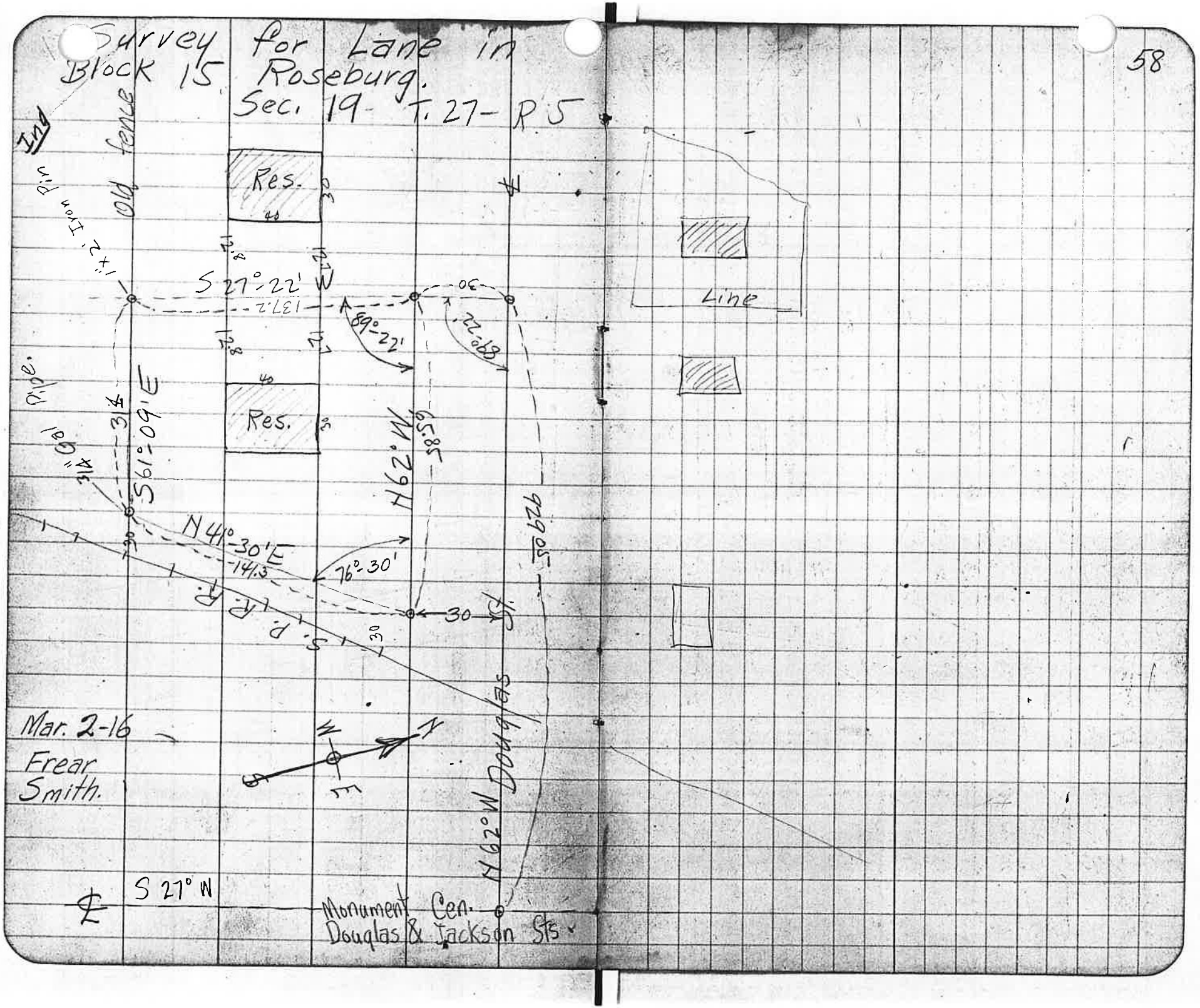
Point No.	Dist. to Point.	Angle Left.	
8			
	195	81°-12'	Bank Creek on East Line.
7			14" Oak 26' West of Corner & 1 ft. South.
6	48 ±	107°-25'	14" Black Oak Stump.

Amanda Lane

Data in Block 15
Roseburg Ore.



