

Sambo 2 + 35

- 5 = Ascend
- 32 = Top Spur
- 40 = 1/2 Cor

5" Laurel $\approx 50^\circ E$ 21 \times
 5" " $S 60^\circ E$ 13 \times

- 46.5 = Creek C.S.
- 63 = Trail up Cor Cr CSE
- 71 = Creek 1 \times wd C.S.
- 75.5 " 1 \times W @ S
- 80 = Cor 1, 2, 35 + 36

16" Fir $\approx 30^\circ E$ 48 \times = 31.7
 8" \times $S 20^\circ E$ 13 \times = 8.6
 5" F $S 22^\circ W$ 26 \times = 13.2
 10" \times $\approx 20^\circ W$ 30 \times = 19.8

E bed 1 + 36

- 6.5 = Top Spur
- 21.5 = Cor or Trail CNE
- 22.0 = Field
- 27. = Leave "
- 35.5 = Sampson French's $\approx 57^\circ E$
- 40 = Cor 8" F. $N 43^\circ E$
 12" F $S 40^\circ E$ 12 \times

43.5 = Cor or (Island in middle)

- 80 = Cor Top 31, 32 R, 3 + 4
- 5" willow $\approx 48^\circ E$ 14 \times
- 5" " $S 48^\circ E$ 11 \times
- 5" " $S 50^\circ W$ 9 \times
- 5" " $N 45^\circ W$ 13 \times

②

Cor → 2, 3, 34, 35

6" R N40E 130 Z

10" R S25E 15 Z

5" R S62W 14 Z

5" R N22W 23 Z

W to E

76 Cho = low er

80 = er above

Fr. Cor 1, 2, 3, 5, 36
Ran S. bet 1 & 2

19 = Trail up Corn Cr.
25 = Corn Cr. Bottom
32 = 10 = Corn Creek

40 = Cor { 6" Yew S50 E 37 X
5" Fir S75 W 9 X

44 = Creek 4 X wd.

80 = Cor -1, 2, 11, 12 -

6" Fir N22 E 8 X

5" " S70 E 8

12" Fir S62 W 42 X

10" Chinks N53 W 15 X

E bet 1 & 12 = Random Line

40 = 1/4 cor Temporary

80.6 intersect Line 20' Sks
S of Cor 1, 6, 7 & 12

S 89 - 57 1/2 W true line

35.6 = top ridge

36.1 = beg descent

40.3 = 1/4 Cor 5" Fir N55 E 8 X
12" Fir Oak
S35 E 12 X

49.3 beg. descent

60.6 = top

80.6 = Cor 1, 2, 11, 12

(4) From cor to 31+325 Rep 3+4W. 1871

2 ran S. on W bar T32/123W

S. on true line bet 1+6

5 = foot deep mtn.

22.5 = Top of cone CNE +1000

35 = a spring C ENE

40 = 1/2 cor

10" F. $\approx 68^\circ E$ 8% ≈ 5.4

8" chink S 65W 4% ≈ 2.5

LET
4
COR
SEC!

