Field Book # 59

DOUGLAS-COUNTY

1911

Date

F.B. 59.

No 4.

FIELD BOOK

59

605

1652
66
9924
9924
109 164
108 5
0

from Cin South 635
" 511'41'12 547

870
489
8.59

522
443
27) 79. (2
4

27
2
54

527
27
495

79
54
15

522
496
26

1327
2655

Pages for ms Barry

Index. Book No 4.

Name.	Sec or DLC.	Twp and Range.	Cor. Sec.	date	Page.
Elliott. E.W.	DLC. 51.	30-5		Nov. 7. 1911	2-3-4
Lonnigan. W.S.		29-4		Dec 1911	13-14
Puckett C.W.	Sec. 34.	28-4.		Dec. 5/11	7-8.
Riddle Water Sply.					17-To end of book
Schooldist 127		32-4		Nov 21/1911	5,6
White. J.C.	DLC 44	30-5		Dec 8/1911	9-12

Nov 7 1911

Survey for E W Elliott — Walter Gregory, Victor Shaw, Chainmen
H. S. Wilson - Marker

Beginning at a point — 50 west of SE Cor of J.G. Clark
D.L.C. #51 in Tp 30 S R 5 W

Thence West 16.34 chs to center of County Road
" N 8½ W 7.31 " along Center " " "
" East 16.44 " to lands of W. Cornutt-
" S 7¾ E 7.30 " along west line of " land to place of-
beginning Containing 11.85 acs More or less,

Beginning at a point 1.48 chs west and 7.23 chs North of-
the SE Cor of The J G Clark D L C #51, Tp 30 S R 5 W

Thence West 16.44 chs to point in Co Road
" N 8½ W 12.49 " " " along " "
" North 1.00 " " "
" East 16.52 " " " to land of W. Cornutt-
" S 7¾ E 13.40 " along " " " " to place of
beginning Cont 22. acres More or less

Same

Beginning at a point at a point 20.53 chs North and 3.28 chs West of the S E Cor of J G Clark D L C #51 Tp 30.5 R 5 W

Thence West 16.52 chs to point in Co Road
" North 2.35 " " Black oak 30" in dia
" N 11°50' E 3.38 " along lands of A P Gillett-
" East 15.01 " " lands of N Cornuth-
" S 7¾° E 5.72 " " place of beginning
Containing 9.02 acres more or less

Beginning at a point 26.19 chs North and 4.05 chs West of the S E Cor of the J G Clark D L C #51, Tp 30.5 R 5 W

Thence West 15.06 chs to land of A P Gillette
" N 11°50' E 6.90 " along land of " "
" North 6.35 " to N E Cor of I.O.O.F Cem.
" East 12.48 "
" S 7¾° E 11.25 " " place of Beginning.
Cont 15 acres more or less

5

Nov 21 1911

Survey for School Dist - 127

Geo. Cheney and Ed Olinghouse - Chainmen. - F. A. Pierce - Marker -

Beginning at a point 1138 ft East and 1326.4 South of the center of Sec 33 Tp 32. R 4 W var 21° 05' E

Thence East 5733 ft to place of beginning

"	N 29° E	262.
1	S 61° E	185 "
"	S 29° W	62 "
1	S 58° W	112 "
"	S 80 3/4° W	159 "
"	N 31 1/2° E	181 "
	N 29° E	51.2 "

7 4

569
17
586
8
594

529
4.3
533.3

Dec. 5 1911

Survey for C.W. Puckett.

Beginning at a point 20.18 chs. East and 6.54 chs North of the S.W. Cor. of Sec 34 Tp 28S. R4W

Thence	N.82°E	1.37	chs.
"	S.88°E	2.43	"
"	N.41°E	2.78	"
"	S. 81°45'E	1.69	"
"	S. 55°30'E	3.64	"
"	N. 38°45'E	2.65	"
"	S.81°30'E	2.33	"
"	S57°30'E	3.92	"
"	N.74°45'E	1.58	"
"	N25° E	1.52	"
"	North	6.50	"
"	S74°30'W	7.92	"
"	S78°45'W	11.24	"
"	N 89° W	1.04	"
"	South	8.55	" to place of beginning Cont 8.98 acs.

Also for Road purposes only A strip of land 10 feet wide on each side of the center line described as beginning at a point 20.18 chs East and 10.24 chs North of the SW Cor of Sec 34 Tp 28-4

Thence	S89° E	1.04	chs
"	N 78°45'E	11.24	"
"	N 74°30'E	7.92	"

Dec 8 1911

Survey for John C White

Beginning at a point in Center of Co Road

Thence South Var 21°35'E

11294.0 − 1.8
1200' to point 24ft East of Fence var should be 20°27'E

S82°52'E
S81°53'E + 1°9 = 80°18' (82°36') at 430' Drain C N21°E (for 150 then westly) 1000' to Creek

15446.5 − 6.1 = 15405 − 4 = 15365

N0°1'W
N0°45'E 14232 + 1.8 S002

S87°38'W
S88°39'W N84°24'W 1379.8
N83°23'W N84°22'W 160.7
150.7

Beginning at a point 18ch West and 10.5' South of the SE Cor of Wm H Preston DLC #44 Tp 3 S R 5 W var 20°45'E

Thence S88°40'W 1380.0

" N83°23'W 160.7

" South 1293.4

" S81°53'E 1535.0

" N0°45'E 1524.0 to place of beginning Cont 49.12 acs

81-9
10
82-8

Paid Mrs Kimmel Board 2.60

" " Parker 1.00

" " " 2.60

30 acs

1368
315
1399.5

13798
838
541.8
780
239.8

8810
44
8726
53

get blue print 30-5 for each

10.5

Wilson + Cole 4 days each

North	1368 +31.5	to pnt abt 100 ft fm Left bank of Riv — var 21° 11'E —
East —	400	
S 70°25'E (30)	234.1 ✓	
S 84°25'E (75°15')	401.0	
South	1189.0	
S 88°05'W (10')	838.8	
S 85° W (84°55')	168.	

Beginning at a point 553.5 west and 23.0 South of the SE Cor of the W Preston DL C 44 Tp 30 S R 5 W var 21°11'E

Thence	S 88°40'W	844 ft	
"	N 83°23'W	160.7 "	
"	North	140. "	
	East	395 "	
	S 70°30'E	234.1 "	
	S 75°15'E	401.0 "	
	South	1220 "	to place of

Cont 31.12 acs

13 Dec 14

Survey of 40 acs for W S Lonnigan

Beginning at a point 7.57 chs West of the Cor of Secs 7, 8, 17 & 18 Tp 29-21

Thence S 25°45' W 12.36 chs
" East 37.15 "
" North 11.48 "
" West 32.57 " to place of beginning Cont 40.019

Correction for above
S 25°45' W 12.86 chs
East 37.65 "
North 11.58 "
West 32.07 Cont 40.3 acs

South line Secs 17 & 18 29-21
1.70 North myrtle Creek 20 lks E 6 lks
5.50 Enter [illegible]
40.00 1/4 post
Found 10" S 60 W 26
" 6 N 37 E 39

15 Dec 1911

Survey for ET Meese

Beginning at a point 15.00 chs west of ¼ sec Cor between Sections 17 and 18 T 29 S R 4 W

Riddle Water Supply.

Sta	+	X	−	R.	E	
B.M.	2.07	707.07			705.00	U.S.G.S. B.M. Riddle, Ore
△				4.62	702.45	Top of curb at E. line of Bank
⊙	0.96	700.40	7.63		699.44	
△				3.95	696.45	Top of Curb at Harness Shop
⊙	6.13	696.86	9.67		690.73	
△				3.31	693.55	Top of sidewalk curb 10' E. of Concrete gate post
⊙	1.48	686.58	11.76		685.10	
⊙	−0.02	674.63	11.93		674.65	
B.M.				4.56	670.07	On East Approach of Cow Cr. Bridge
⊙	5.32	677.26	2.69		671.94	
⊙	5.48	678.14	4.60		672.66	
⊙	8.84	686.98	0.00		678.14	
△				11.82	675.16	Pt. in Road.
⊙	11.06	698.04	0.00		686.98	
⊙	11.77	709.81	0.00		698.04	Pt. in Road
⊙	11.60	721.41	0.00		709.81	
⊙	11.44	732.85	0.00		721.41	
⊙	11.34	744.19	0.00		732.85	
⊙	8.17	752.36	0.00		744.19	
⊙	11.26	763.62	0.00		752.36	
⊙	11.49	775.11	0.00		763.62	
⊙	11.67	786.78	0.00		775.11	
⊙	11.98	798.76	0.00			
⊙	11.99	810.75	0.00			
⊙	11.89	822.64	0.00			

778.27
20
758.27
757.
.67

Sta	+	N	−	R	E	
		822.64				
0	11.70	834.34	0.00		820.64	
0	11.01	845.35	0.00		832.34	
0	10.79	856.14	0.00		843.35	
0	11.15	867.29	0.00		854.14	
0	11.92	879.21	0.00		865.29	
0	11.84	891 889.05	0.00		877.21	
0	11.45	902.50	0.00		889.05	
0	10.69	913.19	0.00		900.50	
0	11.96	925.15	0.00		911.19	
				3.06	922.09	B.M. B.O. 4" diam.
0	9.82	928.82	6.66		919.00 923.15	
0	7.87	929.22	7.47		921.35	
0	3.36	929.50	3.08		926.14	
0	5.54	928.66	6.38		923.12	
0	4.55	934.46	1.75		926.91	
B.M.				4.13	927.33	Laurel Reservoir Site.

922.

Sta	+	T	−	R.	E.	
0	3.02	678.18			675.16	
⊙	7.56	679.90	5.84		672.34	
5+39				6.7	673.2	= 2+83
6				5.9	674.0	
7				5.4	674.5	
8				6.1	673.8	
9				6.2	673.7	
10				7.5	672.4	
10+82				6.2	673.7	
11				6.3	673.6	
12				4.4	675.5	
13				2.1	677.8	
14				5.0	674.9	
15				5.0	674.9	
⊙	6.12	682.55	3.47		676.43	
16				5.8	676.7	
17				7.0	675.5	
18				6.9	675.6	
19				6.7	675.8	
20				5.7	676.8	
21				5.2	677.3	
22				2.6	679.9	
+40				3.6	678.9	Mouth small creek
⊙	9.16	690.95	0.76		681.79	
B3	4.76			7.9	683.0	

Sta	+	=	−	R.	E	
24		690.95		4.9	686.0	
25				1.7	689.2	
26				4.4	686.5	
27				1.2	689.7	
27 + 20				4.9	686.0	Bottom Small Creek
⊙	9.92	700.19	0.68		690.27	
28				7.9	692.3	
29				4.7	695.5	
30				1.8	698.4	
⊙	7.11	706.75	0.55		699.64	
B.M.				7.33	699.42	On B.O. 26" diam 14' L of Sta 30+17
31				6.1	700.6	
32				6.2	700.5	
33				5.0	701.7	
34				3.5	703.2	Sta 33+50 opposite Cains House
35				2.4	704.3	
36				3.7	703.0	
37				8.1 7.8	698.6	
⊙	2.09	701.52	7.32		699.43	
38				10.00	691.5	
+ 90				12.2	689.3	Bottom of small Creek
39				10.0	691.5	
40				1.8	699.7	
41				1.0	700.5	
⊙	6.74	707.29	0.97		700.55	

Sta.	+	X	−	R	E	
42		707.29		5.7	701.6	
43				3.4	703.9	
44				3.1	704.2	
45				3.6	703.7	
46				7.9	699.4	
47+				11.6	695.7	
48				5.0	702.3	
⊙	4.22	706.49	5.02		702.27	
49				1.8	704.7	
50				6.8	699.8	
⊙	4.88	699.73	11.64		694.85	
51				8.1	691.6	
+30				12.5	687.2	Bottom small Creek
52				10.4	689.3	
53				6.9	692.8	
54				2.1	697.6	
55				1.8	697.9	
⊙	10.33	708.93	1.13		698.60	
56				5.0	703.9	
57				3.1	705.8	
58				4.5	704.4	
59				6.9	702.0	
+75				9.5	699.4	Draw
60				7.4	701.5	
⊙	9.12	717.25	0.80		708.13	

