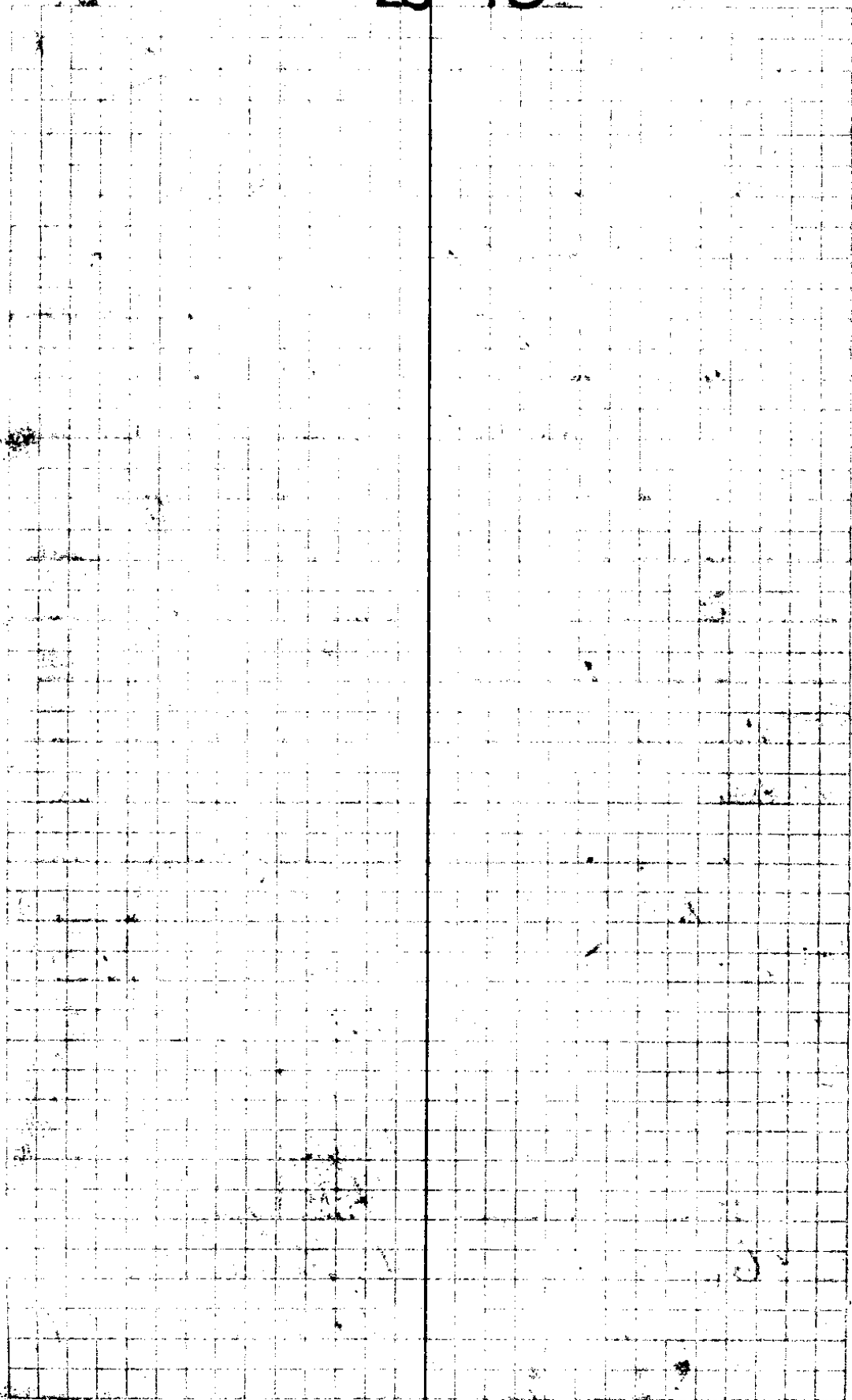


23-78



23/78

Sta	+S	H1	-S	Elev	BM
				16.04	
	6.64	22.68			
①			3.60	19.08	
	3.37	22.45			
			6.2	16.2	2 st + Bdwy
②			9.49	12.96	
	0.78	13.74			
0+0 = 35	10.43		5.38	8.36	Top Pipe Bdwy
1+30	33	7.12	3.0	10.74	Top Rail
③			3.43	10.31	
	3.87	14.18			
5+13.1 = 28	9.12		4.90	09.28	
6+00 = 28	0.43		5.40	08.8	
④			4.28	09.90	
	9.00	18.90			
7+60.2 = 26	44.1		9.2	09.7	Side Flat
8+60	25	44	9.1	09.8	
9+10	24	9.4	10.0	08.9	
9+50	24	5.4	10.3	08.6	
9+88	24	2.0	4.3	14.6	Top Rail
9+88	24	18	10.3	08.6	Ground
Stump			7.47	11.43	
	3.20	14.63			

RR here bears $N 44\frac{1}{2}^{\circ} E$

23/78

Sta	+S	H1	-S	Elev	Side Slope
		14.63			

23+44			6.0	08.3	Flat
-------	--	--	-----	------	------

22+94			5.6	09.0	
-------	--	--	-----	------	--

22+29			5.7	08.9	
-------	--	--	-----	------	--

21+79			5.6	09.0	Flat
-------	--	--	-----	------	------

⊕			2.06	12.57	✓
---	--	--	------	-------	---

	11.32	23.89			
--	-------	-------	--	--	--

21+28			13.7	10.2	Flat
-------	--	--	------	------	------

21+15			14.9	09.0	cut 8.0
-------	--	--	------	------	---------

20+74			1.7	22.2	25%
-------	--	--	-----	------	-----

⊕			1.19	22.70	✓
---	--	--	------	-------	---

	12.33	35.03			
--	-------	-------	--	--	--

19+94			4.1	30.9	26%
-------	--	--	-----	------	-----

⊕			5.29	29.74	
---	--	--	------	-------	--

	12.99	42.73			
--	-------	-------	--	--	--

19+34			11.1	31.6	F 10
-------	--	--	------	------	------

18+84			3.4	39.3	23%
-------	--	--	-----	------	-----

⊕			00	42.73	
---	--	--	----	-------	--

	11.64	54.37			
--	-------	-------	--	--	--

18+32			7.6	46.8	checked
-------	--	--	-----	------	---------

⊕			2.34	52.03	to here
---	--	--	------	-------	---------

	12.32	64.35			
--	-------	-------	--	--	--

✓

NOV 13

NOV 14

23/28

Sta	12.32	41.1	Elev	52.03	
17+76		64.35	11.1	53.2	Grade
16+69			3.2	64.2	F2.0
			0.62	63.73	
	10.39	74.12			
16+19			8.5	65.6	17%
			0.15	73.97	
	12.55	86.52			
15+70			8.0	78.5	17%
			0.32	86.20	
	12.83	99.03			
15+21			4.3	94.7	17%
14+70				101.1	24.5%
14+22			2.9	96.1	15%
			2.92	96.11	
	4.24	100.35			
13+53			4.9	95.5	14%
12+79			12.3	88.1	26%
12+16			3.8	96.6	Grade 22%
			1.59	98.76	
	12.30	111.06			
11+75			9.5	101.6	26%
11+32			4.3	106.8	17%
			0.97	110.69	