Survey for Lane in Block 15 Roseburg.
Sec. 19 T. 27 - R 5

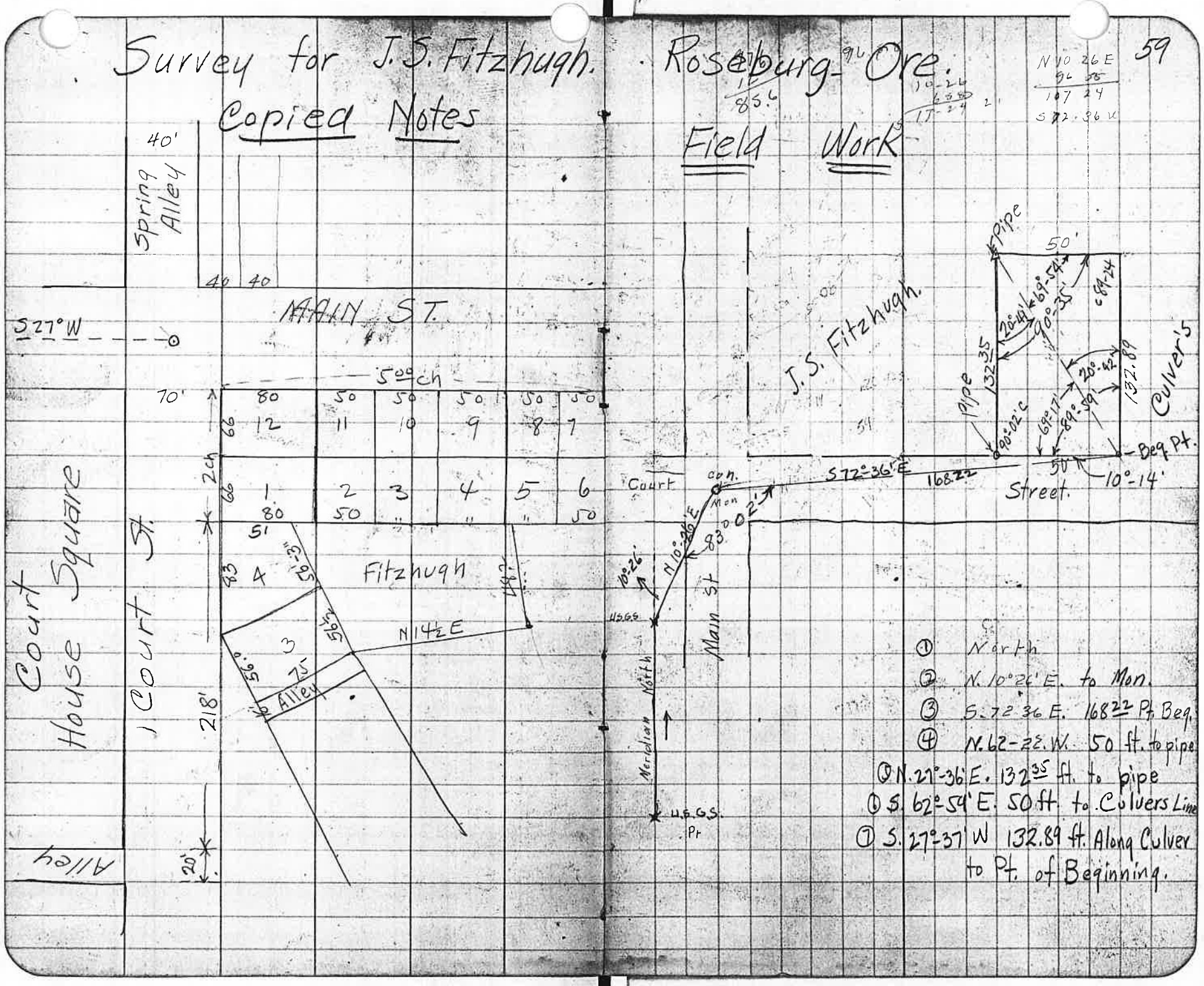


Survey for J.S. Fitzhugh. Roseburg Ore.

59

Copied Notes

Field Work



① North

② N. 10° 26' E. to Mon.

③ S. 72 36 E. 168 22 Pt. Beg.