Sta	+	x	-	R	E
61		717.25		7.5	709.7
+31				7.0	710.2
62				4.9	712.3
63				3.9	713.3
64				2.5	714.7
℄	9.32	724.36	2.21		715.04
65				7.4	717.0
66				6.1	718.3
B.M.				4.12	720.24
67				4.7	719.7
68				1.9	722.5
℄					
B.M.	8.36	728.60			720.24
69				4.7	723.9
70				4.4	724.2
71				2.2	726.4
72				0.9	727.7
℄	5.00	732.95	0.65		727.95
73				3.5	729.4
74				4.4	728.5
75				7.0	725.9
76				7.1	725.8
77				5.1	727.8
78				2.4	730.5

On laurel 10' R. Sta 66+66

Sta	+	X	−	S	E
		732.95			
0	11.73	742.55	2.13		730.82
79				9.6	733.0
80				7.3	735.3
81				4.7	737.9
82				3.1	739.5
83				1.8	740.8
0	10.23	751.56	1.22		741.33
84				8.6	743.0
85				5.6	746.0
86				2.1	749.5
0	11.32	761.75	1.13		750.43
87				8.5	753.2
88				2.9	758.8
0	10.65	772.40	0.00		761.75
89				4.7	767.7
0	11.30	783.70	0.00		772.40
90				5.1	778.6
0	7.92	791.62	0.00		783.70
91				4.8	786.8
92				3.4	788.2
93				4.8	786.8
+50				7.8	783.8
94				6.6	785.0
BM				1.92	789.7
95				6.5	785.1
96				0.2	791.4

Draw

B.O. 6" 15' L. Sta 92 +60

31

	+	= 791.62	−	R	E	
⊙	11.57	803.19 ✓	0.00		791.62	
97				2.4	800.8	
⊙	5.08	808.27 ✓	0.00		803.19	
98				2.7	805.6	
99				2.2	806.1	
100				7.2	801.1	Draw
101				4.1	804.2	
102				3.6	804.7	
103				1.6	806.7	
⊙	11.29	819.56 ✓	0.00		808.27	
104				10.9	808.8	
105				8.7	810.9	
106				3.4	816.2	
⊙	11.71	831.27 ✓	0.00		819.56	
107				5.6	825.7	
⊙	7.67	838.94 ✓	0.00		831.27	
108				5.6	833.3	
109				1.0	837.9	
110				6.1	832.8	
111				7.5	831.4	
112				9.4	829.5	
⊙	2.77	837.14 ✓	4.57		834.37	
113				2.0	835.1	
114				6.9	830.21	
115				9.5	827.6	

32

Sta	+	X	−	R	E
		837.14			
⊙	1.85	827.20 ✓	11.79		825.35
116				4.3	822.9
117				12.6	814.6
⊙	0.35	815.57 ✓	11.98		815.22
118				6.2	809.4
B.M.				6.75	808.82
119				9.4	806.2
120				9.2	806.4
121				5.4	810.2
⊙	8.27	823.84 ✓	0.00		815.57
122				8.0	815.8
123				5.8	818.0
+60				11.5	
~~+50~~				~~12.5~~	812.3
124				5.1	818.7
+47				3.0	820.8
125				4.9	818.9
+25				9.0	814.8
126				0.3	823.5
⊙	11.28	835.12 ✓	0.00		823.84
127				10.4	824.7
128				8.4	826.7
129				2.9	832.2
⊙	9.52	844.64 ✓	0.00		835.12
130				7.7	836.9
131				6.7	837.9

W.O. 16" St. @ 117 + 60

Drain

Sta	+	X	−	R	E	
132		84464		4.1	840.6	
133				1.6	843.0	
⊙	8.23	852.87	0.00		844.64	
134				6.6	846.3	
135				4.4	848.5	
+61				7.4	845.5	
⊙	0.99	846.59	7.27		845.60	
136				9.8	836.8	
+25				12.3	834.3	Bank of Draw
+30				17.0	829.6	In Draw
+35				12.4	834.2	Bank of Draw
137				1.0	845.6	
B.M.	5.90	851.69	0.80		845.79	4" W.O. near Sta 137+05 (18' R.)
138				5.0	846.7	
⊙ +50				3.6	848.1	
⊙	8.32	860.01	0.00		851.69	Conglomerate point
139				3.0	857.0	
⊙	0.58	850.29	10.30		849.71	139+60
139+60				5.1	845.2	
140				5.5	844.8	
141				3.0	847.3	
⊙	11.34	861.63	0.00		850.29	
142				9.5	852.1	
143				4.8	856.8	
144				1.5	860.1	
⊙	11.71	873.34	0.00		861.63	
145				10.2	863.1	

Sta	+	x	−	R	E	
146		873.34		7.9	865.4	
+15				11.2	862.1	Draw
147				4.0	869.3	
+60				6.9	866.4	Draw
148				4.2	869.1	
149				3.4	869.9	
150				0.1	873.2	
⊙	9.50	882.84	0.00		873.34	
151				7.3	875.5	
152				4.9	877.9	
153				2.1	880.7	
⊙	10.94	893.78	0.00		882.84	
154				10.8	883.0	
155				5.5	888.3	
+26				4.1	889.7	
156				4.9	888.9	
157				1.9	891.9	
⊙						
⊙	7.32	901.10	0.00		893.78	
158				6.1	895.0	
159				0.9	900.2	
⊙	8.70	909.80	0.00		901.10	
160				6.1	903.7	
161				8.2	901.6	
162				7.6	902.2	

39

Sta	+	℄	−	R	E	
		909.80				
⊙	9.05	910.99	7.86		901.94	
B.M				3.82	907.17	Alder 20" 10' R. Sta 162+85
163				0.3	910.7	
⊙	9.97	920.96	0.00		910.99	
⊙	4.03	922.06	2.93		918.03	
⊙	10.98	933.04	0.00		922.06	
⊙	11.88	940.97	3.95		929.09	T.P. in bed of Crk.
⊙	7.99	948.96	0.00		940.97	
⊙	6.72	955.68	0.00		948.96	
				8.2	947.5	
B.M				7.81	947.87	✓ 24" Alder

40

Cross Section of Creek at Dam

41

42

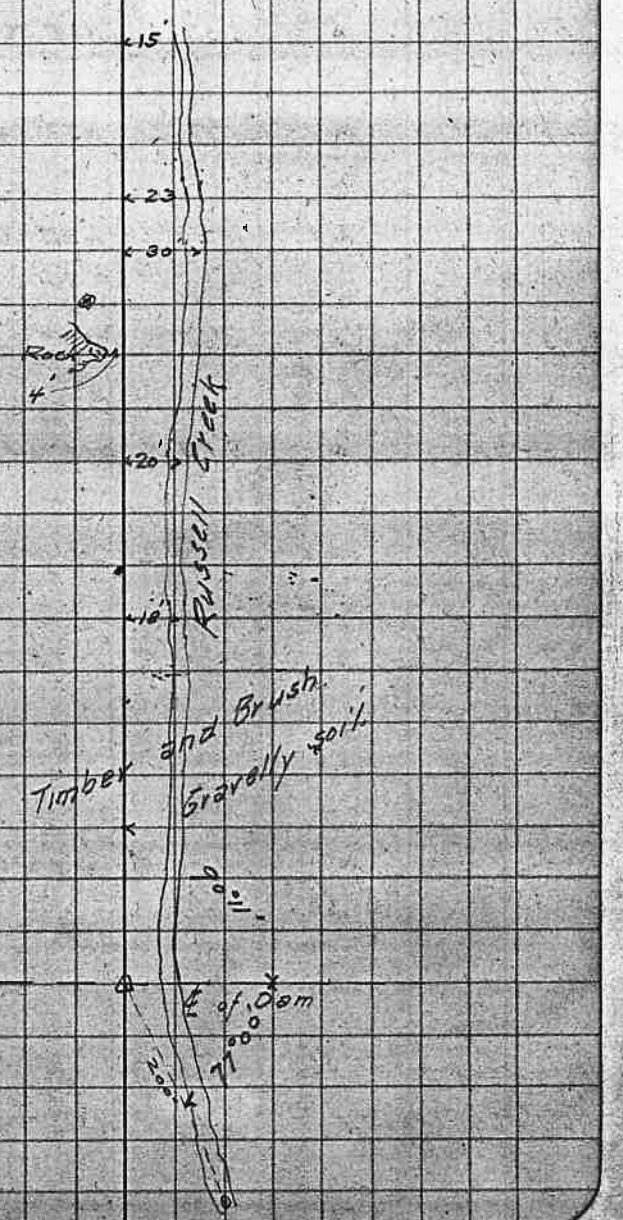
Sta	+	=	−	R	E	
B.M.	9.00	956.87			947.87	Alder near Damsite
0				4.6	952.3	Sta 178+31
0+13 R				7.0	949.9	
0+27 R				9.45	947.42	Water Edge
0+38 R				10.2	946.7	In Water on Bottom
0+47 R				11.8	945.1	
0+50 R				5.35	951.57	High Water
0+57 R				0.00	956.9	
0+45 L				4.00	952.9	
0+52 L				0.00	956.9	

Sta	+	H	−	R	E	
B.M.	9.00	956.87			947.87	
178+31				4.6	952.3	
178				5.9	951.0	
177				9.9	947.0	
⊙	2.13	947.42	11.58		945.29	
176				2.4	945.0	
175+31				5.0	942.4	
175				6.4	941.0	
174				7.8	939.6	
173				11.6	935.8	
⊙	4.86	940.57	11.71		935.71	
172				8.8	931.8	
171				11.3	929.3	
170+77				12.0	928.6	
170				10.7	929.9	
169+67				11.5	929.1	
169				11.3	929.3	
⊙	2.18	932.16	10.59		929.98	
168				6.0	926.2	
⊙	4.59	924.93	11.82		920.34	
167				9.2	915.7	L. Bank of Creek
166+80				15.0	909.9	Bottom " "
166+44		95		8.5	916.4	R Bank " "
166				9.7	915.2	
165		45.9 6 22.7 6 22.9 4		6.0	918.9	
	2.71		45.70			

5+2	+	⊼	−	R	E	
		924.93				
0	2.13	921.05	6.01		918.92	
164+22				4.8	916.2	
164				6.0	915.0	
163				10.1	910.9	
0	1.79	913.42	9.42		911.63	
162				5.9	907.5	
161				9.6	903.8	
B.M.			6.41		907.01	Alder old 5+2 162+85 10' R
	3.92		2.84			
			3.92			
			6.92			

Sta	Hub	Def	C.C.	M.C.		
5	110	10		S67°45'W	75'	To Cabin
170+77	△	28°53'L	N43°56'W	N44° W	✓	
1	1.23				✓	
172	△	13°15'L	N15°03'W	N15°W		
173						
3	3.31					
174+55						
175+31	△	43°46'R	N1°48'W	N1°45'W	✓	
2	1.69					
177+00	△	8°06'R	N45°34'W	N45°30'W	✓	
1	3.31					
178+31	△	0°00'	N53°40'W	N53°40'W		=0+00 of Dam