Nov 14, 36

23/78

Sta	+S	H1	-5° Elev	
		111.06	0.97	110.09
	⊕	12.17	122.26	
10+57			4.8	117.5 3
	⊕	12.03	134.10	
9+57			1.30	132.8 = 35°
	⊕	11.00	143.86	
9+18			5.2	138.7 37%
	⊕	8.81	152.65	
8+18			1.20	151.4 37%
	⊕	12.40	164.32	
-7+43			1.8	162.5 24%
7+18			0.0	164.3
	⊕	12.30	175.94	
6+63			4.6	171.3 34%
	⊕	13.16	188.03	
6+127			10.7	177.3 28°

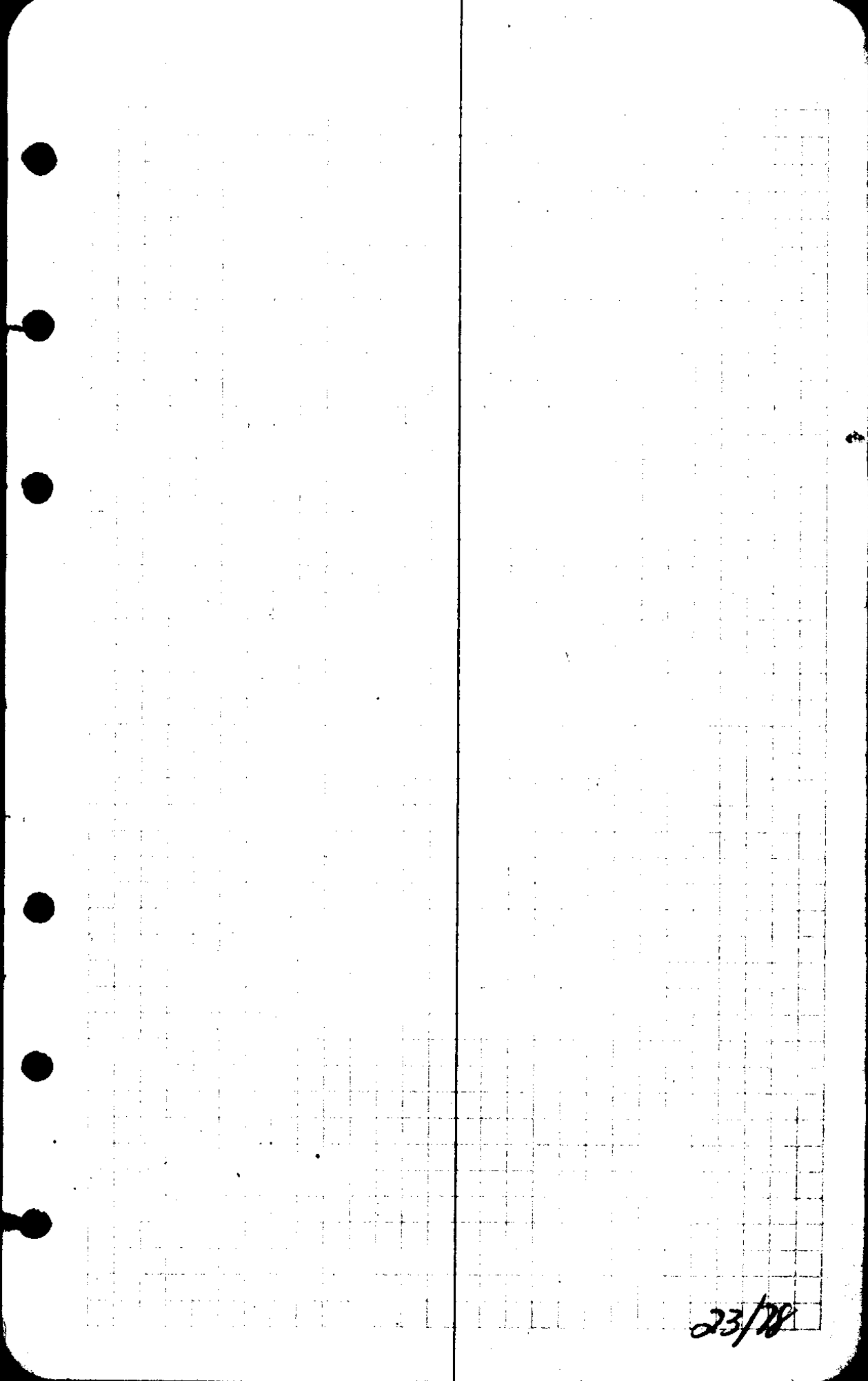
9792
12 17

110.09

Note At 7+00 Set L Point
10' to R. of Line

23/18

Sta	TS	H1	-S	Elev	
		188.03			
5+57			4.4	183.6	354
	⊕		0.2	187.82	
		12.56		200.38	
4+98			7.7	192.7	354
	⊕		0.31	200.07	
		10.66		210.73	
3+83			4.0	206.7	338
	⊕		0.14	210.59	
		12.86		223.45	
2+96			4.6	218.9	339
	⊕		0.0	223.45	
		9.30		232.75	
2+69			9.0	223.8	354
2+05			1.7	231.1	310
	⊕		1.30	231.45	
		11.90		243.35	
1+44			4.7	238.6	269
1+21			0.6	242.7	200
	⊕		0.27	243.08	
		12.46		255.54	
0+65			4.3	251.2	
	⊕		0.82	254.72	