58 = creek ³² CSE

64.72 " " CSE

68.25 " " C ENE

80 = cor. 1, 6, 7+12

30" F. $\approx 22^\circ E$ 20%

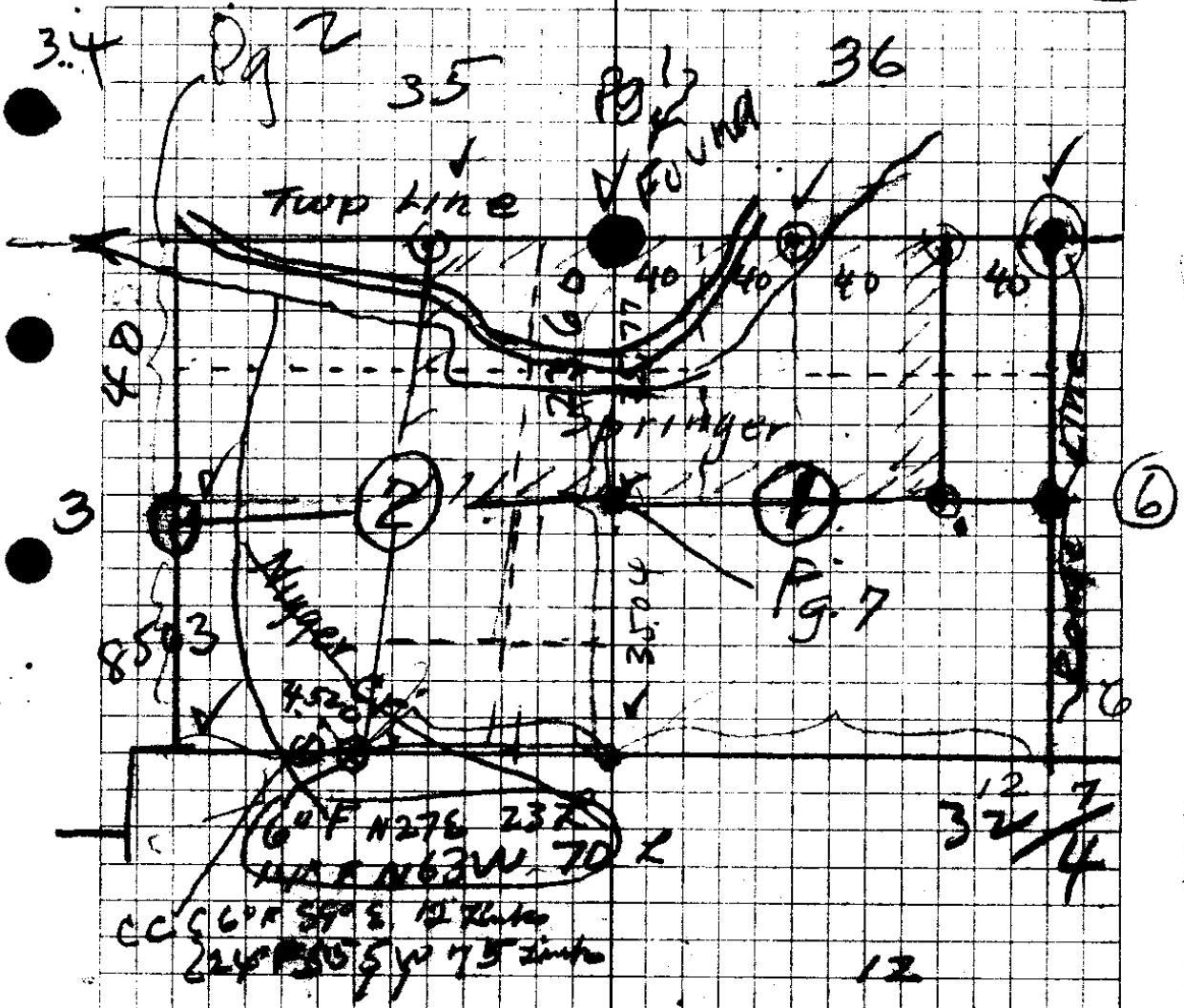
6" ch. S 10°E 37%

8" F S 50W 35%

5" C. $\approx 65^\circ W$ 41%

40
35
~~15~~

2
4
8



N 89° 58' E on R line bet 2 & 11
 40. Chs = 1/2

84.20 = N+S Line 29 X N of 2/1
 11/12

W- N 89° 50' W on TRUE line bet 2 & 11
 4.5 = Bottoming

12.5 = Top Ridge

33.5 Ravine c.s.

37 = Top Spur

Ca 4.22 St Madrone etc from which
 24" Ced. from 290° W 31 X

10" Mad 583E - 81 X

58 = wood

84.2 = Col.

(b) From $\frac{1}{4}$ Sec cor bet 2+3 F ran.:

South bet 2+3

3.5 = top spur

13.5 = creek - 3 L. CC

21.80 = Top spur

28.40 Butte Canyon

35.04 Intersect E+W Line 531 Lks

S 89:50' E of Top cor of 23, 10+11

Set a madrone Plot

12" Fir N 77 E 33 L

6" " N 63 W 9 L

This cor is on NE slope of spur
150' above butte canyon

S bet 2+3

South bet 2+3

1.0 = cor cr.