Variation 20°15'E

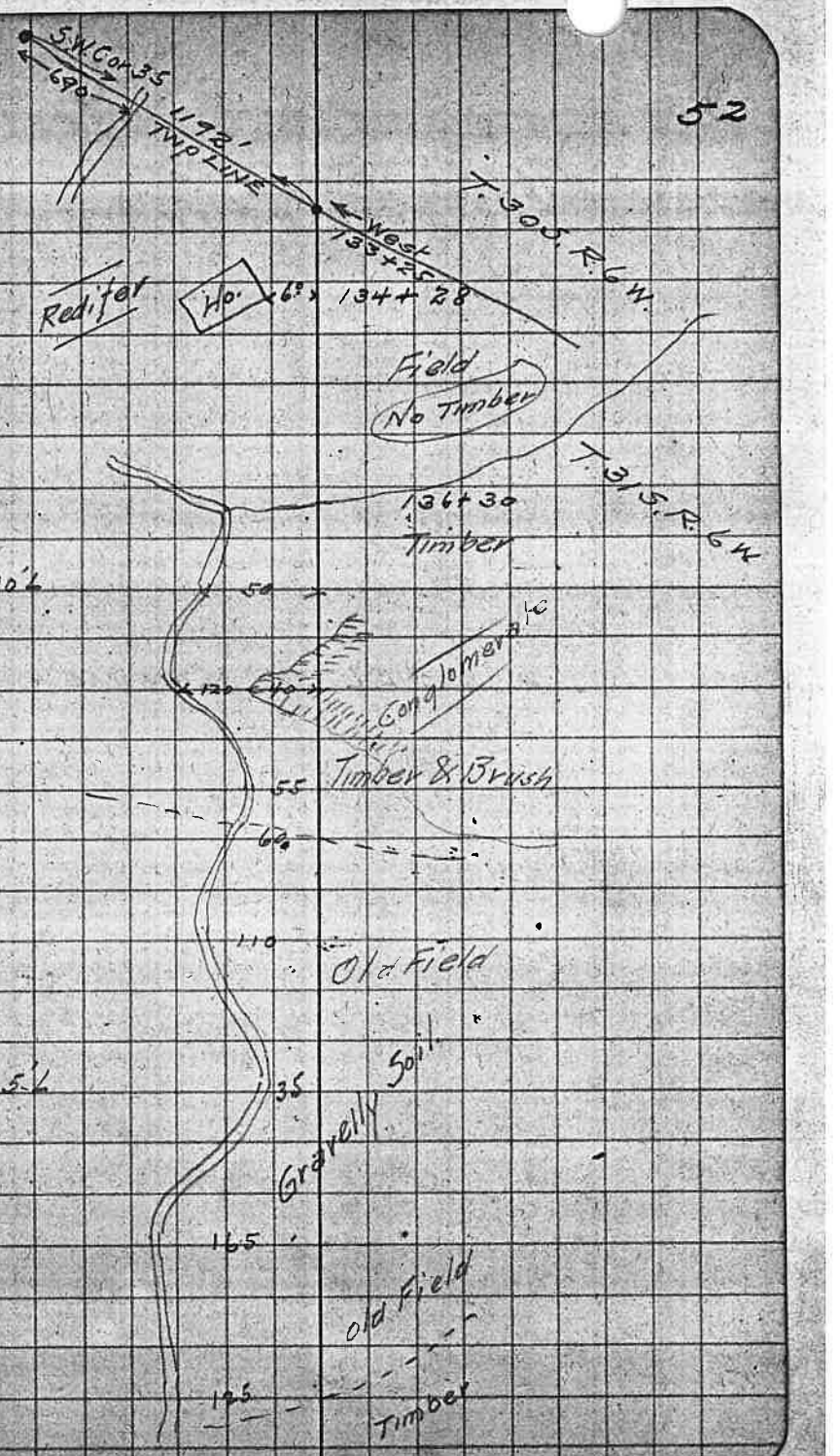


Sta	Hub	Def	C.C.	M.C.	
158+03	△	31°39'R	N8°17'W	N8°50'W	
	97				
159	△	2°02'L	N39°52'W	N40°30'W	Edge of R Bank
	106				
160	△	1°18'L	N37°54'W	N39°W	Edge of R Bank
	100				
161	△	9°03'L	N36°36'W	N37°45'W	
	200				
163	△	13°56'L	N27°33'W	N28°50'W	
	122				
164+22	△	5°43'R	N3°37'W	N14°45'W	
	2,22				
166+44	△	38°24'L	N19°20'W	N20°30'W	On R. Bank
	56				
167	△	41°01'R	N18°54'E	N18°20'E	on L Bank
	100				
168	△	14°18'R	N22°07'W	N23°05'W	L Bank & R.
	167				
169+67	△	6°37'R	N36°19'W	N37°20'W	

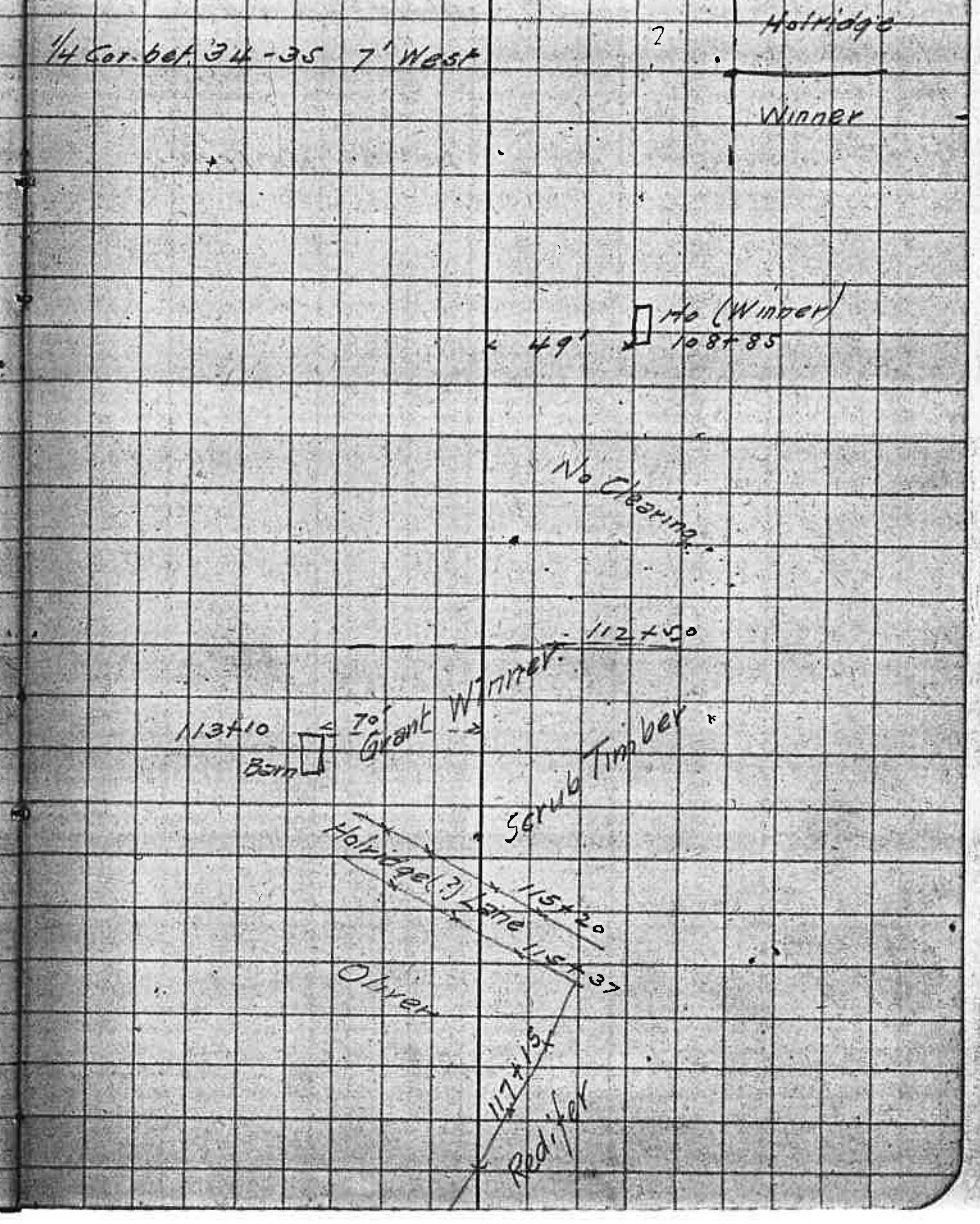
51

Sta	Hub	Def	C.C.	M.C.
	1096			
135+43.4	△	31°41' L	N50°43'W	N51°10'W
	157			
137	△	0°00'	N19°02'W	N19°30'W
	200			
139	△	0°00'	N19°02'W	N19°45'W
	107			
140+07	△	5°50 R	N19°02'W	N19°30'W
141				
	793			
145				
148	△	16°35' L	N24°52'W	N25°20'W
	1003			
152				
155				

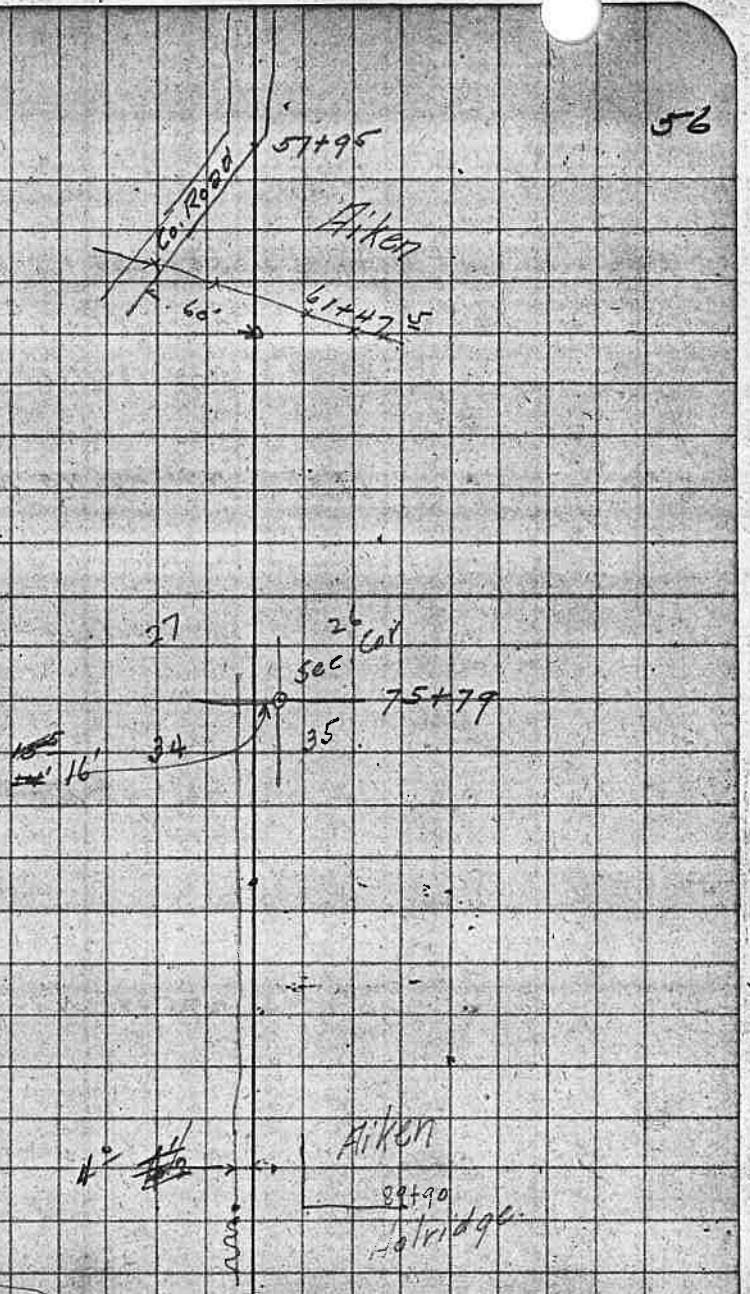
52



98	700	0°38'R	N0°38'W	N1°15'W	
	3.94				
101+94					
	700				
109		0°12'L	N1°16'W	N1°55'W	
	400				
113		1°44'R	N1°54'W	N1°45'W	
	200				
115		25°36'R	N2°48'W	N3°30'W	
	9.47				
124+47		32°19'R	N28°24'W	N28°55'W	



	1731				✓
61+31	△	65°52'R	N65°42'E	N65°40'E	
	7 69				
69	△	0°16'L	N0°10'E	N0°00W	
	1400				✓
83	△	0°10'R	N0°36'E	N0°05'E	
	800				
89+90					
	1.10				
91	△	1°04'R	N0°26'E	N0°15W	



Sta	Hub	Def	C.C.	M.C.	
2+83	△	74°14'R	S81°28E		= 11+27
	25 L				
5+39	△	27°29'L	N24°18'E	N24°00'E	
	5 U 3				
10+82	△	19°57'L	N51°47E	N51°25'E	
	2 18				
13	△	10°30'R	N71°44E	N71°20'E	Opposite Wilson's Gate
	300				
16	△	14°10'L	N61°14'E	N61°E	
	1000				
26	△	2°07'L	N75°24E	N75°E	
26+93					5'R to N.E. Cor Sowersby Tract
	500				
31 1800	△	0°00'	N77°31	N77°15'E	
	1300				
44	△	11°49'R	N77°31'E	N77°15E	
	1731				

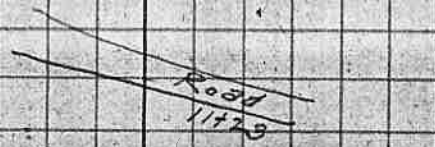
4

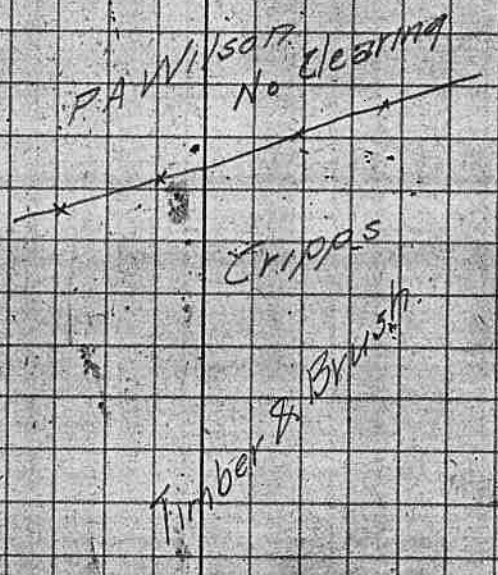
Road

From Reservoir Site to Supply Line Survey.