23/18

Sta +S HI -S Elev

254.72

11.07 265.79

0+6

5.1 260.7

Grade for
Sta Site ⁴⁰₂₀

⊕

0.20 265.59

10.83 276.42

1.92 274.50

BM, used
El. 100.00
on sta
Site Work

171

$\frac{1}{4}$ Cor

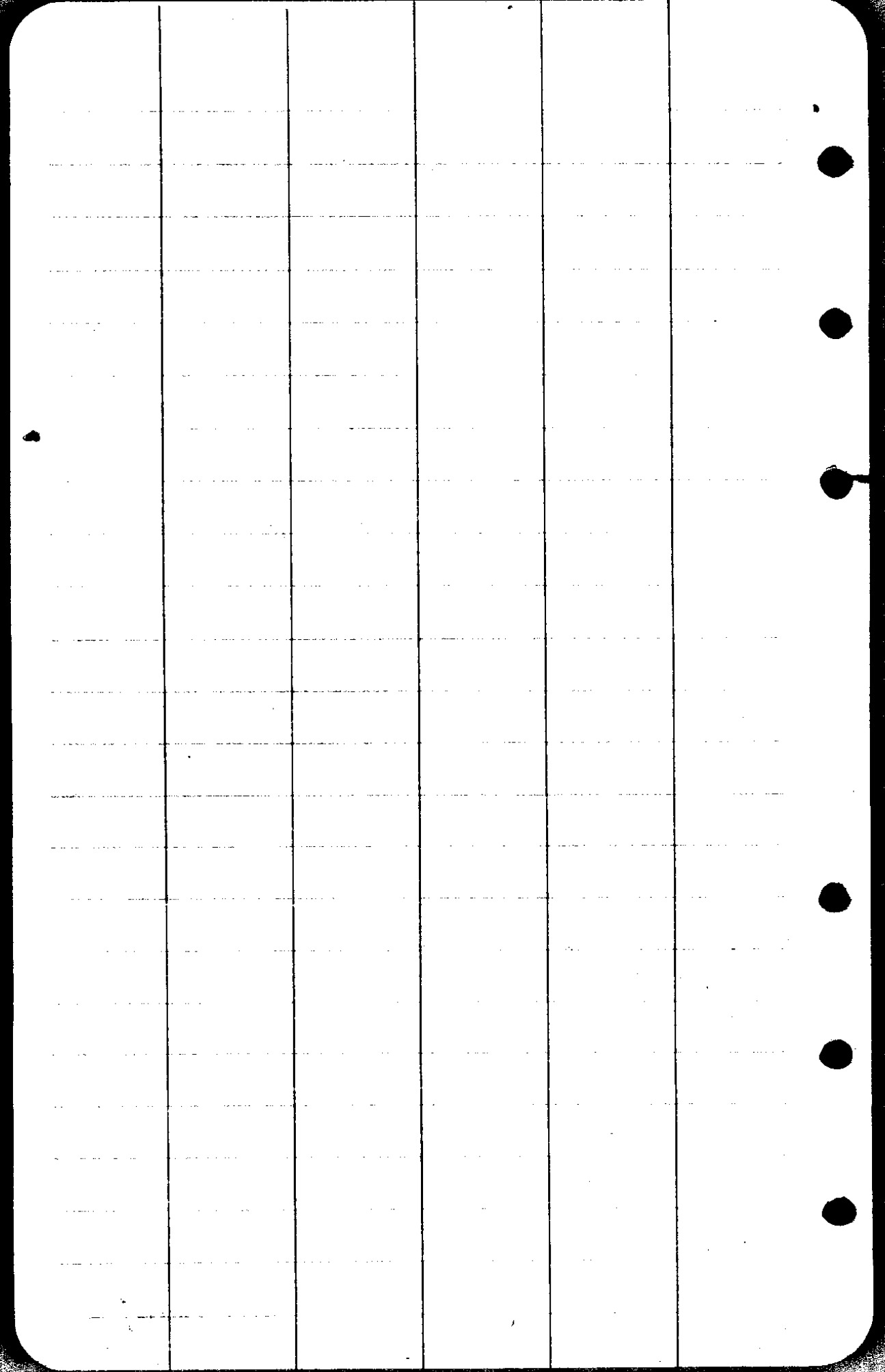


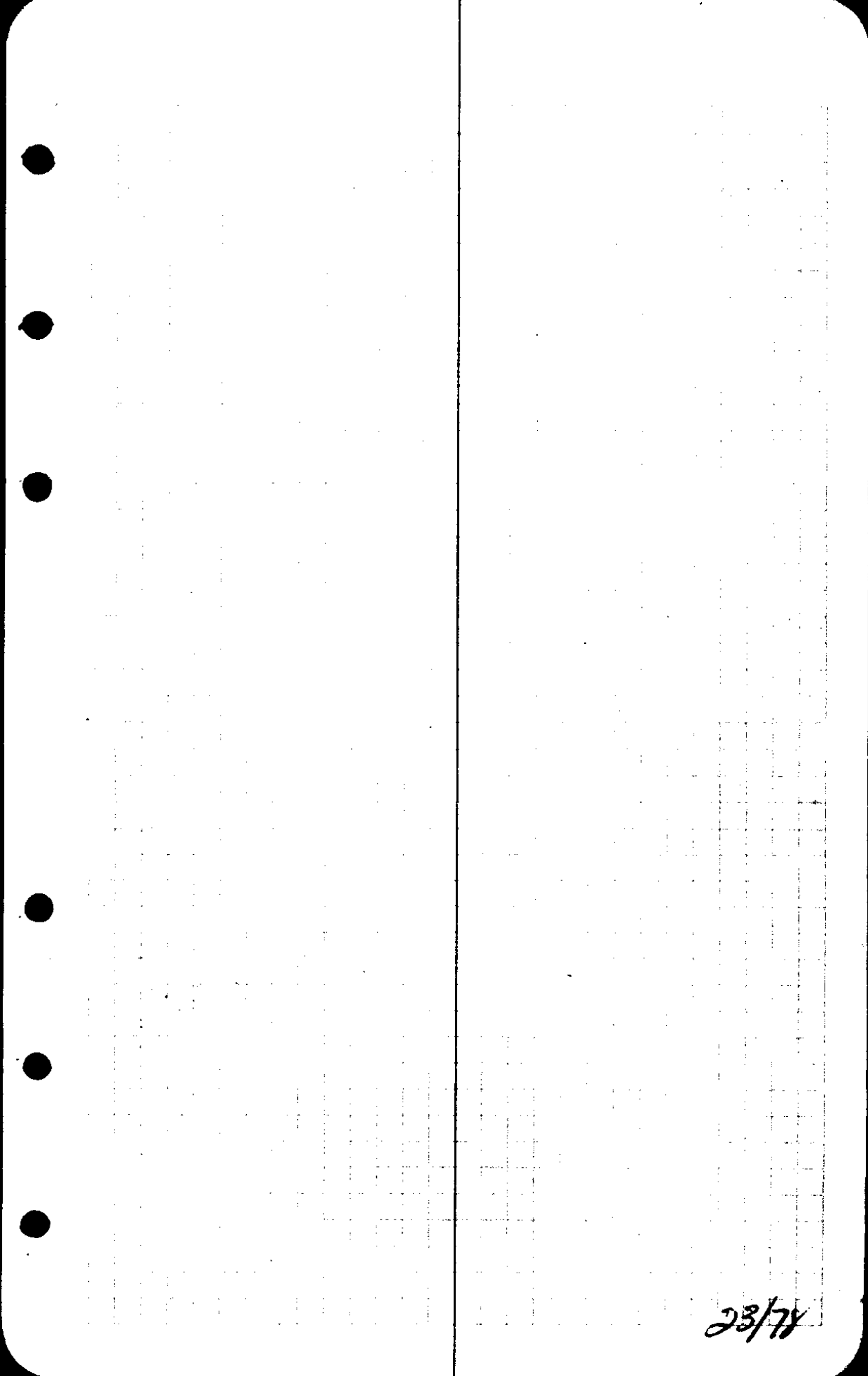
← Sta Site Grade
= -4.4 = 261.4

264

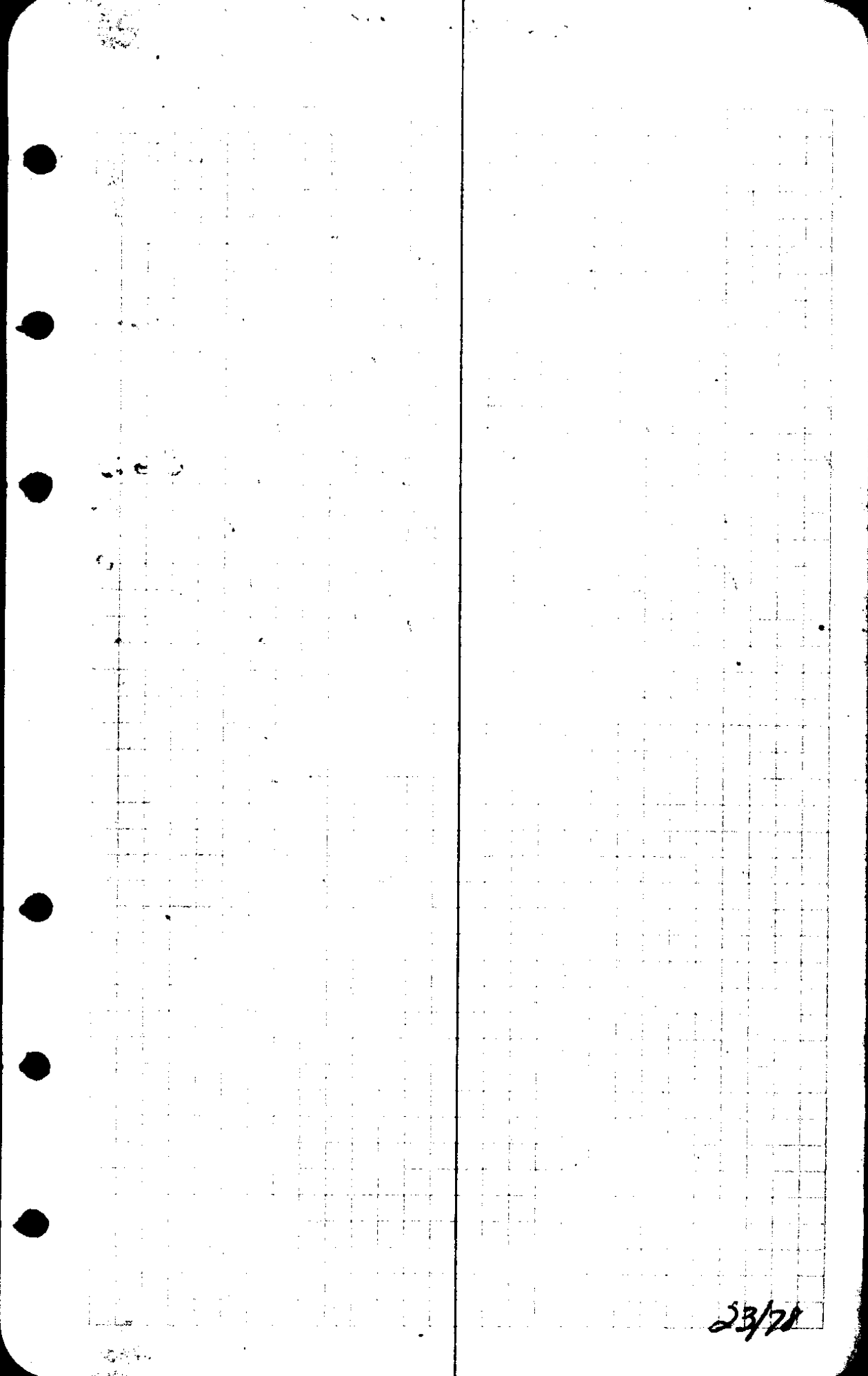


23/78





23/7x



23/78

16
26
—
10
19
—
10

300
182
—
118

23/10

Cross Sec. - Station Site

Sta	+S	HI	-S	Elev	
	0.65	275.15		274.50	B.M. ● 6" Spruce Abt 80' N Sta 1+20, Station Site
		275.15			
2+00			4.95	270.20	-261.4 = C 8.8
1+77			6.25	268.90	-261.4 = C 7.5
			5.49	269.66	
	⊙ 5.10	274.76			
1+20			5.10	269.66	-261.4 = C 8.2
0+77			5.20	269.56	-261.4 = 8.2
0+50			6.40	268.36	-261.4 = 7.0
0+0			11.40	263.36	Grade
				cut → 2.00	OK.
				261.4 ←	

Line Stationed S. to North

$$\begin{array}{r} 261.4 \\ 260.7 \\ \hline .7 \end{array}$$

NOV 12-36

23/20

0+0

1+20

0+77

10

0+50

2+13

0+0

L.

⊕

R

2
3

90

00
49.0

C63

80

00
44.0

C62

00
41

90

0.0
31.0

C5.0 +7.2
15.0

00
46.0

00

+3.7
30

+2.8
55

00
74

4.9

23/78

Cross Sec Sta Site
Stationed S to N.