④ N. 62 - 28. W. 50 ft. to pipe

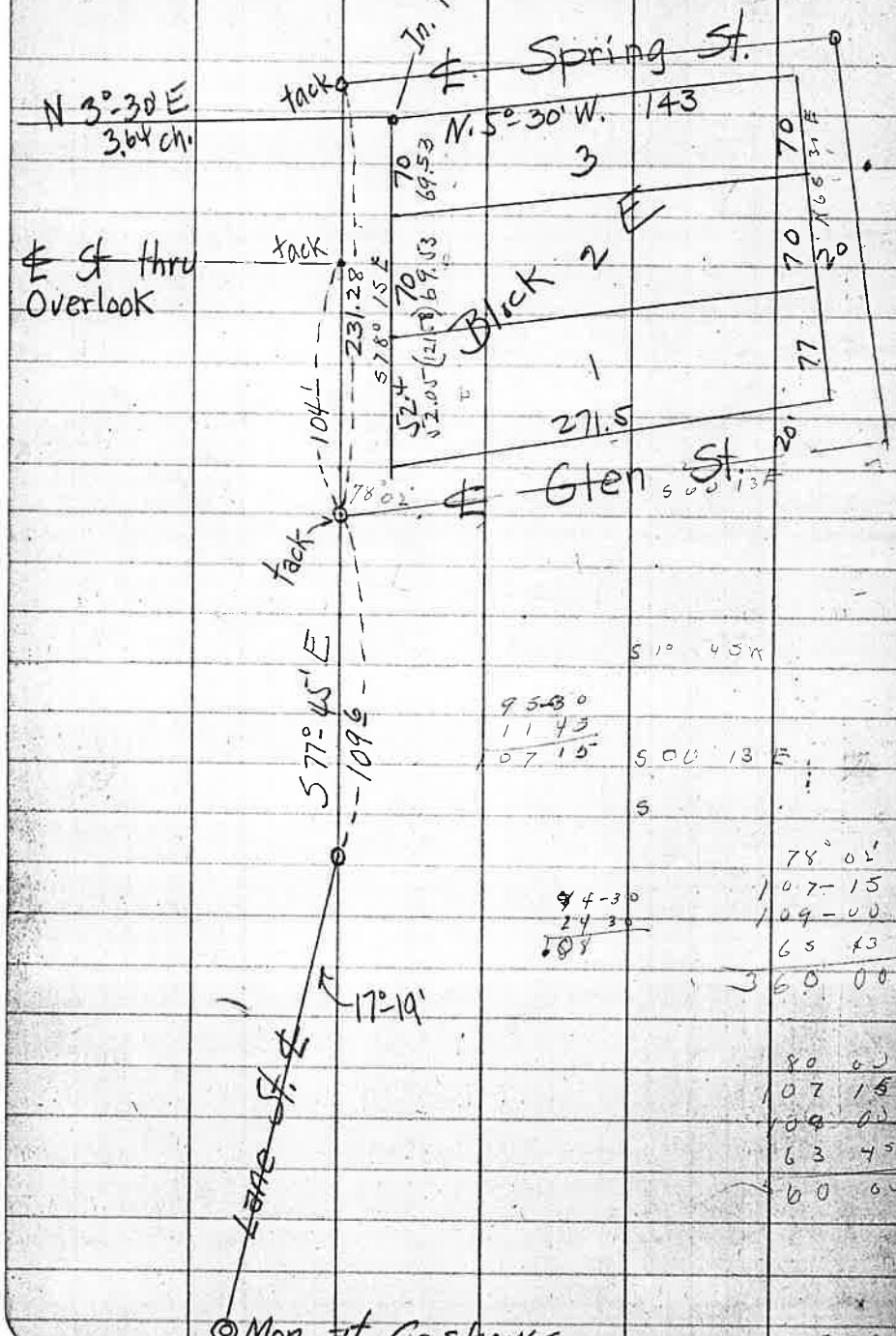
⑤ N. 27° - 36' E. 132 35 ft. to pipe

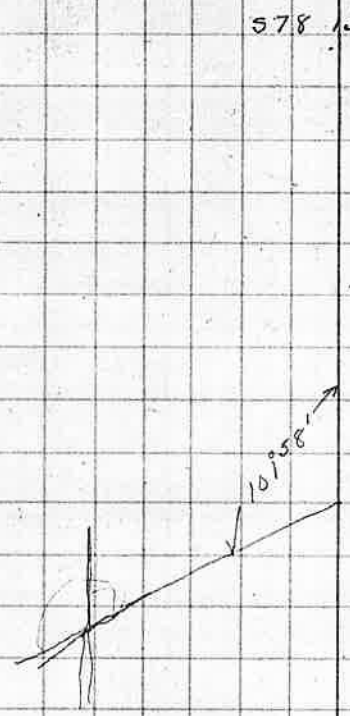
⑥ S. 62° - 54' E. 50 ft. to Culvers Line

⑦ S. 27° - 37' W 132.89 ft. Along Culver to Pt. of Beginning.

Field data on R.G. Hall Survey

60





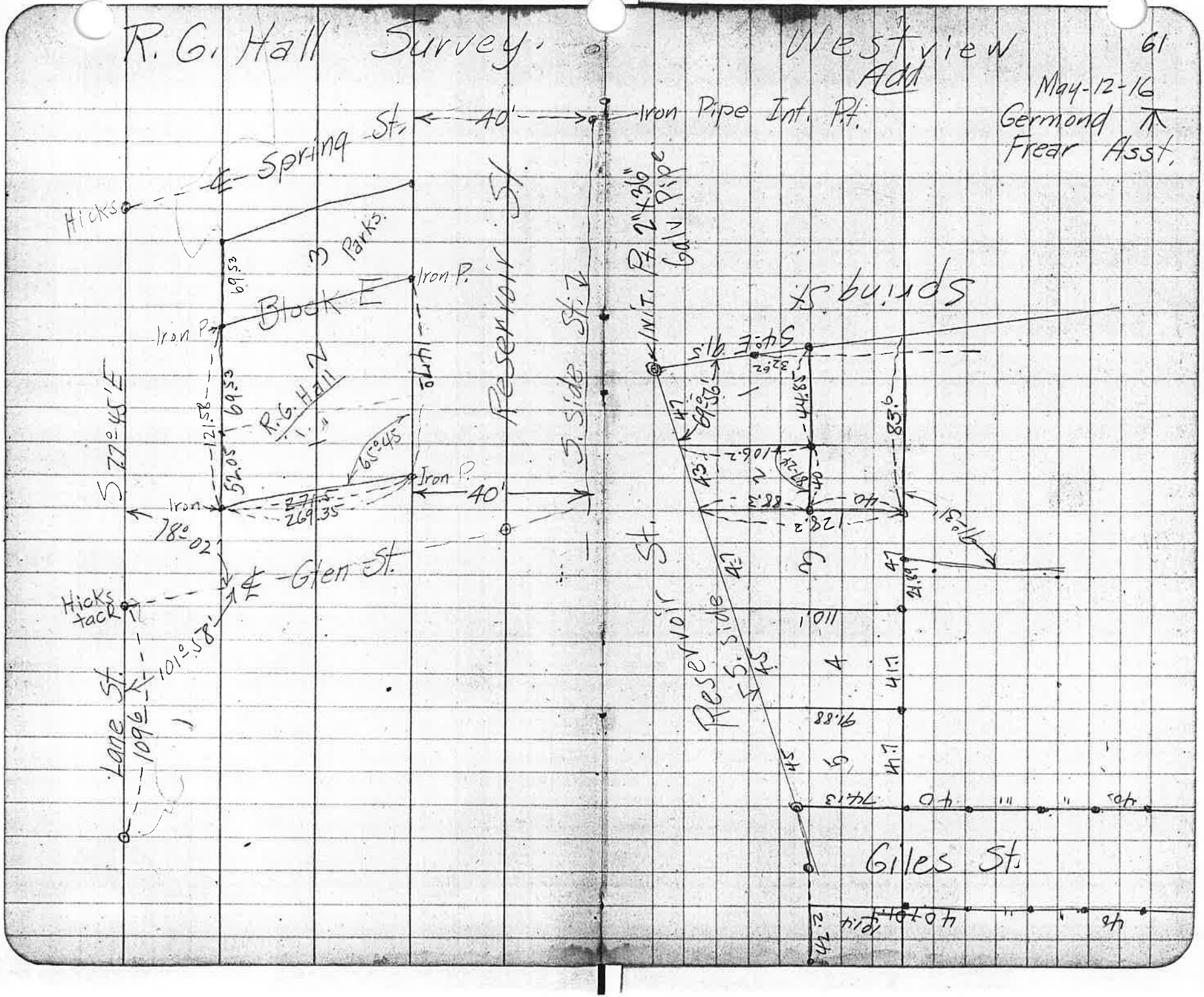
990127 2000000 (201
148037
1 19 2600
494187
972413 0

978268 2000000 (204
1956536
43464 00
3913072
433328 0

R. G. Hall Survey.

Westview Add

May-12-16
Germond
Frear Asst.