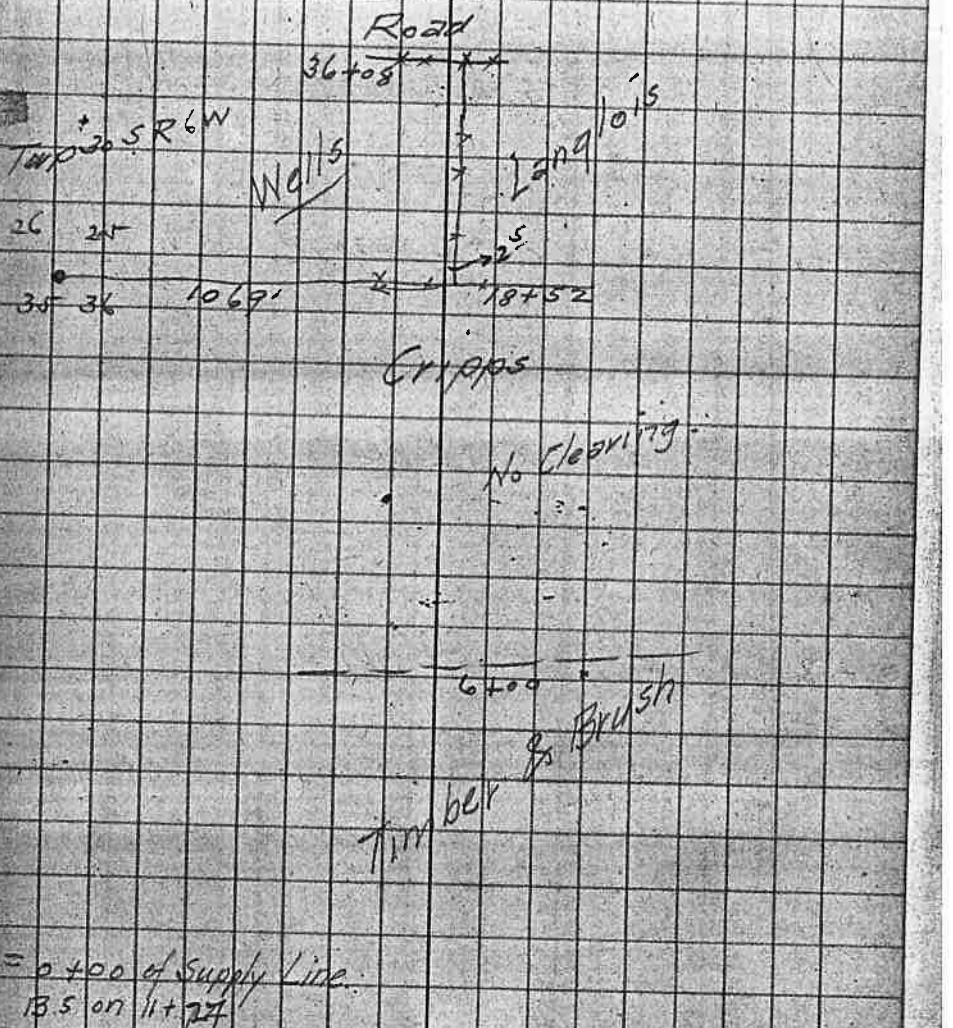
Sta	Hub.	Def	C.C	M.C.
11+27	△	74°14' L	N 7° 14' W	
7+51				
0+00	△	0°00'	N 81° 28' W	N 81° 45' W

To 5+39





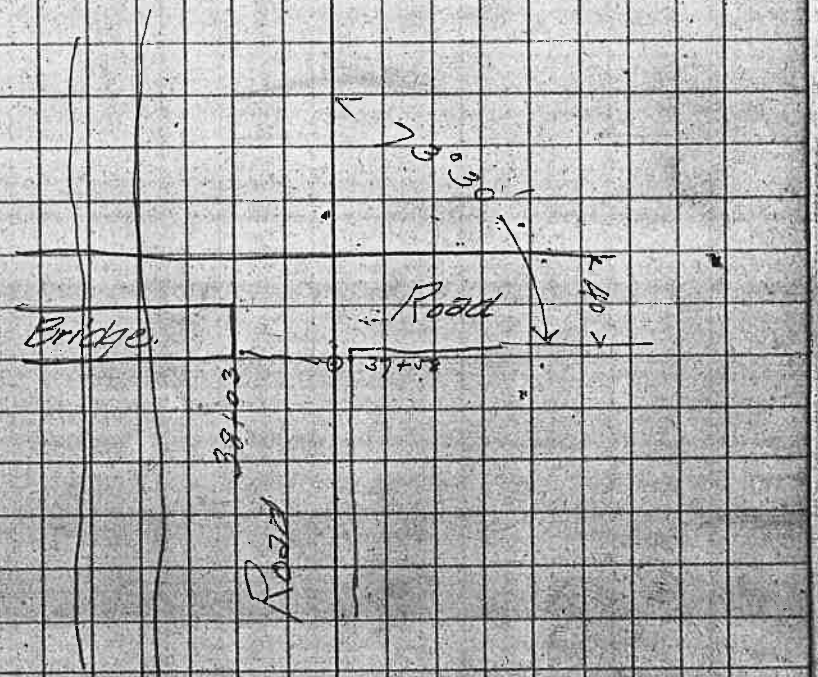
Line to Sta	Tower Hub	Def	C.C.	M.C.
36+12	△	52°18'R	N51°54'E	N51°40'E
	171'			
19	△	0°56'L	N0°24'W	N0°38'W
0+00	△	98°00'L	N0°32'E	N0°14'E



= 0+00 of Supply Line
13.5 on 11+27

57+65 5				
57				
52+64 5				
44+44	Δ	5°08' R	N33°39'W	N34°W
43+46 4	Δ	3°58' L	N38°47'W	N39°W
38	Δ	18°38' L	N34°49'W	
37+58	Δ	68°05' L	N16°11'W	

N N Line of Bank Bldg
W " " Logsdon Store
S Line of Street (3rd St)



Sta	+	X	-	R	E
@	10.78	685.94			675.16
11+27				14.8	671.1
11+00				16.5	669.4
10+83				14.5	671.4 = 2+83
10				0.0	685.9
@	11.79	697.73	0.00		685.94
@	11.11	708.84	0.00		697.73
9				4.7	704.1
@	11.96	720.80	0.00		708.84
8+35				6.6	714.2
@	12.05	732.85	0.00		720.80
8				4.1	728.7
@	11.97	744.82	0.00		732.85
7+50				5.2	739.6
@	12.05	756.87	0.00		744.82
7				3.9	753.0
@	11.18	768.05	0.00		756.87
6+75				10.1	758.0
@	11.41	779.46	0.00		768.05
6				3.5	776.0
@	10.50	789.96	0.00		779.46
5				0.9	789.1
@	11.55	801.51	0.00		789.96
@	11.60	813.11	0.00		801.51
4				9.0	804.1
@	11.67	824.78	0.00		813.11
	149.62				

Sta	+	X	−	R	E
		824.78			
⊙	11.62	836.40	0.00		824.78
3				4.4	832.00
⊙	11.44	847.84	0.00		836.40
⊙	12.02	859.86	0.00		847.84
⊙	11.44	871.30	0.00		859.86
2				11.1	869.2
⊙	11.36	887.66	0.00		876.30
⊙	11.98	894.64	0.00		887.66
1				7.1	887.5
⊙	11.88	906.52	0.00		894.64
⊙	11.32	917.84	0.00		906.52
⊙	11.14	928.98	0.00		917.84
0+00.				8.4	920.6
B.M.				1.65	927.33
⊙	0.76	917.77	11.97		917.01
⊙	0.29	906.14	11.92		905.85
⊙	1.12	895.40	11.86		894.28
⊙	0.72	884.39	11.73		883.67
1				4.2	880.2
⊙	0.07	872.67	11.79		872.60
⊙	0.00	860.87	11.80		860.87
2				3.3	857.6
⊙	0.17	849.11	11.93		848.94
2+75				4.8	844.3
⊙	0.43	837.60	11.94		837.17

903.87 HUB

922.5
18.8
903.7
8.5
912.2

883.67
11.94
895.63
5.43
880.2

104.20
149.42
253.62

927.33
675.14
252.19
1.65
253.82

920.

883.67
+ 11.31
894.98
- 0.31
894.67
+ 11.33
906.00
2.24
903.76
+ 4.22
907.98
4.12
903.86

Laurel at Reservoir Site

880.2

920.6
880.2
40.4

908.7
880.2
28.5

X/100 = 28.5/40.4

404 | 2350 | 5 8
2020 | 1 8
330 | 76

Sta	+	Δ	−	R	E
3		837.60		4.4	833.2
4				13.0	824.6
0	0.44	826.19	11.85		825.75
0	1.62	816.00	11.81		814.38
5				6.0	810.00
0	1.25	805.49	11.76		804.24
6				12.63	792.9
0	0.04	793.96	11.63		793.86
0	0.01	782.04	11.93		782.03
7				5.4	776.6
+20				8.8	773.2
+30				6.7	775.3
+60				7.1	774.9
7+97				11.2	770.8
8				10.4	771.6
+10				7.5	774.5
+50				6.5	775.5
9				10.1	771.9
0	0.32	770.48	11.88		770.16
10				1.9	768.6
0	1.79	760.34	11.93		758.55
0	1.48	749.85	11.97		748.37
0	0.33	738.34	11.84		738.01
11				4.1	734.2
0	0.77	727.18	11.93		726.41
12				8.6	718.6

Sta	+	H	−	R	E
		727.18			
⊙ 12+18	0.36	715.54	12.00		715.18
⊙	1.56	705.26	11.84		703.70
⊙	1.49	694.85	11.90		693.36
⊙	1.12	684.18	11.79		683.06
13				6.2	678.0
⊙	2.92	675.22	11.88		672.30
14				8.0	667.2
15				5.6	669.6
16				4.9	670.3
17				7.1	668.1
18				7.4	667.8
18+45				9.8	665.4
18+75				10.2	665.0
18+85				5.6	669.6
19				4.4	670.8
⊙	3.26	673.95	4.53		670.69
20				5.2	668.7
21				4.2	669.7
22				5.5	668.4
23				4.9	669.0
24				4.7	669.2
25				5.2	668.7
26				4.1	669.8
⊙ +85				5.5	668.4
27				7.7	666.2
+50				8.0	665.9

Sta	+	H	−	R	E
27+60		673.95		4.6	669.3
28				4.3	669.6
29				4.5	669.4
⊙	3.98	673.71	4.22		669.73
30				5.7	668.0
+80				4.2	669.5
31				10.2	663.5
+45				4.8	668.9
32				4.7	669.0
+90				4.4	669.3
33				10.2	663.5
+30				6.9	666.8
+60				6.6	667.1
34				8.4	665.3
35				8.1	665.6
36				5.8	667.9
+12				5.1	668.6
⊙	6.30	674.88	5.13		668.58
37	"			7.2	667.7
+58				7.0	667.9
38				5.3	669.6
⊙	11.23	685.53	0.58		674.30
39				9.5	676.0
40				8.9	676.6
41				8.5	677.0

38+75 12' Lower Ho Ground

39+03 East end of Bridge

41+90 West " " "

42+10 " " " "