5.0 Top Bottom

20 = Top Spur

31.5 = Creek

32. begin ascent

40 = $\frac{1}{4}$ cor bet 2+3

6" Chink N 82 E 44 L
24" F West 32 L
1871

Retracement E Line 2

USE THIS

7

From 1, 2, 35, 36
Ran S - bet 1 + 2

35.77. ~~at~~ $\frac{1}{4}$ Cor } Cⁿ Yew Tree
Yew Post } S 50 E 37 $\frac{1}{2}$ = 24

S' Fir S 75 W 92 = 59

75.22 = pr S $\frac{1}{2}$ W. of Cor
Secs, 1, 2, 11 + 12

Note: The above $\frac{1}{4}$ Cor is on East
Side Creek - abt $\frac{1}{4}$ 100' E of Creek
on side hill, just East of a 24"

Fir windfall - Fir + Yew Wood BTS OK.
Orig Yew wood Corner Post still standing
Drive another 4" x 4" Yew Post beside
Orig Post, Sept 23 - '40

Mon. Sept 22 1940
Buyer S.H. Habinger

Claire Lumber Co.

11 S 4° 30' E 47.5 F - S 4° 17' E

10 Δ 5° 41' R
S 10° E 242.4 - 8° 00' = 240.0 S 9° 58' E

35'S } 1675.5 S } 75' S = Creek Center Δ 9° 37' L
= R Bank 9 = { 34.8 W }

South 234.6 - 3° 45' = 233.3
Δ 35° 36' R

S 35° 30' E 300' - 3° 30' = 299.4
237. Flat (20) S 35° 57' E
= 226.7

7 Δ 43° 40' L
S 8° W 257.3 13° 05' = 250.6
974 S 7° 43' W

6 Δ 3° R
S 5° W 132.0 10° = 130.0
985 S 4° 43' W

5 2° 10' R Left
S 7° W 144.9 6 1/2° = 143.7
992 S 6° 53' W

4 Δ 19° 06' R
S 12° E 144.7 5° 00' = 141.1
996 S 12° 13' E

3 Δ 34° L
S 22° W 67.8 S 21° 47' W

2 Δ 13° 22' R
S 9° W 117.3 F S 8° 25' W

1 Δ 48° 35' L

S 57° W. { 300' } 14° 00' = 970 = 291.0 } = 324.0
33' F

0 to 1-2-35-36
Sec Cor

20-39
Y 2e

183.8²
956⁵ ①

11028
14704
16542

181.2268

East thru mid sec line

1871.0	12	sec 1 -		19.2
		E 280.8	4°-00' .997	279.9
1591.1	11			14.6
		E 43.8 F		43.8
1547.3	10			14.2
		E 164.8	17°-00' .956	157.5
1389.8	9	= 1389.8		12.8
		E 293.0	13°-15' .973	285.0
1104.8	8			10.2
		E 127.5	11°-15' .981	= 125.0
979.8	7	= 979.8 E = End Sect 23.		24.0
		E 359.6 F		
620.2	6			5.7
		E 243.5	-18° .951	231.5
388.1	5			3.6
		E 51.6 F		
337.1	4			3.1
		E 84.2	23° .921	77.5
54.6	3	Δ 6° L	10	2.4
		S 84° E	67.3 - 31 1/2	57.4 57.0
	2	Δ = 12° R	.853	
		N 84° E	67.3	31 1/2 57.4 57.0
145.6	1	Δ 6°-00 L	.853	1.3
		E 9st 176.3	34°-20'	145.6
V4 Cor		bet 1 & 2	.826	

684.5
2100
1415.5

2360
1675.5
684.5

Dick DeHrig
2

2424 3
990
218160
21816
2399760

Sept 22.
1940.