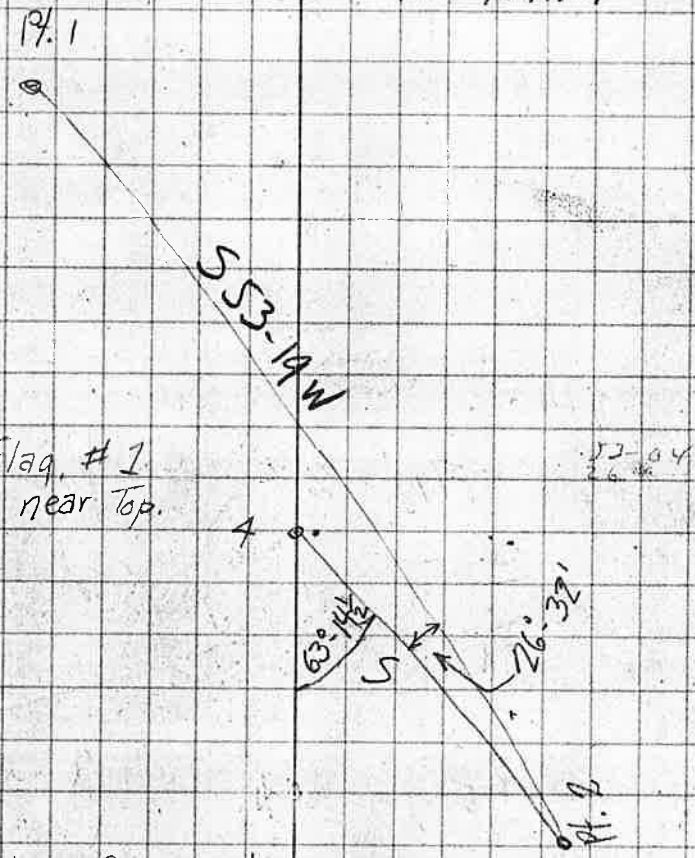
Oscar Lindsey Survey Feb. 2- 62
Rainy

Stg.	Dist	Lt.	Rt.	Needle	C.C.
9	On E. Side River				
8	On W. Side River				
7	on Rocky Pt. Flag #2 tripod ½ way down.				
6	On Rocky Pt.				
5					
Flag #1					
4	on Top Mt. Nebo				
3					
2					
1					
0 = Cor. J. Liesure D.L.C.					

Begin at John Liesure Cor. & Run East

for Triangulation
See Next Page

Frear ⊼
Oscar Lindsey
Al Hawn



Oscar Lindsey Survey
Onondaga River
Base 5.00
Pt. 9
Pt. 8
Flag #2
Flag #1
Pt. 10
Pt. 11
South
East.
29.10
9.36
6.14
8.63
14.33
14.00
Rod 11'+30"
Pipe
2"x4" Iron
N° 1
N° 2
24.13
21.16
15.50
12.76
99°-37½'
48°-36'
31°-46'
17°-06'
10°-12½'
121°-11½'
114°-18'
0.05

Oscar Lindsey Survey 2-2-17 64

Sta	Dist.	Lt.	Rt.	Mag.	C.C	
						49-09 130-51 179 60
						Frear ⊼ O. Lindsey Al. Hawn
12						
	3.195		01°-39'	S11½W	S12°-10'W	
11						200 ft. to ℄
	3.945	30°-20'		S10¾W	S 10°-31'W	
Pt. 10						200 ft. to ℄ River
	6.39 Chs		130°-51'	S41°W	S40°-51'W	
Pt. 8						On W. Side River
				S89½E	East.	

S89 57E 9.0
17 18 17

Set in for S.E Cor of Lindsey Land an Iron pipe
1½"x30" from which an ash 13" S 72 39E 63 lks
" " a maple 8" N 13°22' E .783.

S.E Cor of Cl. 53 John Lieser's 1¼ 2"x36" gal. pipe
from which 12" W. Oak bears N 71°38 W .66.25 lks
" " 4" Madrone Bs S 44 54 W .69.15 "
nail in

NW Cor. of Lindsey's place 15 1½"x24 Iron bar
from which 12" W. Oak S 3° 25 W .95.75 lks
" " 8" R fir S 74 50 E 28.00 "

N.E. Cor Lindseys place Set 2"x36"
Galv. Iron Pipe
from which 12" forked W. Oak S 46-07 W - 54.8 ch.
" " 15" B. Oak N. 86°-14' W. 85.5 ch.

Sec. Cor. 23-24-25-26 Gal. Iron
Pipe Set. 2"x36"
from which a 15" W.O. Bears N. 00°-10' E - 8.72 ch.
Set. Nail in above Exactly on Line.
A. 16" W.O. Bears S. 75°-00' W. - 4.355 ch.
A. 8" W.O. " S. 16°-07' E. - 3.88 ch

Lindsey's S.W Cor 15 1½"x48 gal iron pipe
from which a. B. Oak 14" Bs 21°30 E 64 lks
" " a W " 8" Bs 84.35 E 99½ "

54.8
66
3288
3288
3618
36.2

855 = 18
66
513
513
5643

Allan Hubbard Cl. 41
T. 25 - R 7

Beg. at N.E. Cor in Dec. 26 Set Post
a.B.O. 24" N. 1¾° E. 800 Lks.
a.B.O. 30" N. 8¼° W. 580 "

North On E. Bdy. Cl. 41
~~44~~ 80 N.W. Cor. Cl. 40
50.27 Intersect Line bet. 23 & 26 - 7.06 ch. W. of Cor. Sec. 23-24-25-26
52.02 Intersect N. BR. Ump. & Set Post for N.E. Cor. Cl. 41 - from which
a Maple 30" N 75° E. 105 Lks.
a " 24" S. 80° W. 268 "

Thence following Meanders of River
N. 82½° W. 13.06 ch
N. 76° W 20.60 " on N. Bdy Cl. 41
S. 80° W. 20.30 " Set Post
N.W. Cor. Cl. 41 & N.E. Cor Cl. 42
a.B.O. 24" E. 32° W 27 Lks
an Oak 24" N. 74½° E 22 "

South Ber. Cl. 41 & 42
5.00 Int. Line bet. 23 & 26 - 20 ch E. of Cor Secs 22-23-26-27
58.75 a Creek 25 Lks Course N.W.
66.50 Set Post S.W. Cor Cl 41
X an Oak 30" S 75° W 174 Lks
" alder 12" S 67° E. 142 "

East On E. Bdy Cl. 41
1.35 Creek 25 Lks Wide Course N.
11.46 Set Post Cor. Cl 41
a.B.O. 30" bears E. 80° W 1112 Lks
Only tree taken - Omission

North
11.00 Set Post for Cor
an Oak 30" N. 43° W 292 Lks
" " 15" N. 0°-30' E. 256 "

East 30.08 To beg. Corner.