Sta	+	x	−	R	E	
42		685.53		7.7	677.8	
⊙	11.87	696.81	0.59		684.94	
43+46½				7.3	689.5	
44				5.0	691.8	
44+44				4.4	692.4	
45				3.8	693.0	
46				3.8	693.0	
47				5.0	691.8	
48				6.4	690.4	
49				7.4	689.4	
50				6.5	690.3	
51				4.6	692.2	
~~52~~						
⊙	10.17	703.66	3.32		693.49	
52				9.6	694.1	
53				8.3	695.4	
54				6.9	696.8	
55				5.3	698.4	
56				3.3	700.4	
57				1.8	701.9	
					702.43	
B.M.			1.23		702.45	Top of Curb E. Line of Bank

Sta	+	X	−	R	E
B.M.					927.33
⊙	8.67	868.53			859.86
34+92				8.5	860.0
⊙ 6+34	9.11	869.09	8.55		859.98
△ 8+20					
⊙	0.29	857.47	11.91		857.18
⊙	0.40	847.92	11.95		847.52
⊙	0.06	836.06	11.92		836.00
⊙ 8+20	10.03	835.02	11.07		824.99
△ 10+04					
⊙ 12+14	8.71	833.71	10.02		825.00
△ 16+75					
⊙ 19+47	3.38	828.38	8.71		825.00
△ 24+10					
⊙ 28+15	8.67	833.67	3.38		825.00
△ 32+03					
⊙ 38+28	6.98	831.98	8.67		825.00
△ 39+50					
⊙ 47+90	11.60	836.60	6.98		825.00
△ 49+65					
⊙ 53+25	8.54	833.54	11.60		825.00
△ 55+80					
⊙ 56+00	10.43	843.97	0.00		833.54
△ 57+35					
⊙ 61+35	11.63	855.60	0.00		843.97
△ 62+00					
⊙ 72+00	8.36	863.96	0.00		855.60
△ 73+05					
⊙ 73+10	11.67	872.42	3.21		860.75
△ 78+60					
⊙ 81+40	11.39	881.39	2.42		870.00
⊙	11.82	893.21	0.00		881.39
⊙	11.86	905.07	0.00		893.21
⊙	11.659	916.66	0.00		905.07
⊙	11.82	928.48	0.00		916.66

Grade	Distance +	Distance −
On Laurel near Sta 0+00		
T.P. near Sta 2+00 of Supply Line		
860.00	192	
	186	142
	184	
	461	210
	463	272
	388	405
	620	625
	175	840
	255	360
	135	

8.00 per mile.
0.15 - Sta.

		℄ 928.48				
⊙ B	7.13	935.61	0.00		928.48	
△ 86+00						
B.M			0.00		935.61	Top of Peg
Sta 95+00	= Sta 98+90		of Line A.			

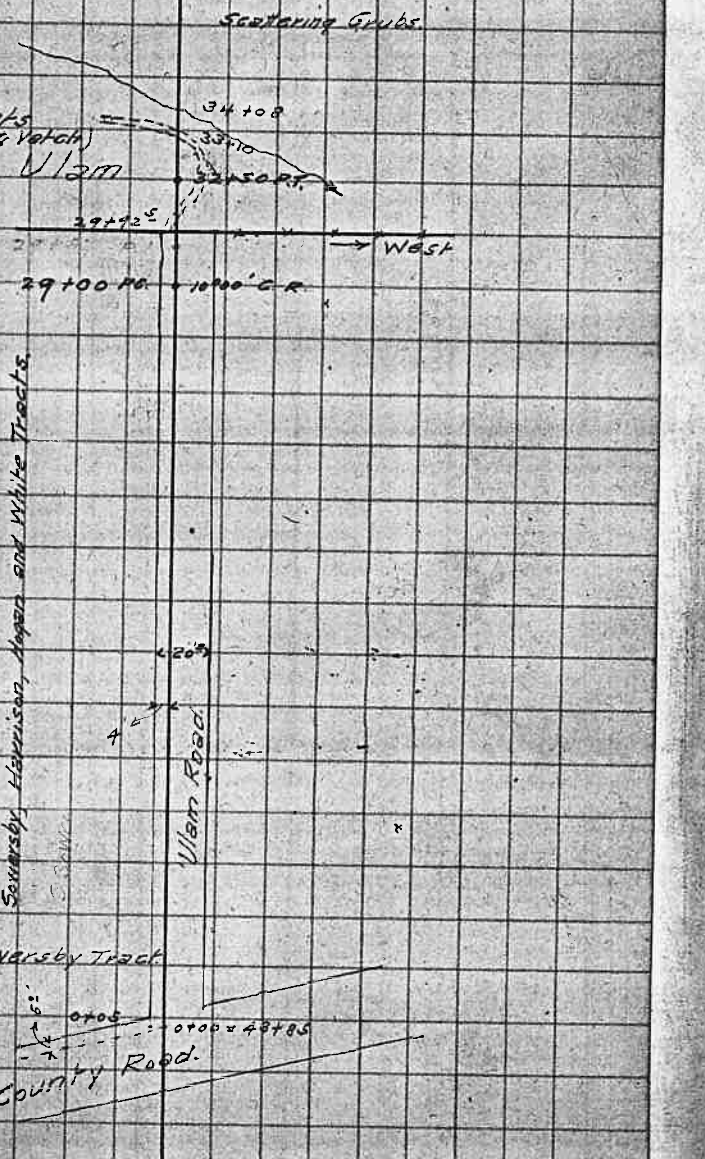
Memo. Line 400' S of SW. Cor. } J.C.W.
" 550' S. of NE. "

187
374

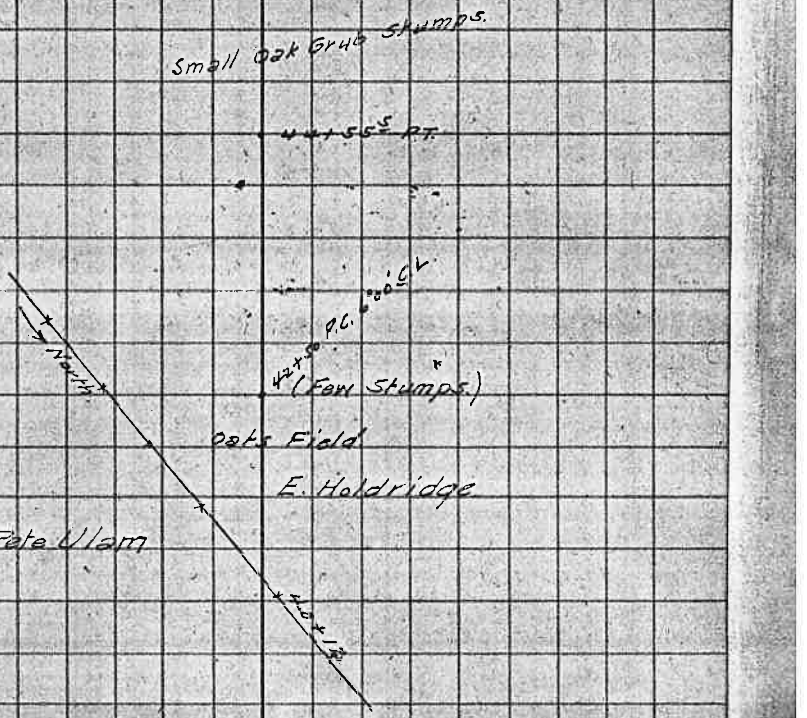
176
374
550

83

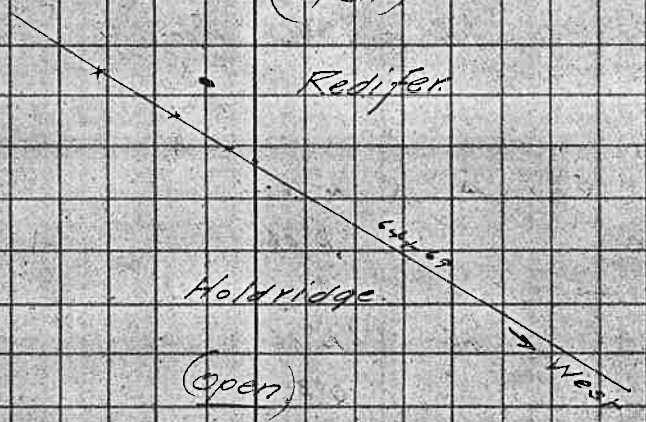
Sta	Hub	Def.		C.C.	M.C.
32+50 P.T.	△			5.35° W	3.35° W
29+00 P.C.	△		10°00' C.R. R. = 573.0 Δ = 35°00' T =		
0+05					
0+00	△	77°30' L		South	South



Sta	Hub.	Def.		C.C.	M.C.
44+55 S P.T.	Δ			S22°40'W	S.22°40'W
44+50		6°10'			
44		6°00'			
43+50	Δ	4°30'			
43		3°00'			
42+50 P.C.	Δ	1°30'	6°00° C.L. R. Δ 12°20' T =		



Sta	Hub	Def		C.C.	M.C.
67		26°15'			
+50	△	25°			
66		23°45'			
+50		22°30'			
65		21°15'			
+50	△	20°00'			
64		18°45'			
+50		17°30'			
63		16°15'			
+50		15°00'			
62		13°45'			
+50	△	12°30'			
61		11°15'			
+50		10°00'			
60		8°45'			
+50	△	7°30'			
59		6°15'			
+50		5°00'			
58		3°45'			
+50		2°30'			
57+00 P.C.	△	1°15'	5°00' C.L. Δ = 61°15' T =		



Light Clearing & Grubbing

89

Sta	Hub	Def		C.C.	M.C.
82		3°21'			
81+50		0°51'			
81+33 P.C.	△		10°00' C.R. Δ = 32°30' T = R =		
				S 43°05' E	S 43°05' E
78+15 P.T.	△	2°15'			
78		2°06'			
+50		1°36'			
77	△	2°06'			
+50		0°36'			
76		0°06'			
75+90 P.C.	△		2°00' C.L. Δ = 4°30' T = 112.55 L = 2.21 R =		
69+25	△			S 38°35' E	S 38°35' E
69		30°37½'			
+50		30°00'			
68		28°45'			
67+50		27°30'			

90

Sta. 81+68 Intersect Twp Line between Twp 30/31 & 13.10' W. of S.W. cor Sec 35

House

< 112½°

Redifer.

77+00

Timber & Grubbs

Very Light Grubbing

70+00

Sta	Hub	Def		C. C.	M. C.
+27 P.T.	△	8° 42'			S 8°30' E
96		7°21'			
+50		4°51'			
95		2°21'			
94+53 P.C.	△		R 10°00' C.L. Δ = 17°24'		
					S 25°55' E
87+74 P.T.	△	7°27½'			
87+50		6°15'			
87		3°45			
86+50		1°15'			
86+25 P.C.	△	[illegible]	10°00' C.L. Δ = 14°55' T = 75.0 R. =		
85	△				
84+58 P.T.	△	16°15'			
+50		15°51'			
84		13°21			
+50		10°51'			
+20.	△	9°21'			
83		8°21			
82+50		5°51'			

17.4

Old field

84+00

Timber & Brush

No Clearing

83+90

29°5

To House

93

Sta	Hub	Def		C.C.	M.C
+55.2 PT	△	5°05'			
109		3°42'			
+50		2°27'			
108		1°12'			
107+52 P.C.	△		5°00' C.R Δ = 10°10' T = 101.9 R =		
106+48.5	△	15°30'			
+25		13°09'			
106		10°39'			
+75		8°09'			
+50		5°39'			
+25		3°09'			
105		0°39'			
104+93.5 P.C.	△		20°00' C.L Δ = 31°00' T = 79.5 R =		

18
18

S 10.2
204

S 10.16
203.2

104+93.5
- 104+48.5
45

S 8°30' E

31

S 39°30' E
10 10

S 29 20 E
1 20

S 28 40 E
18

S 28 40
3 30
25

94

Sta	Hub	Def		C.C.	M.C.
					S35°35'E
115 + 28	△	9°00			
115		8°10'			
+50		6°40'			
114		5°10'			
+50	△	3°40'			
113		2°10'			
+50		0°40'			
112+28 P.C.	△		6°00' C.L. Δ = 18°00' T = 151.2		
111	△	6°40'			
+50		3°40'			
110		0°40'			
109+86.2 P.C.	△		(R) 10°00' C.L. Δ = 11°20' T = 77.3 R =		