2369.6

181.2

2550.8

2491.6

59.2

15 = Corner $\frac{1}{4}$ cor bet 1 & 2 181.2

S48°E 183.8 90°30'

986

14

2369.6 S.

13 =

S11°E 2052 Flat S11°16'E

12

$\Delta 27^{\circ} 38' L$

S16 $\frac{1}{2}$ °W 720.6

8°30' = S16°22'W
218.1

989

11

$\Delta 20^{\circ} 59' R$

$$\begin{array}{r} 13.20 \\ \underline{3} \\ 395.0 \end{array} - \frac{3}{4} \text{ MI}$$

$$\begin{array}{r} 2874.4 \quad 7 \\ 208.1 \quad 2 \\ 214.6 \quad 4 \\ 206.2 \quad 1 \\ \hline 3503.3 \end{array}$$

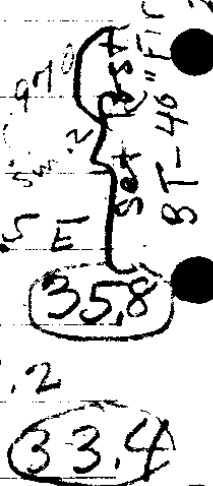
$$\begin{array}{r} 209.4 \quad 6 \\ \underline{794 \quad 6} \\ 8376 \\ 8846 \\ 8846 \\ \hline 208,1456 \end{array}$$

$$\begin{array}{r} 216.8 \\ \underline{270} \\ 19512 \\ \underline{19512} \\ 2146320 \end{array}$$

$$\begin{array}{r} 219.9 \quad 3 \\ \underline{938 \quad (6)} \\ 17592 \\ 6597 \\ \hline 19791 \\ 2062662 \end{array}$$

36	= 4955.7			
	1762	-33	.839	= 147.8
35	E 122.2		28° .883	= 107.9
34	E 563		17°45' .952	= 53.6
33	Δ 8°L			
	S 82°E	77.3F		= 76.6 East
32	Δ 16°R			
	N 82°E	80.5	16°00' .961	77.36 = 76.6 East
31	Δ 8°L			
	E 87.9	- +27°		= 78.3
30	= 4415.2		.891	End Dep - 24
	E 154.4		21½°	930 = 1436
29	E 244.1		6°25' .994	242.6
28	Δ 14°L			
	S 76°E	70.7F		= 68.5E
3.3 N 219	Δ 28°R = 39	60.5		
	N 76°E	70.7		F. - 68.5E
38920	Δ 14°L			
MKA 21	E 257.7		3°15' .998	257.2
3634.25	E 136.0		14°50' .967	= 131.5
24	= 3503.3			

MOVE 4331
 39 N 54 E
 24 N 66 E



~~1389.8~~ 2
 157.5 0
 43.8 6
 279.9
 106.9 7
 55.8
 249.2
 74.2

 2357.1

145.6 7
 114.0 6
 77.5 1
 57.6 3
 231.5 2
 359.6 5

 979.8 8
 125 6
 285

 1389.8

 3 50
 240.4

 59.6

	24 = 3503.3				(32.2)
	E 219.9		20° 15'		206.2
3297.1	23		.938		(20.3)
	E 216.8.0		8° 00'		214.6
3082.5	22		.990		(28.3)
	209.4		6° 00'		208.1
	21 = 2874.4		.994		(26.4)
	E 59.9	F			59.9
2814.5	20				(25.9)
	E 200.7		22° 30'		185.4
1629.1	19		.924		(24.2)
	E 298.0		24° 00'		= 272.0
2357.1	18	2357.1	Δ = 7° L		(21.7)
	S 83 E	37.4			37.4 = 37.1 E
	17	Δ 14° R			
	N 83° E	37.4'			37.4 = 37.1 E
2282.9	16	Δ 7° L			(21.0)
	E 251.0		6° 30'		249.2
	15				(18.7)
	N 82° E	28.2	F		28.2 = 27.9 E
2000	14	Δ 16° L			
	S 82° E	28.2	F		28.2 = 27.9 E
1977.9	13	Δ 8° R			(18.2)
	E 122.3		29°		106.9
	12		.874		