K. W. Bradley

K. W. Bradley Cl. 42 4a
in T. 25 - R - 7 Cont 158.85
Beg at Meander Post which is
N. W. Cor. on Lt Bank S. Imp
2.75 chs N. of Cor. Sees 22-23-26-27
N. 83½° E. On Rt. Bank of River Up.
20.10 To N. W. Cor. Cl. 41
An Oak 24" D 32° W. 27 Lks
" " 24" N. 74½° E. 22 "
South On E. Bdy Cl. 42
5.00 Sub. Line bet Sec 23 & 26
20 ch E. of Cor 22-23-26-27
66.50 S. W. Cor Cl 41
80.60 Set Post S. E. Cor Cl. 42
a. B. O. 30" N. 76° E. 263 Lks
a. B. O. 30" N. 23° W. 165 "
West. On S. Bdy. Cl. 42
19.98 Intersect Line bet Sec. 26 & 27
4.25 chs N. of Cor Sees
26-27-34-35
Set Post for S. W. Cor. Cl. 42
& S. E. Cor Cl. 43 from which
a. B. O 36" bears N. 72° W 81 Lk
a. B. O. 15" " N. 85° E. 56 Lk

North On Line bet. 26 & 27 &
Cl. 42 & 43
35.75 ¼ Sec. Post
75.75 Cor. Sees 22-23-26-27
78.50 To Beg. Cor.

H. P. Comm Survey of Sec. 26 - (T 25-1)

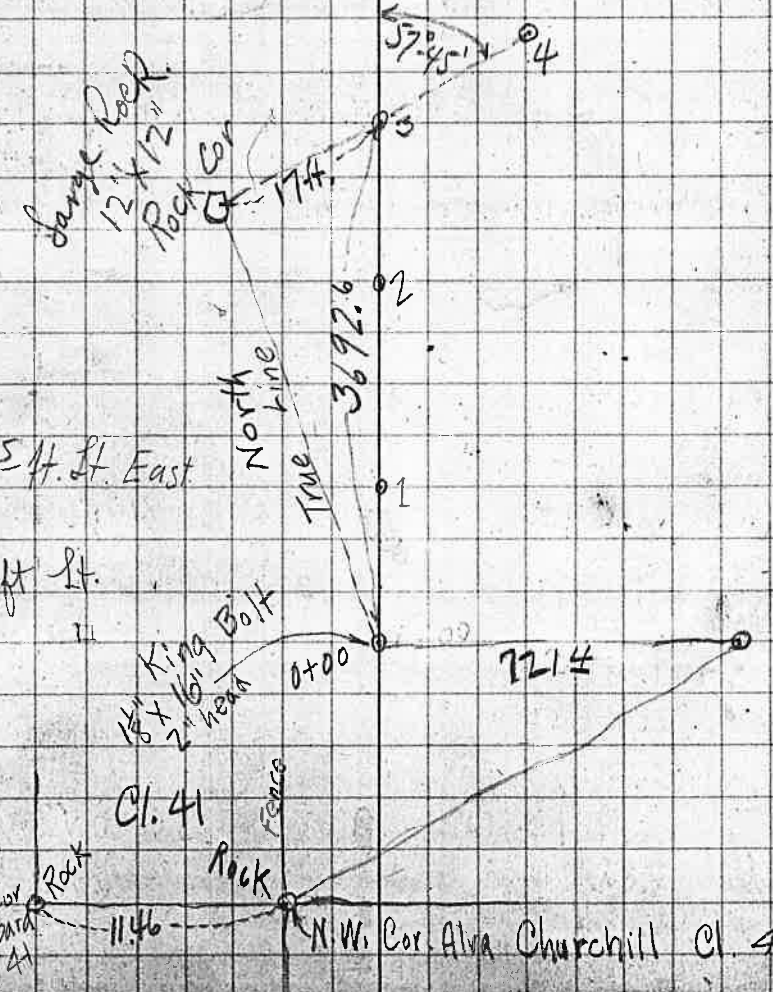
Coles Valley 1679 Mar. 7-17 68

3692.6 Rainy Frear ↑ Murphy Conn " "

Stg.	Dist.	Lt.	Rt	Mag.	
9					
	147±		84°-22'	S00½°W	S00-13W
8					
	157±		01°-42'	S83½°E	S84.09E
7					
	222±		6°-46'	S85½°E	S85-51E
6					
	219±	8°-34'		N88°E	N87-23E
5					
	95±		37°-57'	S84°E	S84-03E
4					
	44±		57°-45'	N58°E	N58°E
3					
				N00½°E	
2 P.O.T.	1667.8				
1 P.O.T.	2024.8			N00°-45'E	
0+00					

Fence

7 ft. West of fen & 10 ft. West of Cor. Iron Pipe



H. P. Conn Survey

Mar. 8-17 271.8
Very Stormy

69

Sta.	Dist	Lt.	Rt.	Mag	
N.E.Cor. is a ½"x 40" I.P. from which					
An 18" B.O. Bears N. 68° W — 13 ft.					
A. 20" B.O. " East. — 47 ft.					
S.E.Cor. is a 4"x8"x15" Rock from Which					
A. 40" B.O. Bears N. 3°-40' E. 60 ft.					
A 10" W.O. " N. 20°-45' W. 167 ft.					
S.W. Cor. is a 1⅛"x16" King Bolt with a 2" head					
from which					
A. 30" W.O. at the Gate Bears			S. 08°-00' W	123±	
1					
			90°-24'		N 00-14 E
0					
	721±		89°-37'	S 89° W	S 89-50 W
12 P.O.T.					
	607±				S 00-13 W
11 P.O.T.					
	1758±				
10 P.O.T.					
	1171±			S 00-30 W	S 00-13 W
9 P.O.T.					

Fence

Rock N.W. Cor Alva Church Ct.

Fence

Road

1" x 16" Germonds Pipe from which Bears N. 67°-31' W. 32.55 ch. from A. Church 11 D.L.C. 44 the N.E. Cor.