Timber & Brush

Sta	Hub	Def		C.C.	M.C.
+75	△	19°43½			
+50		15°58½			
+25		12°13½'			
123		8°28½'			
+75		4°43½'			
+50		0°58½'			
122+43.5 P.C.	△	0°~~58½~~'	30°00' C.L. Δ = 52°00' T = 93.1 R =		
					S1°40' E
119+87.3 P.T.	△	9°35'			
+75		8°21'			
+50		5°51'			
+25		3°21'			
119		0°51'			
118+91.5 P.C.	△		20°00' C.R. Δ = 19°10' T = 48.4 R =		
118+70	△	45°00' L			S20°40' E
118	△	60°00' R			S24°20' W

Timber of British

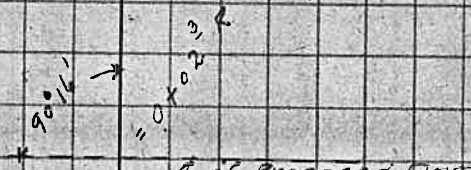
118+40

125+99 △

553°40' E

124+16 8 PT △ 26° 00'

124 23° 29½'



Sta	+	X	−	R.	E	
B.M.	7.71	955.58			947.87	24" Alder near Proposed Dam.
125+99				3.2	952.4	
125				7.1	948.5	
124				11.2	944.4	
⊙	2.03	946.30	11.31		944.27	
123+75				2.3	944.0	
123+50				2.3	944.0	
123+25				1.2	945.1	
123				4.2	942.1	
122+75				5.0	941.3	
122+50				5.7	940.6	122 to 122+50 No ditch.
122				6.8	939.5	
121				9.3	937.0	
⊙	1.69	936.53	11.46		934.84	
120				3.6	932.9	
119+75				4.6	931.9	
119+50				5.7	930.8	
119+25				6.8	929.7	
119				7.7	928.8	
118+70				7.4	929.1	
118+60				10.2	926.3	
118+50				12.5	924.0	
118+40				14.5	922.0	
118+30				13.2	923.3	Water Surface Wilson Creek
118+20				12.5	924.0	
	11.43		22.77			

Sta	+	=	−	R	E
118		936.53		7.0	929.5
Δ				10.2	926.3
117				9.2	927.3
⊙	3.56	932.41	7.68		928.85
117+25				7.4	925.0
116+75				4.5	927.7
116+50				7.9	924.5
116				9.0	923.4
115+28				9.3	923.1
115				9.9	922.5
⊙	2.43	922.99	11.85		920.56
114+50				3.8	918.2
114				5.7	916.3
113+50				7.5	915.5
113				4.3	918.7
112+50				3.4	918.6
112+28				4.6	918.4
112				5.1	918.9
⊙	2.91	916.84	9.06		913.93
111				5.1	911.7
110+50				7.0	909.8
110				7.9	908.9
⊙	0.89	909.63	8.10		908.74
109+55²				3.1	906.5
109				5.8	903.8
	9.79		36.69		

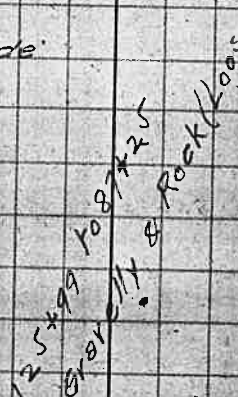
High Water Mark

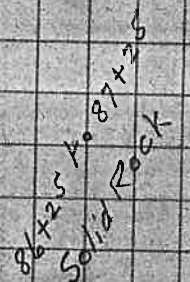
Sta	+	H.I.	−	R	E	
108+50		909.63		7.9	901.7	
108				7.8	901.8	
107+52				6.0	903.6	
107				7.5	902.1	
106+48				11.4	898.2	
⊙	0.99	899.98	10.64		898.99	
106+25				3.6	896.4	
106				4.5	895.5	
105+75				3.9	896.1	
105+50				5.0	895.0	
105+25				6.2	893.8	
105				7.3	892.7	
104				10.1	889.1	
103+30				11.9	888.1	
103				10.4	889.6	
102+50				13.5	886.5	
⊙	1.46	889.55	11.89		888.09	
BM				4.38	885.17	W. Oak 12" diam. 40' R. of Sta 102+10
102				5.2	884.4	
101				7.8	881.8	
100				10.9	878.7	
⊙	1.15	879.38	11.32		878.23	
99				3.1	876.3	
98				5.2	874.2	
97				8.1	871.3	
	3.60		33.85			

Sta	+	T	−	R	E
96		879.38		10.8	868.6
95+50				9.8	869.6
95+30				12.6	866.8
95				9.4	870.0
⊙	2.52	873.21	8.69		870.69
94+53				3.4	869.8
94				7.9	865.3
93+88				10.2	863.0
93				8.8	864.4
92				11.8	861.4
⊙	0.31	861.79	11.73		861.48
91				4.2	857.6
90				7.8	854.0
89				12.7	849.1
⊙	2.14	851.99	11.94		849.85
88				6.3	845.7
87+74				7.0	845.0
87+50				7.6	844.4
87+25				7.2	844.8
87				1.8	850.2
⊙	8.01	859.53	0.47		851.52
86+75				5.8	853.7
86+50				3.7	855.8
86+25				11.6	847.9
86				12.5	847.0
	12.98		32.83		

In Draw 7' wide.

In Draw 4' wide.





Sta	+	X	−	R	E	
		859.53				
⊙	5.60	853.27	11.86		847.67	
85+60				5.5	847.8	
85+50				2.5	850.8	
85				3.3	850.0	
84+50				6.5	846.8	
⊙	2.59	844.05	11.81		841.46	
84				8.6	835.4	
83+85				12.9	831.1	In Draw 10' wide
83+70				7.7	836.3	
83+50				1.7	842.3	
⊙	11.47	855.52	0.00		844.05	
83+20				9.6	8459	
83				8.0	847.5	
82+50				5.6	849.9	
82				4.6	850.9	
81+50				3.9	851.6	
81				4.6	850.9	
80				3.2	852.3	
⊙	8.65	861.20	2.97		852.55	
79				5.3	855.9	
⊙	7.25	868.45	0.00			
78				6.4	862.0	
77+50				6.3	862.1	
77				5.9	862.5	
76+50				6.8	861.6	

Sta	+	=	−	R	E
76		868.45		11.00	857.4
75+90				11.5	856.9
⊙	2.10	859.09	11.46		856.99
B.M.				4.53	854.56
75				7.3	851.8
74				12.6	846.5
⊙	1.12	848.65	11.56		847.53
73+50				5.1	843.5
73				12.0	836.6
72+95				10.1	838.5
72				7.7	840.9
⊙	6.82	855.47	0.00		848.65
71				6.5	849.0
70				4.9	850.6
69				8.0	847.5
68				7.1	848.4
67				3.4	852.1
⊙	11.40	866.87	0.00		855.47
66+50				11.00	855.9
66				7.4	859.5
65+50				7.9	859.0
65				6.9	860.0
64+50				3.7	863.2
64				3.0	863.9
63+50				1.3	865.6
	21.44		23.02		

W.O. 8" S.L. Sta 75+15

To Draw

Sta	+	±	−	R	E	
		866.87				
⊙	11.66	877.62	0.91		865.96	
63				8.3	869.3	
62+50				3.8	873.8	
62				4.2	873.4	
61+50				0.7	876.9	
61				7.8	869.8	11 Elm 12"
60+50				6.0	871.6	
60				5.4	872.2	
59+50				5.3	872.3	
59				3.5	874.1	
⊙	11.86	889.48	0.00		877.62	
58+50				10.3	879.2	
58				2.8	886.7	
⊙	11.56	900.25	0.79		888.69	
57+50				7.4	892.9	
57				3.5	896.8	
56+50				0.1	900.2	
⊙	1.68	890.91	11.02		889.23	
55				2.8	888.1	
54+50				6.8	884.1	
⊙	2.97	881.98	11.90		879.01	
54				4.9	877.1	
53				12.8	869.2	
BM				5.20	876.78	W Oak 12" diam 50' / Sta 52+10
⊙	3.11	873.53	11.56		870.42	

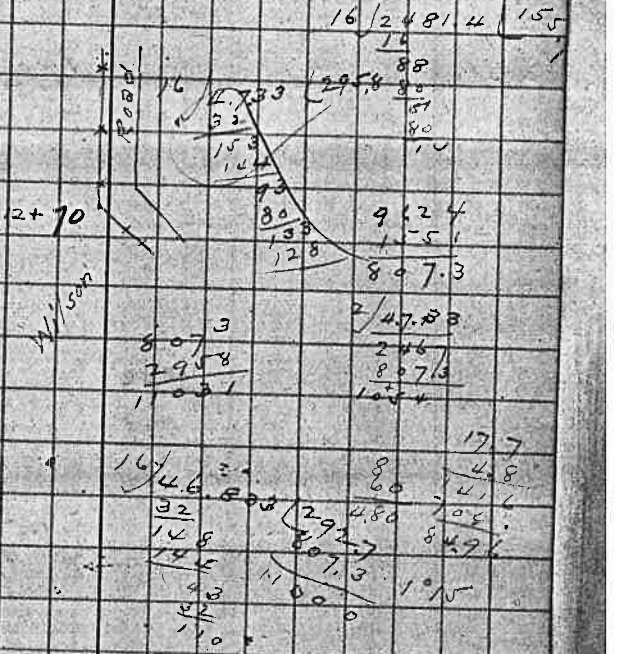
	+	℄	−	R	E
52		873.53		9.2	864.3
51+50				7.8	865.7
51				6.1	867.4
50+50				7.9	865.6
50				15.8	857.7
49+50				14.0	859.5
49				8.6	864.9
⊙	11.90	885.43	0.00		873.53
48				4.2	881.2
⊙	11.91	897.34	0.00		885.43
47				1.8	895.5
⊙	11.18	908.52	0.00		897.34
46				0.8	907.7
⊙	11.85	920.37	0.00		908.52
45				0.5	919.9
⊙	11.31	931.68	0.00		920.37
44+50				6.4	925.3
44				2.0	929.7
43+50				5.1	926.6
⊙	0.50	920.31	11.87		919.81
43				3.8	916.5
⊙	0.41	908.89	11.83		908.48
42+50				3.6	905.3
⊙	0.25	897.39	11.75		897.14
42				3.5	893.9
	59.31		35.45		

Sta	+	X	−	R	E	
		897.39				
@	0.36	885.91	11.84		885.55	
41				10.7	875.2	
@	1.16	875.16	11.91		874.00	
@	0.64	863.94	11.86		863.30	
40				3.2	860.7	
@	0.45	852.52	11.87		852.07	
39				2.9	849.6	
@	0.84	841.40	11.96		840.56	
38				2.7	838.7	
@	1.57	831.00	11.97		829.42	
37				3.8	827.2	
@	0.86	819.87	11.99		819.01	
36				7.4	812.5	
@	1.36	809.23	12.00		807.87	
35				13.1	796.1	
@	0.85	798.08	12.00		797.23	
@	0.95	787.36	11.67		786.41	
34+40				4.8	782.6	
34+25				6.5	780.9	L. Bank
34+10				14.5	772.9	In Drain
34				7.7	779.7	R Bank
@	6.91	794.27	0.00		787.36	
33				2.4	797.9	
32+50				2.1	792.2	
32				7.3	787.0	
31+50				11.8	782.5	
@	0.63	783.01	11.89		782.38	
31				5.4	777.6	
30+50				11.6	771.4	
@	1.11	772.16	11.96	0	771.05	
30				8.7	763.2	
@	0.19	760.44	11.91		760.25	
29+50				3.2	757.2	
29				7.6	752.8	
28				12.4	748.0	
@	1.68	750.18	11.94		748.50	
27				5.8	744.4	
26				8.2	742.0	
25				9.2	741.0	
24				11.3	738.9	
@	1.28	739.50	11.96		738.22	
23				3.2	736.3	
22				4.6	734.9	
21				6.0	733.5	
20				7.5	732.0	
19				9.3	730.2	
	20.84		178.73			

119

Sta	Hub	Def		C.C	M.C.
18+77	△	10°00'			
+50		7°18'			
+25		4°48			
18		2°18'			
17+77 P.C.	△		20°00' C.R. Δ = 20°00 T = 50.5		
11+00	△	23°25'			
+75		21°25'			
+50		19°25'			
+25		17°25			
10		15°25'			
+75		13°25			
+50		11°25			
+25		9°25			
9		7°25'			
+75		5°25'			
+50		3°25'			
+25		1°25'			
8+07 3/5 P.C.	△		16°00' C.C. Δ = 46°50 T = 155±		
0+00	△				