1+77

80

1+20

0+77

0+50

0+0

NOV 12-36

130

$$\frac{00}{73}$$

$$\frac{+80}{310}$$

C.75

$$\frac{00}{29.5}$$

$$\frac{00}{53.}$$

C8.3

$$\frac{00}{36} = 0 \text{ to Road}$$

$$\frac{00}{49.6}$$

C8.2

$$\frac{00}{47.6}$$

$$\frac{00}{40.0}$$

C7.0

$$\frac{+9.2}{15}$$

$$\frac{00}{53.5}$$

$$\frac{00}{90}$$

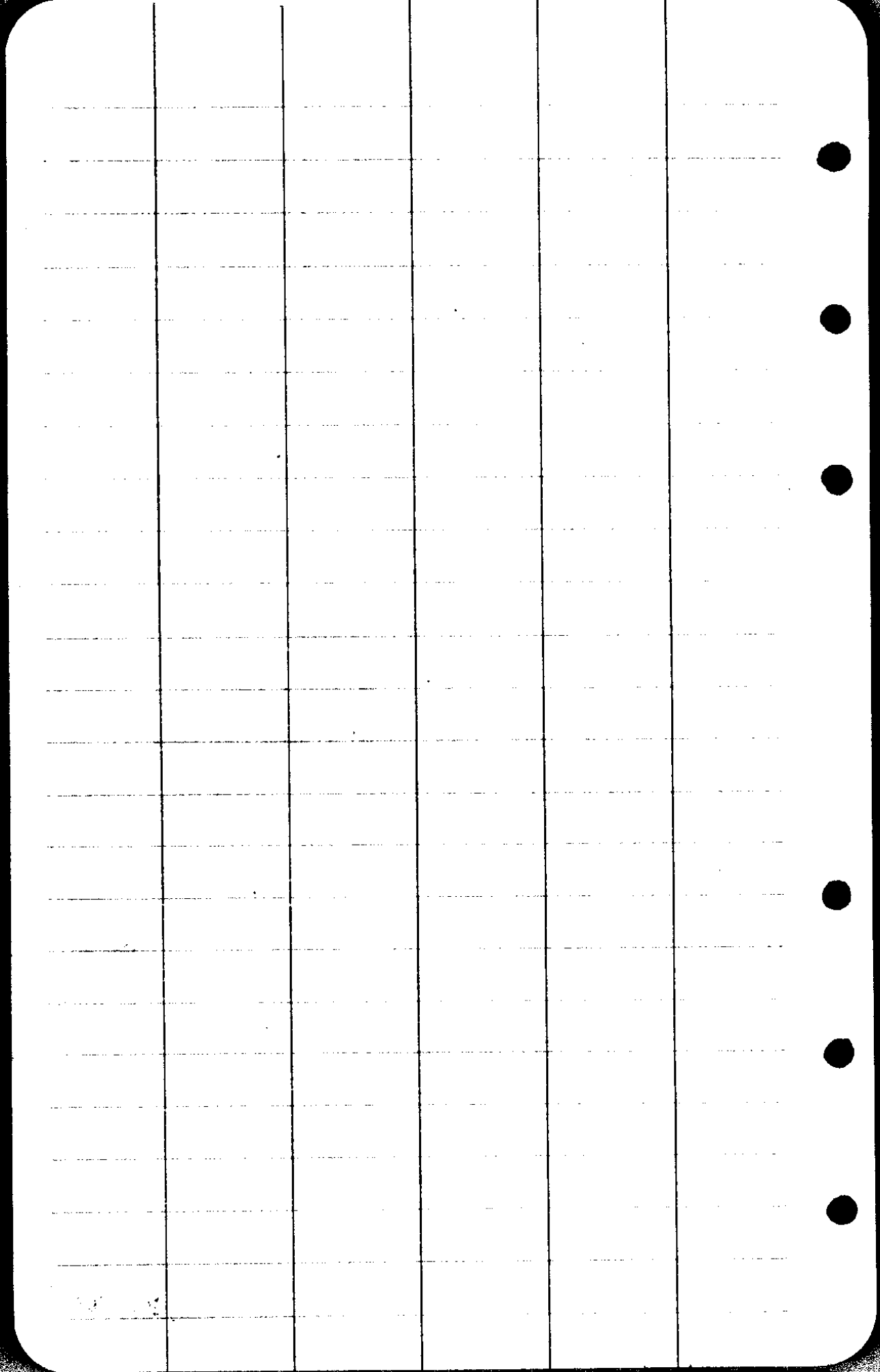
C2.0

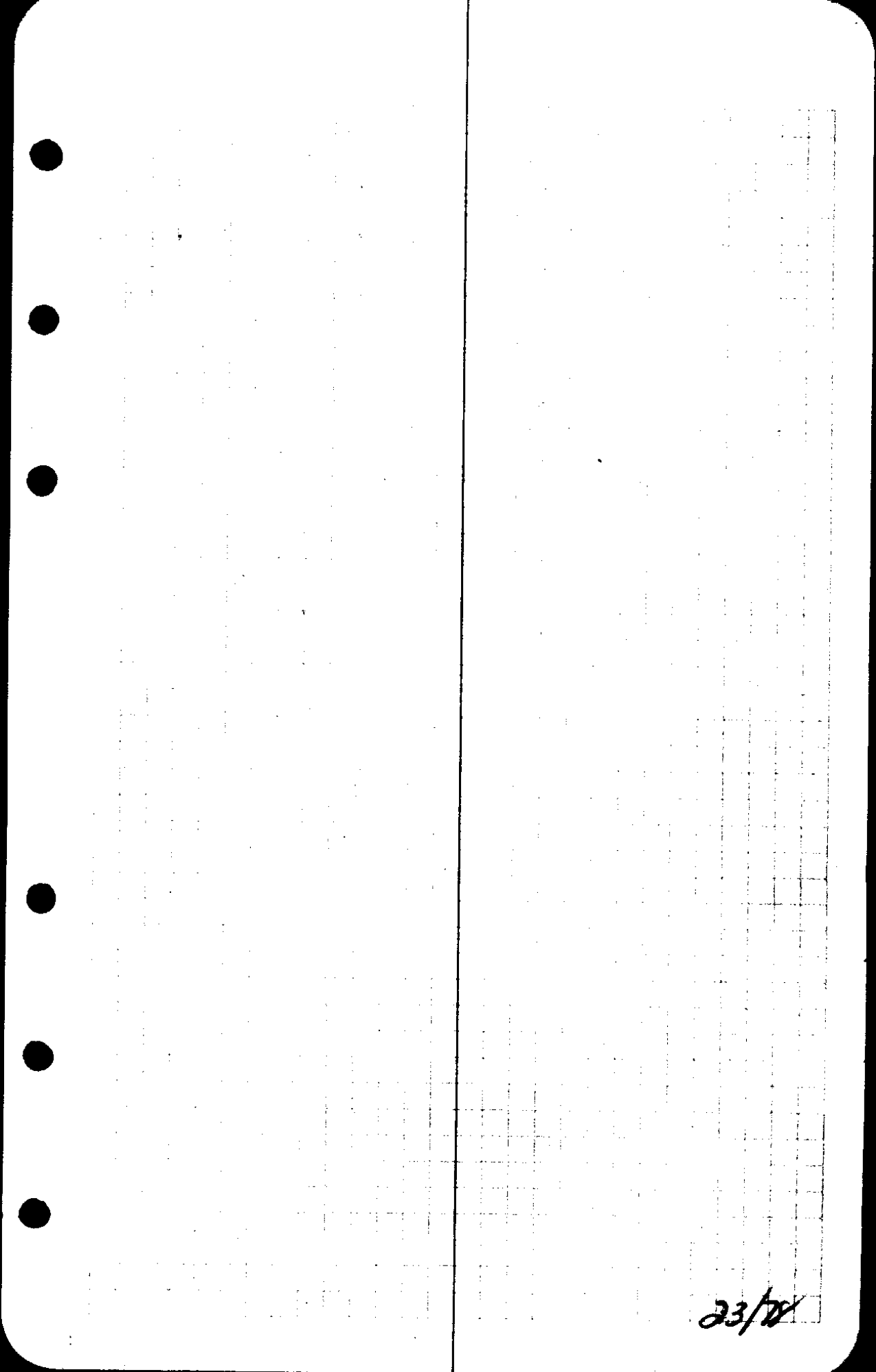
$$\frac{+5.7}{30}$$

$$\frac{+48}{55}$$

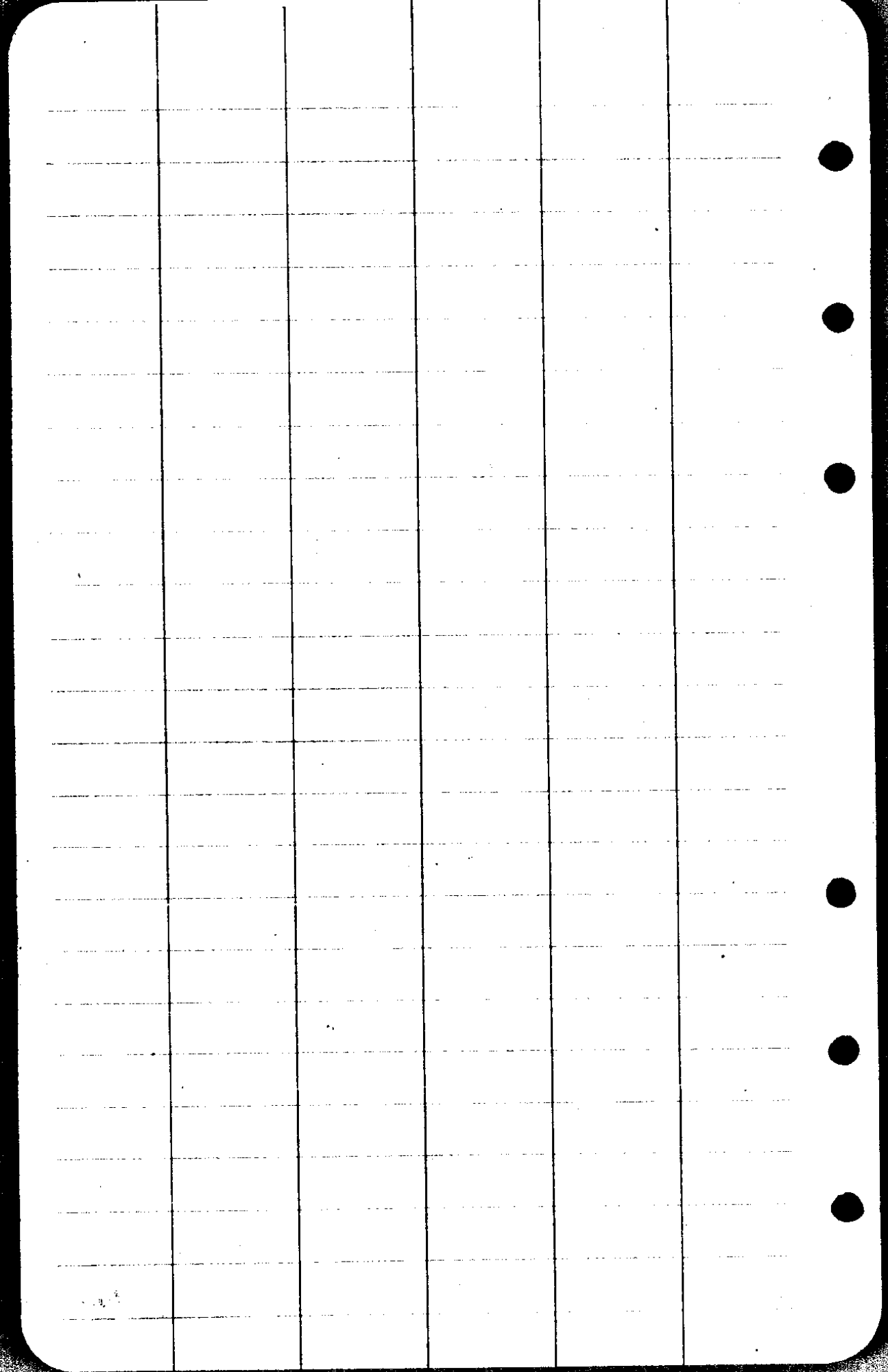
$$\frac{00}{82.0}$$

23/78



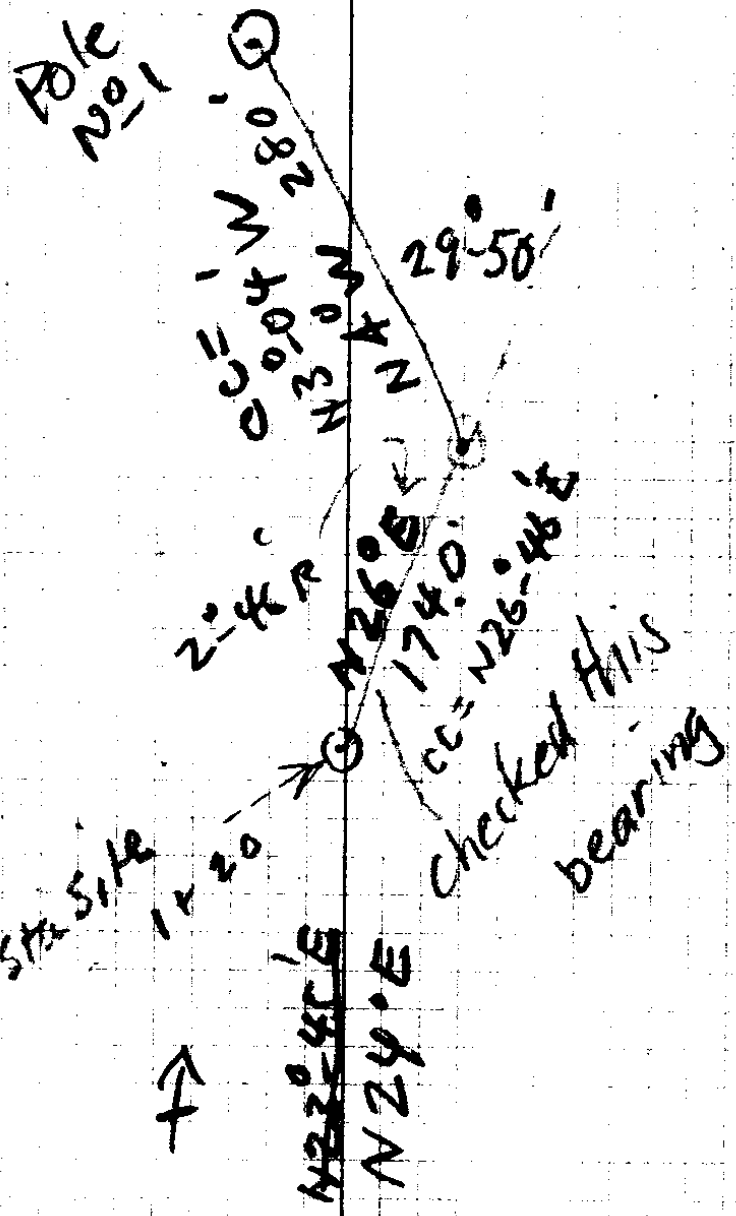


23/10



29-50
26-46

3-04



23/78

POINTON SEC Line = hub
6+127

S 20° W, 55.7' N 14° 59' E S.S.

5+57 Δ 45-55 R 28%