1117±

643±

40°-37'

37°-35'

89°-37'

721±

0

89°-36'

20'

90'

25'

4"x8"x15" Rock 4" deep.

16.7

12

True Line

11

1

10 10

10'

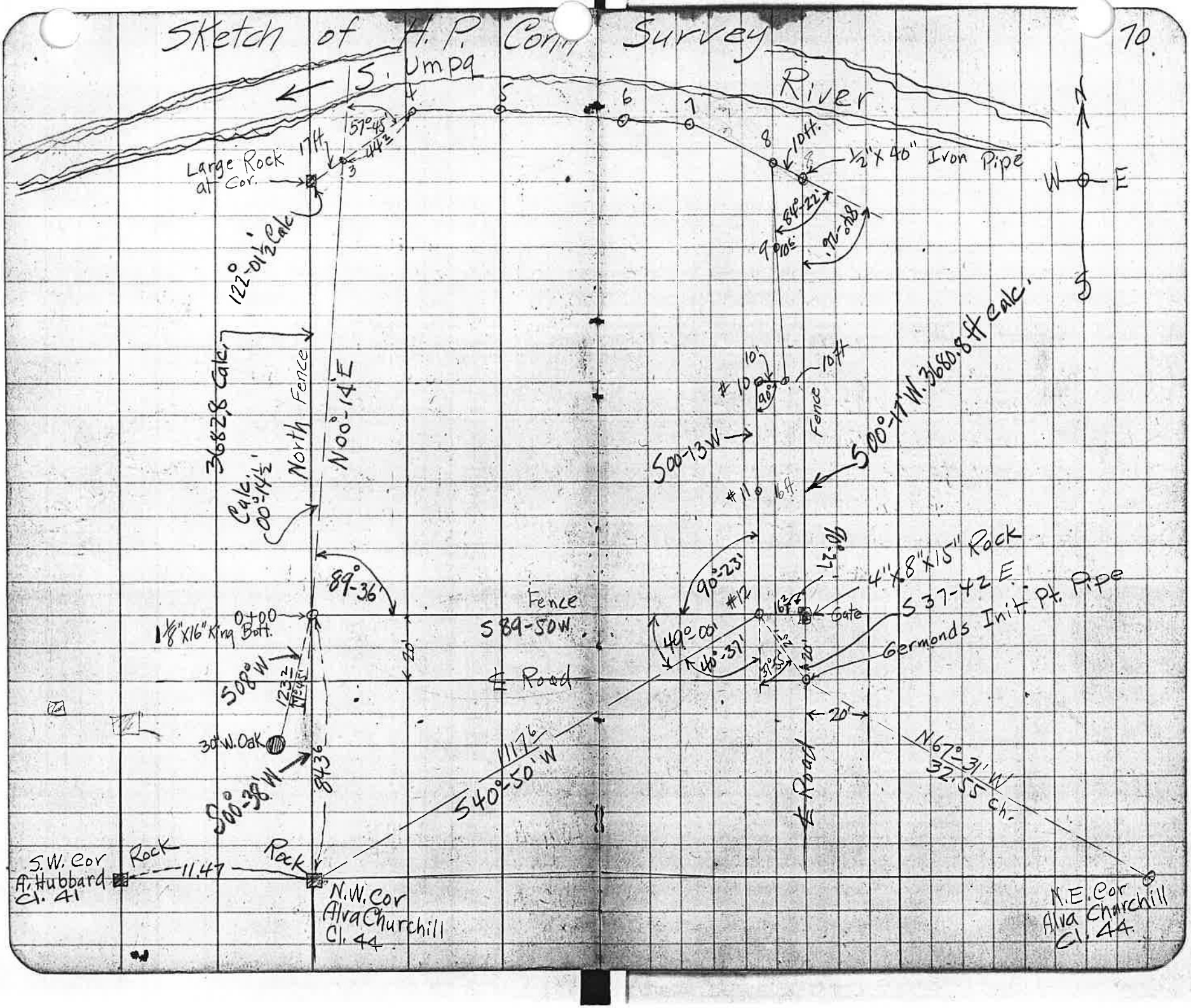
16 ft. W.

20 ft. W. - Offset 10 ft.