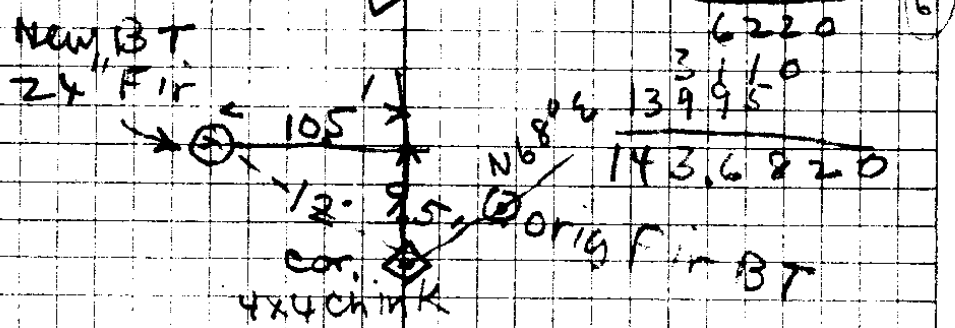
$$\begin{array}{r} 90.00 \\ - 1.24 \\ \hline 88.76 \\ - 1.58 \\ \hline 87.18 \end{array}$$
 ca 024 1.0
 143.7 } 1059 998

$$\begin{array}{r} 185.6 \\ - 9.40 \\ \hline 176.20 \\ - 167.22 \\ \hline 9.98 \end{array}$$

$$\begin{array}{r} 143.7 \\ - 10.89 \\ \hline 129.33 \\ - 114.96 \\ \hline 12.9893 \end{array}$$
 143.7 6
 998 8
 11496 3
 12933
 2933
 143.4126

$$\begin{array}{r} 174.6 \\ - 10.24 \\ \hline 164.36 \\ - 134.92 \\ \hline 29.44 \end{array}$$

$$\frac{1}{2} \text{ ca } \text{ feet}$$



$$\begin{array}{r} 155.5 \\ - 9.24 \\ \hline 146.26 \end{array}$$

$$\begin{array}{r} 4 \overline{) 5273.7} \\ \underline{1318.4} \\ 3955.2 \end{array}$$

$$\begin{array}{r} 35.8 \\ - 8.5 \\ \hline 27.3 \\ - 4.2 \\ \hline 23.1 \\ - 72.1 \\ \hline 36.9 \end{array}$$

$$\begin{array}{r} 35.8 \\ - 12.8 \\ \hline 23.0 \\ - 4.2 \\ \hline 18.8 \end{array}$$
 4) 52.8 South

$$\begin{array}{r} 13.2 \\ - 3 \\ \hline 9.9 \\ - 39.6 \text{ at } 27 \\ \hline 36.4 \\ - 3.2 \end{array}$$

$$\begin{array}{r} 3960.5 \\ - 3955.2 \\ \hline 5.3 \end{array}$$

10	$\Delta 7^{\circ} 20' L$			67.2 E
	N 12 ^u E	289.0		31 ^u 45 = 245.1
9	$\Delta 2^{\circ} 03' R$			14.9 E
	N 10 ^u E	65.9	18 ^u	627
8	$\Delta 9^{\circ} 28' R$		951	37 E
	N 0 ^u 47' E	273.4	14 ^u 00	265.2
7	$\Delta 4^{\circ} 20' R$			P.O.L.
	N 4 ^u W = N 3 ^u 33' W	19.9	23 ^u	202.3
6	$\Delta 6^{\circ} 30' L$			127 E
	N 2 ^u 57' E	118.3	15 ^u 45	106.7
	$\Delta 2^{\circ} 00' R$			
5	$= 7.3 E$	- DIST = 623.3 N.		
	<u>N 0^u 57' E</u>	101.2 F		<u>1.6 E</u>
4	= Boat hill under New Tree	$\Delta 0^{\circ} 57' R$		
North	186.0	32 ^u	848	157.7
3	$\Delta 0^{\circ} 17' Left$			143.8
	North 0 ^u 17' E	150.5	17 ^u	0.7 E
2	$\Delta 1^{\circ} R$ HOI Line			$\Delta 0^{\circ} 17' R$ P.O.L.
	N 1 ^u W	40.5		N 90.5
1	$\Delta 2^{\circ} L$			
	N 1 ^u E	90.5		N 90.5
1"	A ⁿ Station 27	$\Delta 1^{\circ} R =$		$\Delta 1^{\circ} E$
	N #29 USE	39.6		
27 on	Et W & S	001		