55.7 S 26° E 59' N 25° 56' W

4+98 Δ 34-53 R 24%
59 S 61° E, 55 N 60° 49' W

4+43 Δ 19-68 R
5 80° E 60 N 79° 57' W

3+83 Δ 8-15 R 24%
60 S 88° 15' E 87 N 88° 12' W

2+96 Δ 51-37 L
57 S 37° E 27 N 36° 35' W

2+69 Δ 31-20 L 36%
27 S 5° 15' E 64 N 5° 13' W

2+05 Δ 30-30 L
S 25° W 61 N 25° 17' E

1+44 Δ 16-55 R ✓ 26%
61 S 8 1/2° W ✓ 23' N 8° 22' E

1+21 Δ 40-19 R 20%
3 S 32° E 56° N 31° 57' W ✓

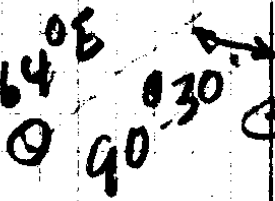
0+65 Δ 12-47 R
17-30 R N 14° 30' E 65° N 14° 27' W = R
N 14° 27' E ✓ R

0+0 Δ = 51-52 R 20%
S 66 1/4° E 36' N 66° 19' W = Tie

Δ 89-41 R
N 24° E

Nov 11-12, 1936

Pole
No. 3 N64°E

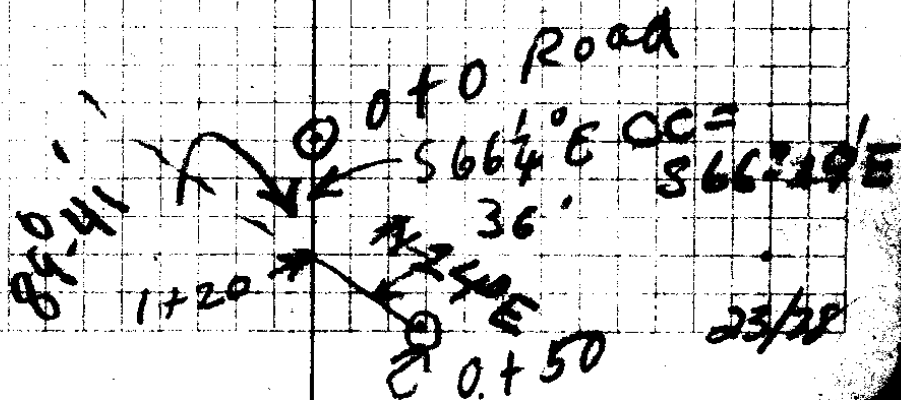
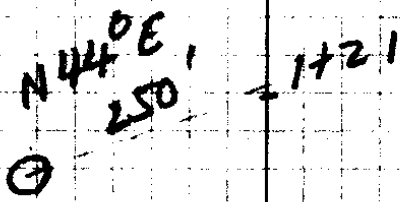