10± W. of

9

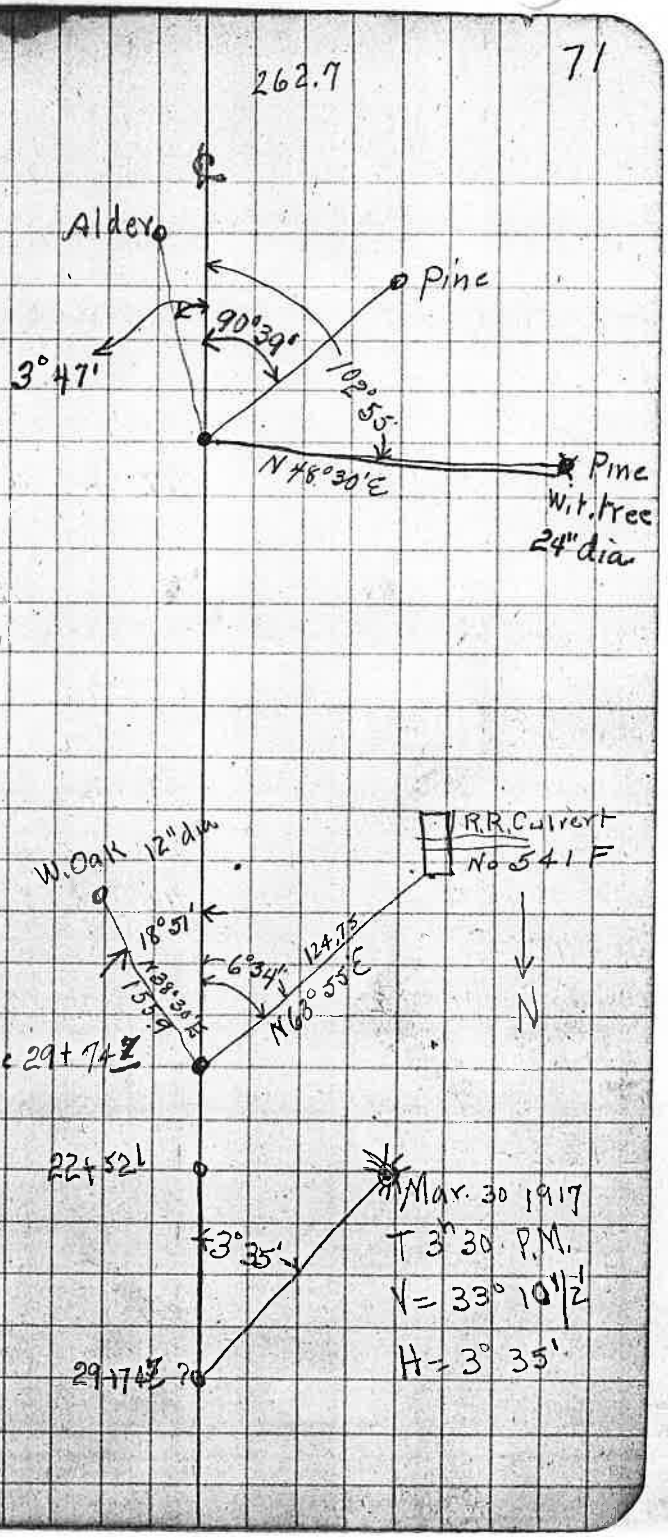
Sketch of H. P. Com'l Survey



Survey of The Ellinger & Smith Gateway Road

Began Survey at a pt. which is a 1"x1"x36" Iron Bar driven 32" deep and from which an alder tree
An Alder 16" dia brs. N59°W 150.85 ft.
a Pine 14" " " N35°40E 262.7 ft.
Thence N55°W 232.8 feet along ℄ of 16½ rt-of-Way Thence N5°00W 182.5 ft. to a pt 4 ft East of W. bdy of said rt-of-Way. Thence along a line that lies 4 ft East of the W. bdy. of rt-of-Way

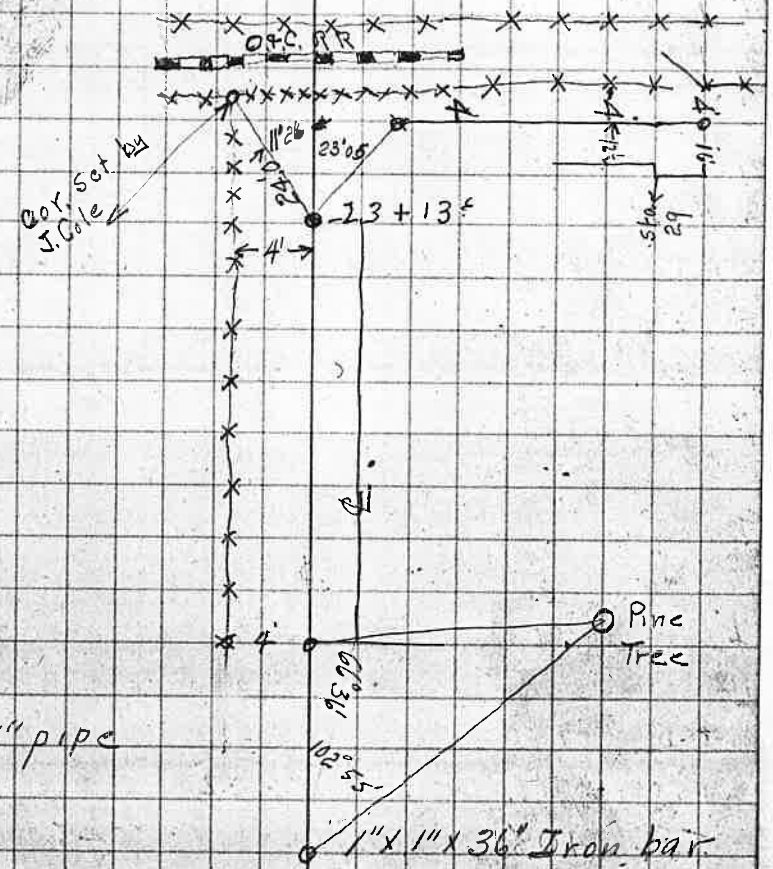
See Next Page



Survey of The Ellinger (Mynatt) to Smith Road

Ed. Weaver Viewer — C.L. Valentine Marker
Raymond " — Eddy " Axman
Clinton Helbig Chman
Ralph Johnson "

	Ang Rt	Ang Lt	Dist.	Need	T. Br.
29+74.7					
	27° 43'		722.6	N 37 10 E	N56°52E
22+52.3					
	23° 05'		38.5	N 29 40 E	N29 09E
22+13.6					
		00 08'	252.0	N 6°25E	N6° 04E
19+61.4					
	00 14'		661.6	N 7°15E	N6' 12' E
13+00					
	00 30'		487.8	N 6 25E	N5° 58 E
8+12.2					
	11° 02'		396.9	N 6' 00E	N5° 28E
4+15.3					
	49°25'		1825	N 5 00W	N 5 34W
2+32.8'					N
			232.8	N 55° 00W	5-4 59 W
0+00	0				
			2974.7		