3503.3 = 5

131.5 = 1

257.2 = 7

137.0 = 2

242.6 = 5

143.6 = 5

4415.2 7

78.3 0

76.6 1

76.3 1

153.6 5

107.9 8

147.8 2

4955.7

174.6

5130.3

143.4

5273.7

1320

3

3960

3503.3

131.5

257.2

3892.0

68.5

3960.5

Synth = 42.9

580.2 (4)

290.1

96.7

131.5 2

257.2

143.6

206.6

231.2 3

257.2 4

244.1

97.4

219.6 4

219.6 9

2426.35 4

154.4 5

93.0 6

463.2 0

138.9 4

1435.920

79.36 5

99.0

696.2 4 0

696.2 4

76.5 8 6 4 0

5280

5120

11.0

5.242 (4)

14

568

242

3388

5280

4475

875

5280

4958

324

175

149

70.7 5

97.0 (8)

494.9 0

63.6 3

68.5 7 9 0

96.1 7

50.5 (1)

450.5

76.8

7736.05

67.9

89.1

87.9

72.1

76.5

79.8 9

78.3 1 8 9

5273.7) 48.5000 (0.09196
 474633

103670

52737

509330

474633

348670

316422

30548

(6)

3955.2

.0092

79104

355968

3638784

4th cor = 5273.7' E of NW 1/4 cor
 south 35.8' S

38 ~~A 10° 58' R~~

S 86° 38' E 155.5' on 22 1/2° = 143.7' } 143.4' E

37 Δ 10° 58' R

174.6' E

4.2' S

36

S 88 1/2° E

185.8'

Δ 10° 4' R

(174.6' E & 4.2' S)

185.8' East

20°

.946

88.36 E

174.6

.024

N 4 58 E

45

~~N 4 40 W~~

N 4 15 E

8 - 27

~~4 - 15~~

N 4 12 W

24 - 18

28 - 30

120.0'