⊙ 5+57

⊙ 4+98

$$\begin{array}{r} 31-57 \\ 14-27 \\ \hline \Delta = 17-30 \end{array}$$

Pole
No. 2



12+79

S 33° W

63

N 32° 59' E

12+16

Δ 8° 30' R

63

S 24½° W

41

N 24° 29' E

11+75

Δ 38° 44' R

41

S 14° E

43'

N 55° 34' E
11+82 Power Pole

11+32

Δ 38° 20' R

43

S 52° 30' E

75'

N 52° 35' W

10+57

Δ 6° 59' R

75

S 59° 15' E

100'

N 59° 34' W

9+57

Δ 22° 09' R

100

S 80° 30' E 39'

N 81° 43' W

37%

9+18

Δ 19° 35' L

39

S 62° E 100'

N 62° 08' W

8+18

Δ 12° 05' R

100

S 73° 30' E 75.0'

N 74° 13' W

36%

7+43

Δ 107° 05' L

75

S 32° 45' W 80'

N 32° 52' E

25%

6+630

Δ 12° 25' R L

80

S 45° W 50.3'

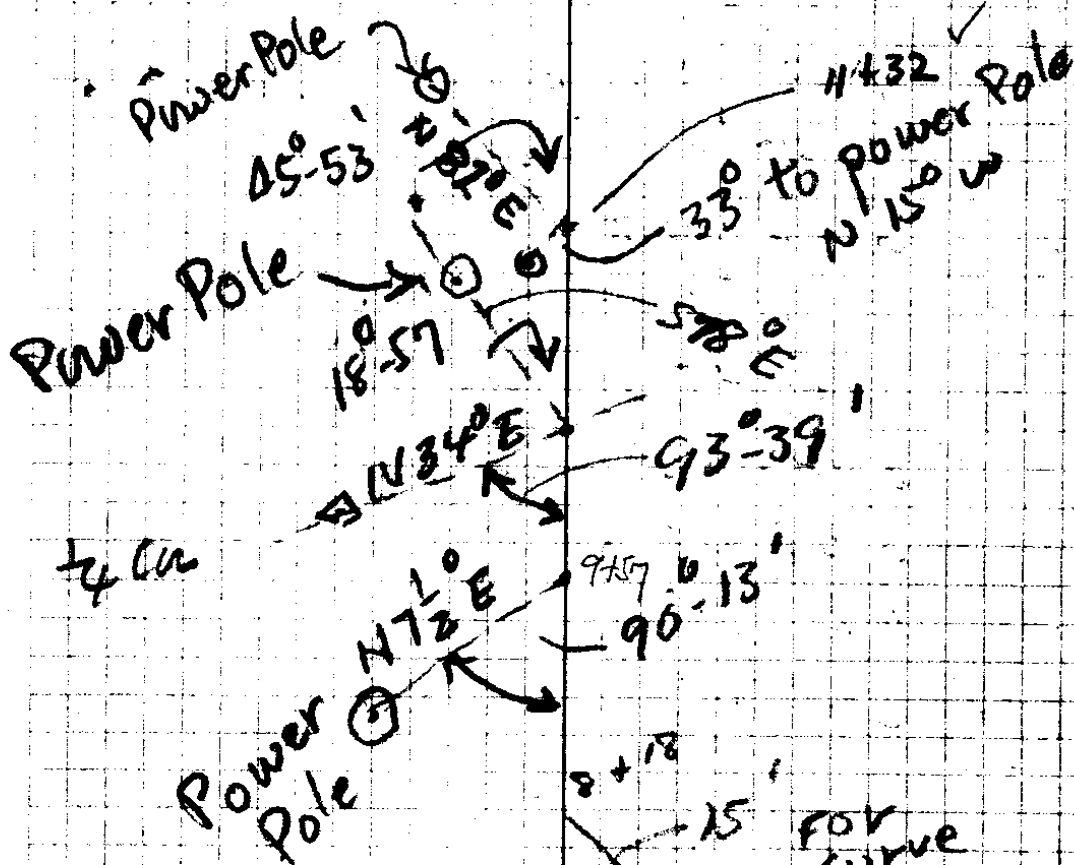
N 45° 37' E

25%

6+127

Point on Sec Line

503



S 73°-30' E 75.0
 7+43 Δ 83°-53' L 35'
 7+12.7 Δ 35°-57' L
 S 45° W 100'
 6+12.7 Δ 25°-38' R

22/10

19+34

N 70°-45' E 50' N 70°-41' E

18+84 Δ 38°-33' R

⁵⁰ N 32° E, 108.0 N 32°-08' E

17+76 Δ 30°-17' L

¹⁰⁸ N 62° E, 107 N 62°-25' E

16+69 Δ 27°-45' R

¹⁰⁷ N 34°-30' E 50' N 34°-40' E

16+19 Δ 62°-42' L

⁵⁰ S 82°-30' E 49' N 82°-38' W F 3.2

15+70 Δ 53°-57' L

⁴⁹ S 28°-45' E, 49.0 N 28°-41' W C 8.2

15+21 Δ 64°-22' L

⁴⁹ S 35°-45' W 51.0 N 35°-41' E C 19.7 2+00

14+70 Δ 27°-35' L

⁵¹ S 63°-15' W, 48.0 N 63°-16' E C 24.5 = 1+47

14+22 Δ 13°-34' R

⁴⁸ S 49°-30' W 69.0 N 49°-42' E C 18.0 1+60