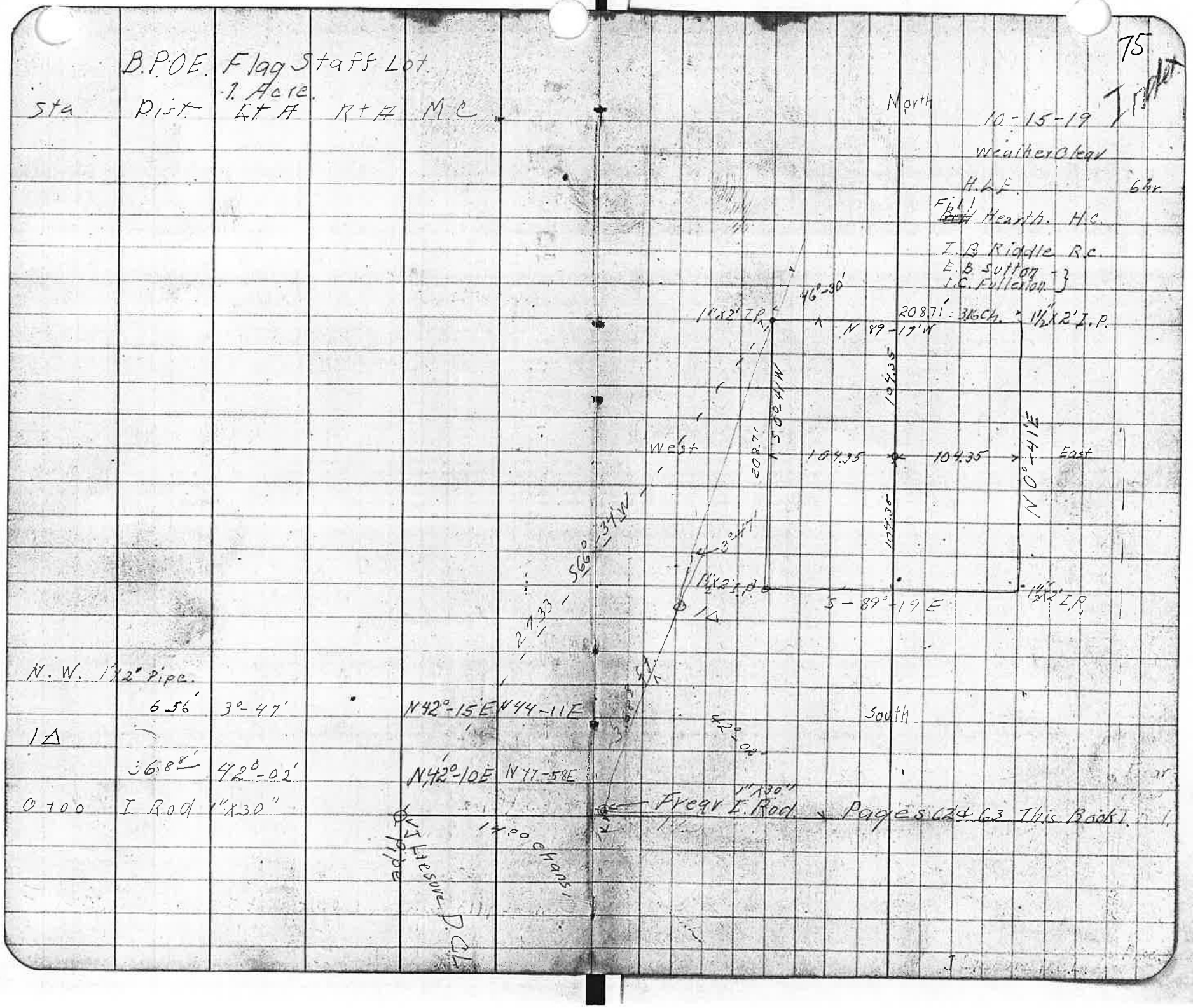
Levels on Ellinger – Smith Road of Base

0 + 00	6.00	106.00			100.00	
1 + 00			5.6		100.4	
2 + 00			4.4		101.6	
2 + 32			4.34		101.66	
3			3.4		102.6	
3 + 80			4.6		99.4	
4			1.6		104.4	
4 + 15			1.62		104.38	
T.P.	6.00	110.38		1.62	104.38	
5			3.2		107.18	
6			3.0		107.38	
7			4.5		105.88	
8			3.7		106.68	
9			6.0		104.38	Culvert here
10			9.0		101.38	
11			5.8		104.58	
12			8.0		102.38	
+25			6.0		104.38	Culvert here
+50			(-0.2)		110.58	
T.P.	10.81	120.71		0.48	109.90	
+75			0.5		120.21	
T.P.	10.55	130.97		0.29	120.42	
13			5.70		125.27	
14			4.1		126.87	

15		130.97				
15			3.8		127.17	
16			4.6		126.37	
17			5.5		125.47	
18			10.1		120.87	
19			7.6		123.37	Culvert here
20			4.0		126.97	
21			1.7		129.27	
T.P.	6.45	135.82		1.60	129.37	
22			4.4		131.42	
22 +13.6			4.11		131.91	
+52.1			4.9		130.92	
23			6.8		129.02	
24			8.6		127.22	
25			8.9		127.92	
26			10.0		125.82	
27			11.5		124.32	
28			16.0 ?		119.82	
T.P.	1.95	127.49		10.28	125.54	
28			7.9		119.59	
+35			8.4		119.09	culvert here
29			6.1		121.39	
+74.7			2.77		124.72	
			5.78		121.71	Cen. of 1913 sign on Culvert about top R.R. Cut 5+1. F

B.P.O.E. Flag Staff Lot.
1. Acre.

Sta	Dist	Lt A	Rt A	M C
N.W. 1½" Pipe.				
	6.56'	3°-47'		N42°-15E N44-11E
1 Δ				
	36.88'	42°-02'		N,42°-10E N47-58E
0+00	I Rod	1"x30"		



N.W. cor of Wm Wilson D.F.C. No 41 in Tp 30 6
post. from which a
B.O. 18" dia Ore S 3½° E 11.70
" " 24" " " S 00¼° W 12.60

Sec. cor for 33. 34 27 & 28
B.O. 18" N 58° W 193
Ash 4" N 28° E 167
Pine 20" S 6° W 371
Ash 18 S 61° E 538

JK H2502

Preliminary Estimates (Cain)
and
Bid or Contract Prices
Canyon — Creek — Road

	Amt	Pen	
Dirt Ex.	13746.92	0.24 per cy	3299.26
" Fill	5		
Rock Ex.	5339.13	1.00 " "	5339.13
" Fill			
Con. Culvert 41 Cy.	6'x 6" x 80 ft		820.00
Tunnel			
Big Fill			
2' pipe (Con.)	25	2.00	50.00
1' pipe (Con.)	366	1.00 per ft	366.00
Steel for Culvert			101.72
			$9976.11