120



Sta	Hub	Def		C.C	M.C.
+46.4 P.T.	△	1°02½'			S77°30'W
34		0°48½			
+50		0°33½'			
33		0°18½'			
32+50		0°3½'			
32+38¹ P.C.	△		7°00' C.R Δ = 2°05' T = 104.2		
+14⁶ P.T.	△	7°06'			S75°20'W
24		6°22'			
+75		5°07'			
+50		3°52'			
+25		2°37'			
23		1°22'			
22+72⁸ P.C	△		10°00' C.R Δ = 14°12'		
20+96⁶ P.T.	△	5°15'			
+75		4°10'			
+50		2°55'			
+25		1°40'			
20		0°25'			
19+91⁶ P.C.	△		10°00' C.L Δ = 10°30' T = 52.6		

57+25⁴

12
30
3.60

60/50.6
48

34+42.3
1 04.2
33+38.1
2.083
35+46.4

27⁴
3
82

23+44.2
71.4
22+72.8
1 42
24+14.6

18		739.50		10.5	729.0
17	0.10	727.87	11.73		727.77
16				2.3	725.6
15				4.7	723.8
14				7.5	720.4
13				9.5	718.4
12				11.3	716.6
11	2.12	718.55	11.44		716.43
10				2.7	715.9
9				4.4	714.2
8				4.8	713.8
7				6.4	712.2
6				9.2	709.4
5				10.2	708.4
4				8.6	710.0
3				9.0	709.6
2	1.92	712.03	8.44		710.11
1				3.4	708.6
0 = 51+25				3.2	708.8
51				4.4	705.6
50				5.6	706.4
49				7.2	704.8
48				6.6	705.4
0	0.95	702.34	10.64	9.0	703.0
47				10.7	701.3
46+70				11.1	700.9
46+30					701.39
46+35				4.2	698.1
46+25				5.4	696.9
46				12.6	689.7
45+40				10.7	691.6
45				10.5	691.8
44+50				11.0	691.3
44				10.5	691.8
0	6.70	708.07	0.97	7.8	694.5
43				4.1	698.2
42				1.5	700.8
41					701.37
40				3.1	705.0
39				4.0	704.1
38				5.0	703.1
B.M				6.8	701.3
37				7.2	700.9
0	0.12	698.49	9.70	8.1	700.0
36				8.32	699.75
35				10.3	697.8
					698.37
				4.3	694.2
				7.9	690.6

In Draw 6' Wide

Sta	+	X	−	R	E
34+70				9.0	689.5
34+60		698.49		12.0	686.5
34+50				9.3	689.2
34				10.3	688.2
33+50				11.5	687.0
33				10.3	688.2
32+50				8.5	690.0
32				9.8	688.7
⊙	1.29	689.06	10.72		687.77
31				4.7	684.4
30				7.5	
29+85				9.6	
29+80				8.6	
29				10.5	
28				11.9	
⊙	4.30	681.86	11.50		677.56
27				5.2	
26				6.5	
25				5.9	
24				6.5	
23				6.9	
22				6.7	
21				5.3	
20				4.5	
⊙	2.84	680.32	4.38		677.48
19				5.7	
18				6.7	
17				7.0	
16				6.3	
15				6.5	
14				5.9	
13				6.5	
12				8.1	
11+70				7.9	
⊙	10.89	691.21	0.00		
11				9.7	
10+75				7.3	
10+50				3.3	
10+25				1.6	
⊙	11.32	702.53	0.00		
10				10.7	
9+75				6.8	
9+50				4.1	
9+25				0.7	
⊙	11.64	714.08	0.09		702.44
9				8.7	
8+75				4.7	
⊙	11.90	725.98	0.00		
8+50				9.0	
8+30				10.8	

In Draw

		+	−	R		
8+25		725.98		4.9		
0	5.61	731.59	0.00			
8				2.6	729.0	
B.M.				4.30	727.29	B 084 25' R. of Sta 8+10

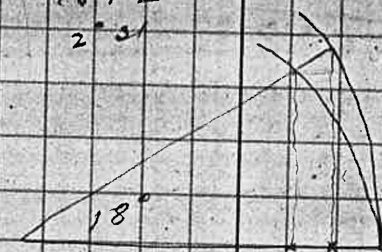
129

130

.565
9
5085
8.28 1/2
168
9
1512
2.31

60
30
1800
90
6.5
5.6

25
9
225
3 45
58 1/2
4 40 1/2
3)5.2
1733



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1433

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287
3
86

122435
1738
1244716.8

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3 45
12 10 1/2
3 45
15 58 1/2
3 15
19 43 1/2
3 40
3 28 1/2

81
8

14444+56 = 90403

131

92881 | 115000 | 12.3
92881
221190
185762
354280
278643
75637

37720
3
1916

4.58
7.57
25.00
37.15
32.57
69.72
3486
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03700

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37) 16200 (4.4
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XX	+	T	−	R		98,9			CAL		
409		103,55		4,05	99,50	98	97	4,58	,53	✓	
410				3,80	99,75		96	59	,79	✓	
411				3,90	99,65		95	60	,75	✓	
412				3,52	100,03		94	61	1,09	✓	
413				3,35	100,20		93	62	1,27	✓	
414 TP	3,20	103,20	3,55	3,55	100,00		92	63	1,08	✓	
415				3,05	100,15		91	4,29	1,28	✓	
416							90	30			
417				3,30	99,90		89	31	1,01	✓	
418				3,65	99,55		88	32	,67	✓	
419				3,71	99,49		87	33	,62	✓	
420				3,80	99,40		86	34	,54	✓	
21				3,88	99,32		85	35	,47	✓	
22				3,95	99,25		84	36	,41	✓	
23				4,01	99,19		83	37	,36	✓	
24				4,28			82	38	,00	✓	
25				3,9			81	39		✓	
26				4,0			80	40		✓	
27				41			79	41		✓	
28 TP	4,92	103,70	4,42	42	98,78		78	42		✓	
29				93			77	4,93		✓	
430				94			76	94		✓	
31				95			75	95		✓	
32				96			74	96		✓	
33				97			73	97		✓	
34				98			72	98		✓	

103.20 − 98.82 = 4.38

103.20 − 9.891 = 4.29

108 − 4.38 = 103.70

98.91 − 4.29 = 94.62

94.53 + 1.74 = 96.27

7.27 − .81 = 6.46

103.70 − 98.91 = 4.79

S	+	X	−	TP	E	G
435		103,70		4,99	✓	98 71
436				5,00	✓	70
37				,01	✓	69
38				,02	✓	68
39				,03	✓	67
440				,04	✓	66
41 TP	3,42	102,07	5,05	,05	98,65	65
42				3,43	✓	64
43				44	✓	63
44				45	✓	62
45				46	✓	61
46				47	✓ 98,60	98, 60
47	4,33	10 2,92	3,48	3,48	98,59	59
48				4,60	✓ 98,32	58
49				4,35	✓	57
450				4,45	98,27	56
51				4,30	✓ 98,62	55
52				4,16	✓ 98,77	54
53				4,2	✓ 98,70	53
54				3,86	✓ 99,12	52
55				4,85	98,07	51
56				5,20	✓ 97,72	98 50
57				4,2	✓ 98,72	49
58				4,22	✓ 98,70	48
59				3,45	✓ 99,27	47
60				3,92	✓ 99,00	46

		102,07	102,72
		98,64	98,48
		3,43	4,24

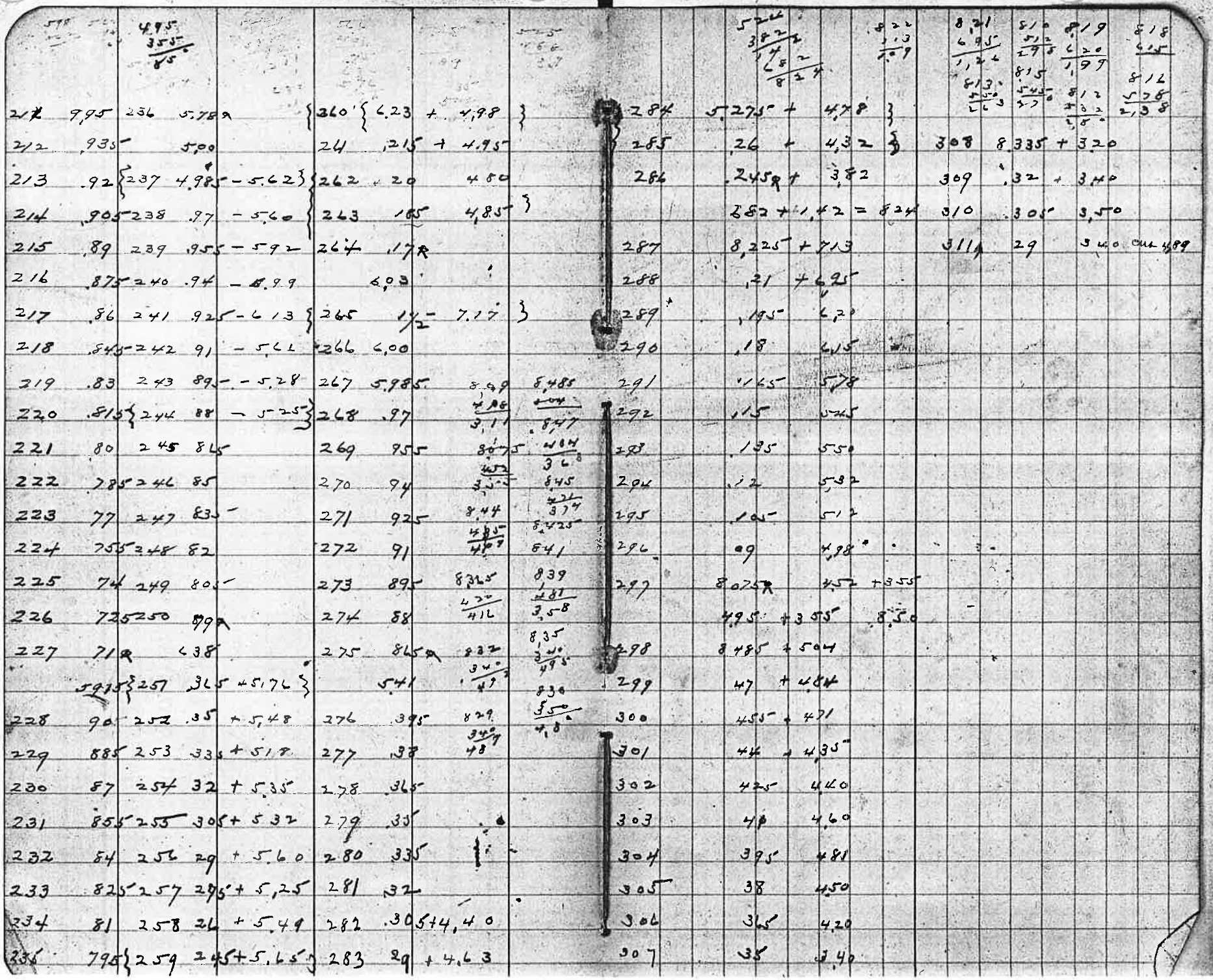
GP	CH	F.H
499		
500		
01		
02		
63		
64		
05		
343		
44		
45		
46		
47		
48		
434		2,6 ✓
35		
36		2,0 ✓
37	07 ✓	
38	0,3 ✓	
39	1,7 ✓	
40	2,0 ✓	
41		44 ✓
42	3	78
43	2,8 ✓	
44	2,7 ✓	
45	8,0 ✓	
46	5,4 ✓	

61			102,92		4.35	✓	98 57	98,	45	✓		4, 47		.12	✓				
62					5.65	✓	97.27		44			48				1.17	✓		
63					5.10	✓	97,52		43			49				61	✓		
64					6,41	✓	96 51		42			50				1.91	✓		
65					5,30	✓	97,62		41			51				79	✓		
66					5,00	✓	97,92		40			52				45	✓		
67					4,58	✓	98 39		39			53					✓		
68					.54	✓	98 98		38			54					✓		
69					.55	✓	98 37		37			55					✓		
70					56	✓	98 26		36			56					✓		
71	TA 427	10 2,22	4,57		57	✓	98 35		35			1 57					✓		
72					520	✓	97 42		34			4,28				92	✓		
73					515	✓	97 47		33			29				96	86		
74					4,44	✓	97 98		32			30				34	✓		
75					4.04	✓	98 58		31			31		27	✓				
76					3,90	✓	98 72		30			32		42	✓				
77					3 52	✓	99 13		29			35		89	✓				
78					3 71	✓	98 91		28			34		63	✓				
79					4,00	✓	98,62	✓	27			33		35 37					
80					4,38	✓	98 24		26			36				(92)			
81					5,82	✓	96 80		25			37				(1,45) 1,43			
82					4,96	✓	97,66		24			38				(58) 52			
83					4,80	✓	97,82		23			39				(41) 39			
84					4,42	✓	98,20		22			40				(.02)			
85					4,43	✓	98.19		21			41				(.02)			
86					4,44	✓	98.18		20			42				(.02)			