W 37' - 20' out ed

1 1/2' line to

N + S. Section

C. S. File No. 34/22

120

220.8

100

120.2

189

1429.8

1400

100

1600

1000

1000

1000

157

1000

cor

1430 E of 1/16 cor

113.6

110

300. F

225.6 F

300' F

2 = 340.8 E

E 223.0 8000' = 2208

1

990

E 120.0 F

1/16 cor

39.6
 181.0
 143.8
 157.7
 101.2

 623.3 N

14.9 = 9
 523

 67.2 = 10
 6.3

 73.5 = 11
 10.4

 83.9 = 12
 11.7

 72.2 = 13

5' W at Beg.
 2.3

 7.3
 6.3

 2.57

 3-33
 8
 4-20
 3-33

 N 0-47
 9-28

 10-15
 2-43

 N 12-78 E
 7-20

 N 4-58 E

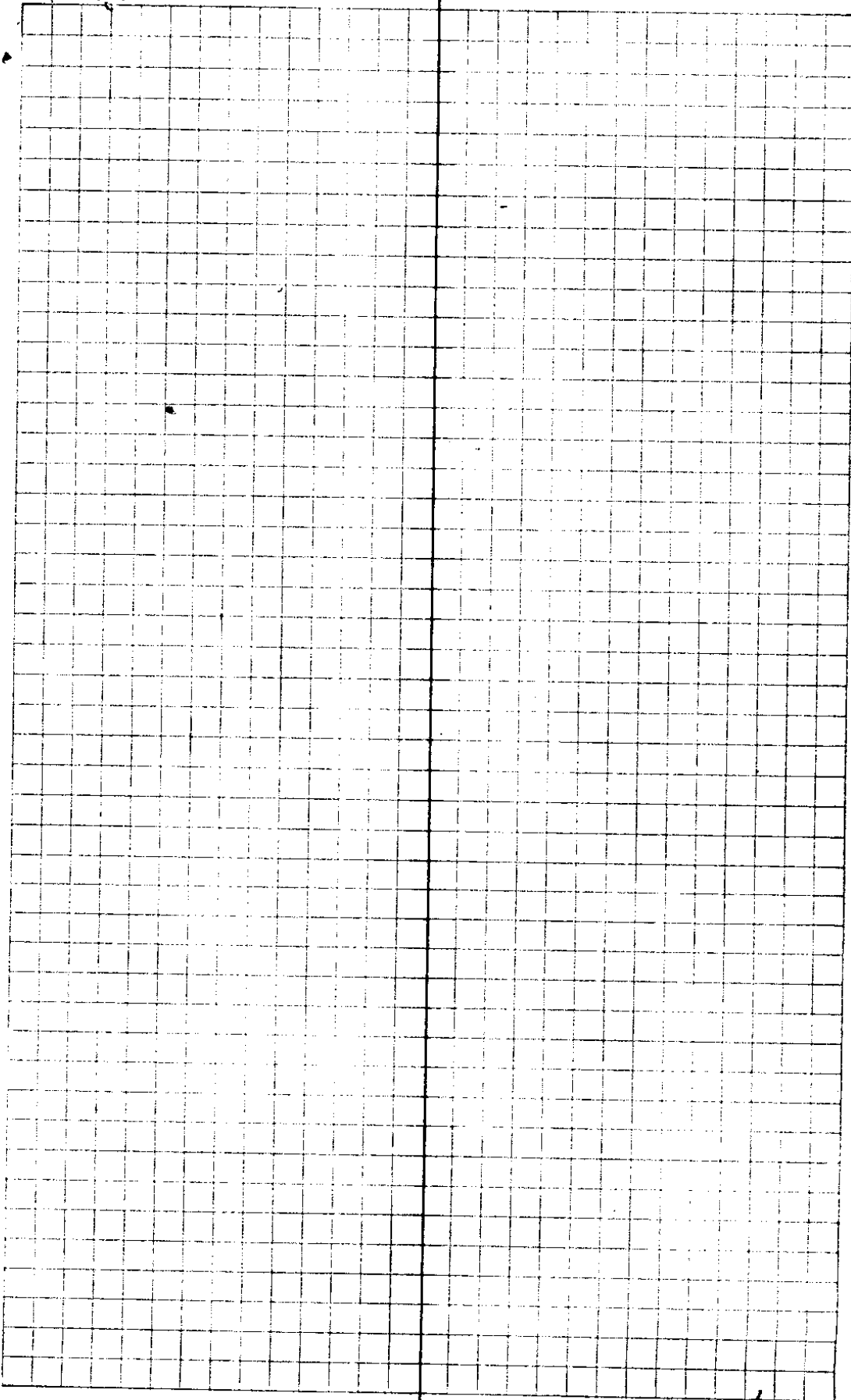
429
 364

 6.5

 144 90.500 95.8
 24.96
 5540
 4720
 6200
 2552
 548

17	253.5	6°00'		P.O.L
16	N 120.8	F		P.O.L
15	North	206.8	8°45'	
14	Δ 28°30' R			P.O.L
	N 28-30 W	164.0	17°00'	156.7
13	Δ 24°18' R		.756	12.2
	N 4°12' W	170.3	19°15'	160.7
12	Δ 8°27' R		.944	83.9 E
	N 4°15' E	160.6	28½°	141.1
11	Δ 0°43' L		.879	73.5 E
	N 4°58' E	82.4	25°	94.3
10				

34-22



C S File No. 34/22

1166.4
 2635
1520.0

110
116.4

866.4
752
 340.8

225.6
~~340.8~~
~~225.6~~
 120

153.6
116.4
 320

340.8
120

226.70
20070
 223

0.2
 0.1
 0.1

CS FILE FOLDER

CONTAINS

MORE

INFORMATION