4 87	102.62	4.45	98.17	98.19	4.45	— (02)
88		.46	98.16	.18	46	(02)
89		.47	98.15	.17	47	(02)
90 TP		48	98.14	.16	48	(02) 5.30 Pm

Nov 23 1911

1	4.94	24	4,49	48	5,24	72	3,83	96	2,87	5	120	4.39		144	4.395			4,18			192	.23		
2	.93	25	48	49	.22	73	.81	97	86		121	.37		145	.38		168	.165			193	.20		
	3,98	26	47	50	.20	74	79	98	84	5	122	31		146	.345		169	.15			193	.20		
3	97	27	46	51	18	75	77	99	83		3,44			147	33		170	13.5			194	1.85		
4	96	28	.45	52	16	76	75	100	.81	5	123	.29		148	335		171	12			195	.17		
5	95		7,50	53	14	77	73	101	.80		124	41		149	32		172	105			196	155		
6	94	29	.49	54	12	78	71		4.38		125	39			4.395		173	09			197	.14		
7	93	30	48	55	16	79	69	102	76	5	126	38		150	58		174	.075			198	125		
8	92	31	47	52	08	80	67	103	75		127	.365		151	525		175	06			199	11		
	7.53	32	46	57	06		553	104	73	5	4.45			152	55		176	0.45			200	095		
9	52	33	45	58	.04	81	57	105	72		128	435		153	535		177	.03			201	.08		
10	51	34	44	59	.02	82	49	106	705		129	42		154	.52		178	.015			202	.065		
11	50	35	43	60	500	83	47	107	69	R	130	60		155	505		179	4,00			203	05	R	
12	49	36	42		5.42	84	45		4.54		31	58		156	49		180	.985				319		
13	48	37	41	61	40	85	43	108	57	5	32	575		157	475		181	.97	R		204	175		
14	47	38	39	57	38	86	41	109	555		33	52		158	42			6.065			205	16		
15	46	39	37	63	36	87	.39	110	54		34	545		159	445		182	.05			206	145		
16	45	40	35	64	34	88	37	111	535		35	53		160	43		183	035			207	13		
	4.57	41	33	65	32	89	35	112	51		36	515		161	415		84	.02			208	115		
17	56	42	31	66	30		299	113	495		37	50		162	40		85	0.005			209	10		
18	55		5.36	67	28	90	97	114	48		138	485		163	385		86	5.99			210	085	R	5 Pm
19	54	43	34	68	26	91	95	115	465		39	47		164	37		87	.975			211	07	R	5 Pm
20	53	44	32	69	24	92	90	116	45		140	455		165	355		88	.96						Nov 24 1911
21	52	45	30	70	22	93	92	117	435		141	44		166	34		89	.945						
22	51	46	28		3.87	94	905	118	42		142	425		167	325	R	190	.93						
23	50	47	26	71	.83	95	89	119	405		143	41					191	.915	A					



Sta	+	TA	=	R	E	G	GT	Cut		
0	6.45	106.45		6.45	100	100	6.45			
1				5.68	100.77	99.99	6.46	.78		
2				5.99	101.36	98	47	1.38		
3				5.21	101.24	97	48	1.27	✓	
4				5.13	101.32	96	49	1.36	✓	
5				4.95	101.50	95	50	1.45	✓	
6				5.65	100.80	94	51	.86	✓	
7				5.78	100.69	93	52	.74	✓	
8				5.04	101.41	92	53	1.49	✓	
9				5.14	101.31	91	54	1.40	✓	
10				4.69	101.76	90	55	1.86	✓	
11				5.14	101.31	89	56	1.42	✓	
12				4.68	101.77	88	57	1.89	✓	
13				5.15	101.30	87	58	1.43	✓	
14				5.32	101.13	86	59	1.27	✓	
15				5.22	101.23	85	60	1.38		
16				5.40	101.05	84	61	1.21		
17				5.41	101.04	83	62	1.21		
18				5.25	101.20	82	63	1.38		
19				5.98	100.47	81	64	.66		
20				5.82	100.63	80	65	.83		
21				5.92	100.53	79	66	.73		
22				6.10	101.35	78	67	.57		
23				6.68	99.77	77	68			
24				6.69	99.76	76	69			

23
6
138
24
162

.23 ✓
600
1.41.000
2.21

	+	X	−	R	E	G	GTP	CHK
		10 CHS						
25				6.70	9.925	99.75	6.70	
26				6.71	9.974	74	.71	
27				6.72	23	73	.72	
28				23	72	72	.73	
29				24	21	71	.74	
30				25	70	70	.75	
31 TP	4.81	104.00	5.76		9.969	69	5.76 ✓	
32				4.32		68	4.32	
33				33		67		
34				34		66		
35				35		65		
36				36		64		
37				37		63		
38				38		62		
39				39		61		
40				40		99.60		
41				41		59		
42				42		58		
43				43		57		
44				44		56		
45				45		55		
46				46		54		
47				47		53		
48				48		52		
49				49		51		
50				50		99.50		
51								
52								
53								
54								
55								
56								

S	+	T	−	R	E		9R	Cul-	
		10+00							
357				4,57	99,49	48	457		
58				,52	48	48	453		
59				,53	47	47	53		
60				4,10	99,90	46	54	44	
61				4,21	99,79	45	55	34	
62				3,95	100,05	44	52	61	
63				3,71	100,29	43	57	86	
64				3,55	100,1	42	58	73	
65				3,67	100,33	41	59	9	
66				3,59	100,41	40	60	1,29	
67				3,86	100,14	39	61	75	
68				3,75	100,15	38	62	77	
69				4,09	99,91	37	63	54	
70				4,28	99,78	36	64	42	
71			4,65	4,25	99,35	35	65		
72				4,46		34			
73				,47		33			
74				,68		32			
75				,69		31			
76				,70		30			
77				,71		29			
78				,72		28			
79				,73		27			
380				,74		26			
381TP	5,47	10472	4,75	,75	99,25	25	547		
382				5,12	99,60	24	148	86	

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1979.6

10.5

20+96.6

84
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25

21.6
3
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	+	×	−	R	E	G	GR	CUM
		100						
383		104,22		✓ 4,67	100,10 ✓ 99	23	5,49	.87 ✓
384				✓ 4,70	100 02	22	,50	.80 ✓
385				✓ 4,48	100 24	21	,7	1,03 ✓
386				✓ 4,38	100,34	20	52	1,14 ✓
387				✓ 4,21	100 51	19	53	1,37 ✓
388				✓ 4,30	100,42	18	54	1,24 ✓
389		8 ⟌ 5097		✓ 4,42	100 30	17	55	1,13 ✓
390		637		✓ 4,20	100 52	16	56	1,36 ✓
391				✓ 430	100,42	15	57	1,25 ✓
92				✓ 4,45	100,27	14	58	1,13 ✓
93				✓ 435	100,37	13	59	1,24 ✓
94				✓ 4,83	99,89	12	60	.77 ✓
95				✓ 4,85	99 87	11	61	.74 ✓
96				✓ 482	99 92	10	62	84 ✓
97				✓ 5,30	99,42	09	63	38 ✓
98 TP	3,87	103,58	5,04	✓ 5,04	99 62	8	64	40 ✓
99				✓ 4,20	99 35	7	4,48	,28 ✓
400				✓ 4,36	99 25	6	49	,19 ✓
1				✓ 4,45	99 10	5	50	,05 ✓
2				✓ 4,35	99 20	4	51	,14 ✓
3				✓ 4,19	99 36	3	52	,33 ✓
4				✓ 4,53	99,02	2	53	,00 ✓
5				✓ 447	98,08	1	54	,07 ✓
6				✓ 429	99,26 99 00		55	,24 ✓
7				✓ 4,36	99 19 98 99		56	,20
8				✓ 4,25	99 30	98	57	,32 see XX

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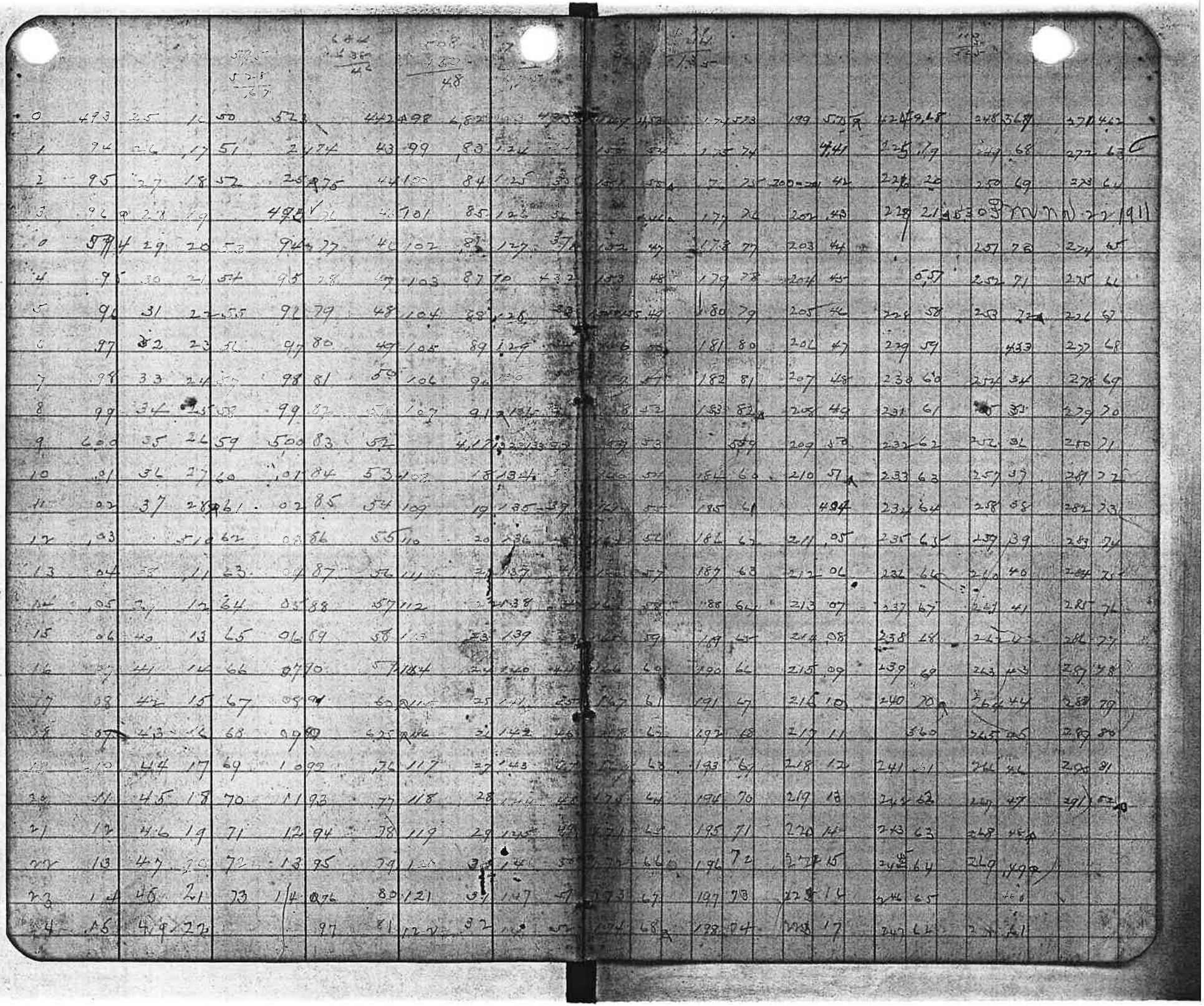
78.37



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School Dist 121 Gallsville

From Roxburg 16

to 11 25 162 miles 16.20

1 day 5.00