13+53 Δ 19°-28' R

⁶⁹ S 30°-15' W 74.0 N 30°-14' E

12+79 Δ 2°-45' L

13+48

~~S 70°-45' W 69'~~

12+79 Δ 22°-24' L

~~⁶⁹ S 33' W 63'~~

Pole

⊙ N 13 57 E

18° 35'
18 + 84

23/78

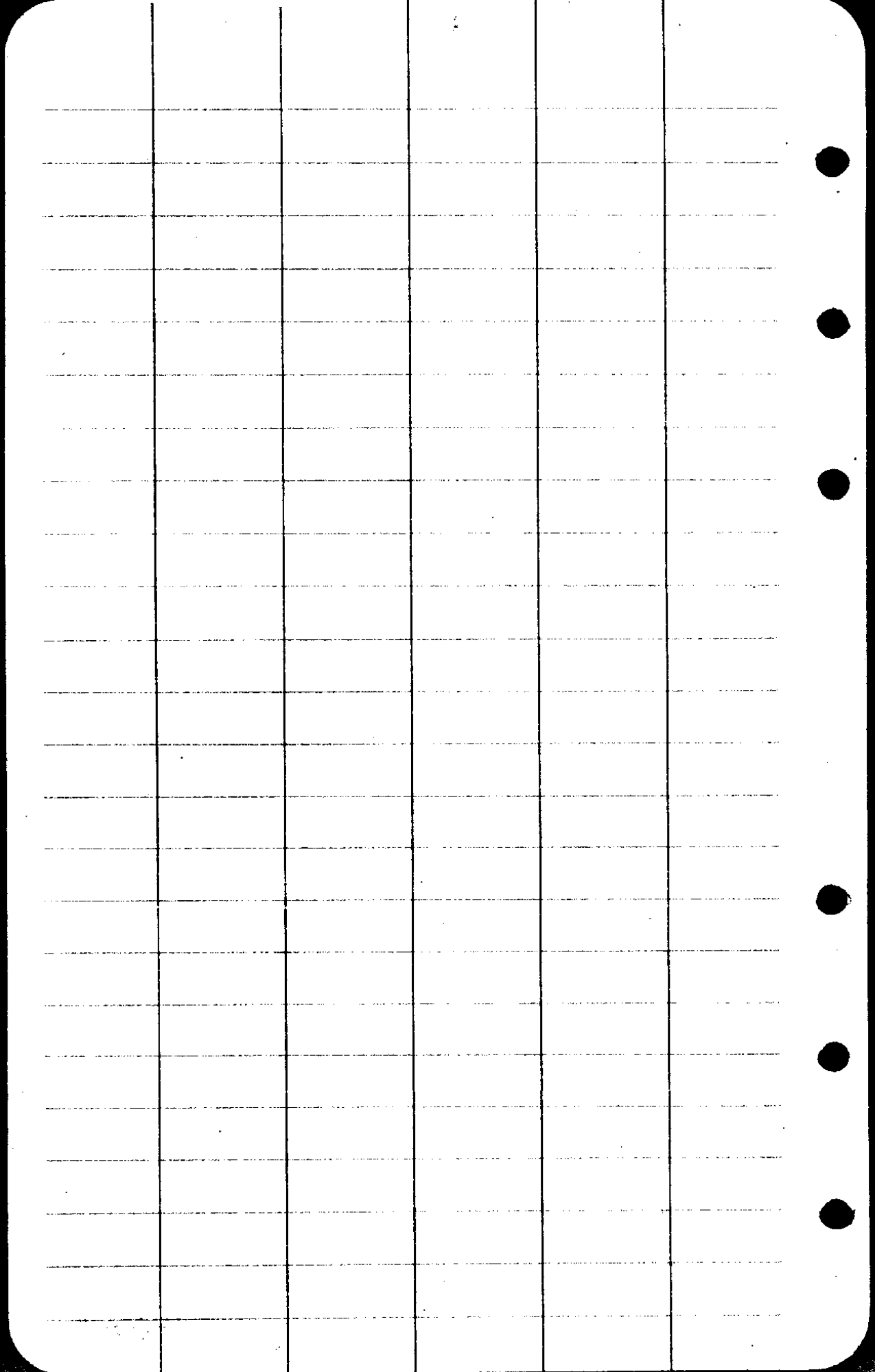
$S 27^{\circ} 15' E,$
 $(24+178) \rightarrow \Delta 5^{\circ} 56' L$
 $(9+885) S 12^{\circ} 15' E, 73.8 \quad N 17^{\circ} 20' W$
 $23+44 \Delta 10^{\circ} 57' R L,$
 $73.8 \quad S 6^{\circ} E, 50' \quad N 6^{\circ} 23' W$
 $22 \quad 94 \Delta 55^{\circ} 13' R L,$
 $50 \quad S 49^{\circ} 30' W 65 \quad N 48^{\circ} 50' E$
 $22+29 \Delta 6^{\circ} 35' R$
 $65 \quad S 43^{\circ} W 50' \quad N 42^{\circ} 15' E$
 $21+79 \Delta 67^{\circ} 51' R$
 $50 \quad S 25^{\circ} E, 51' \quad N 25^{\circ} 36' W$
 $21+28 \Delta 71^{\circ} 10' R$
 $51 \quad N 83^{\circ} E = 54. \quad S 83^{\circ} 14' W$
 $20+74 \Delta 43^{\circ} 15' R$
 $54 \quad N 40^{\circ} E, \quad 80' \quad S 39^{\circ} 59' W$
 $19+94 \quad 9^{\circ} 42' L$
 $90 \quad N 49^{\circ} 30' E \quad 60 \quad S 49^{\circ} 41' W$
 $19+34 \Delta 21^{\circ} L$
 $N 70^{\circ} 45' E \quad 50.0' \quad S 70^{\circ} 41' W$

$$\begin{array}{r} 24 + 178 \\ 2263 \\ \hline 26 + 441 \end{array}$$

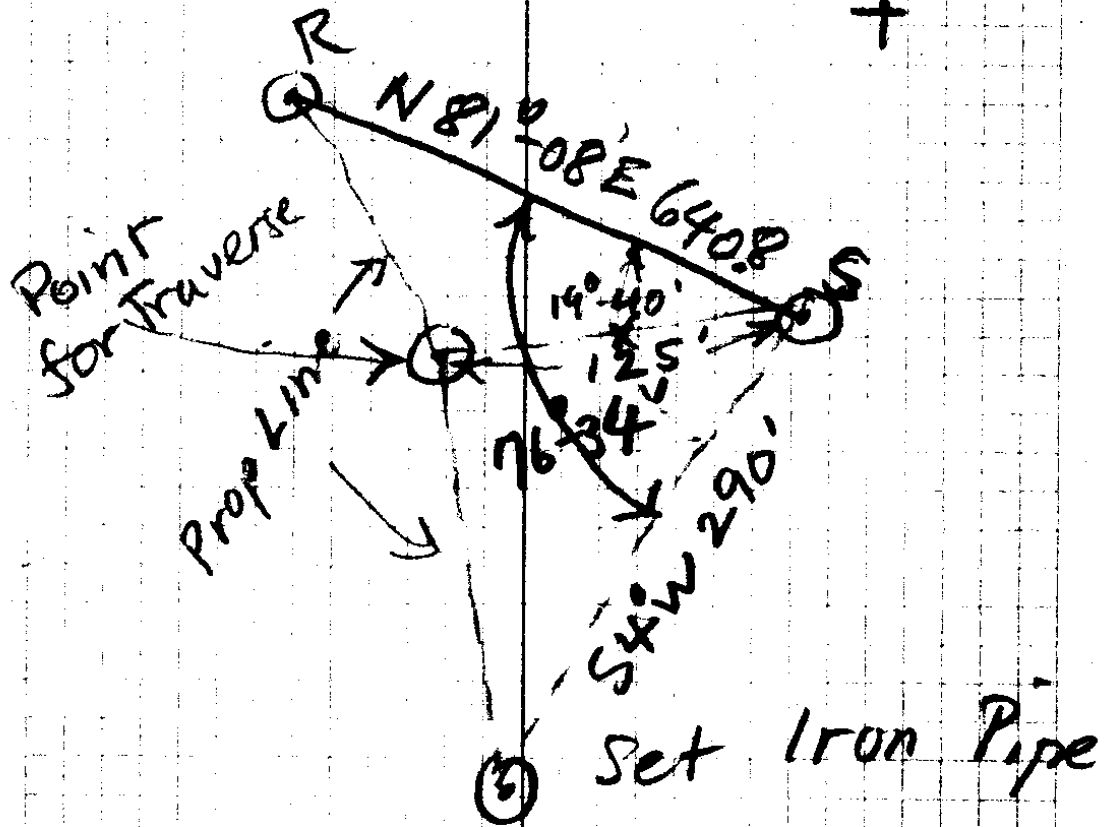
$$\begin{array}{r} 17 + 76 \\ 54 \\ \hline 1930 \end{array}$$

21 + 28
2692
⊙ Pole

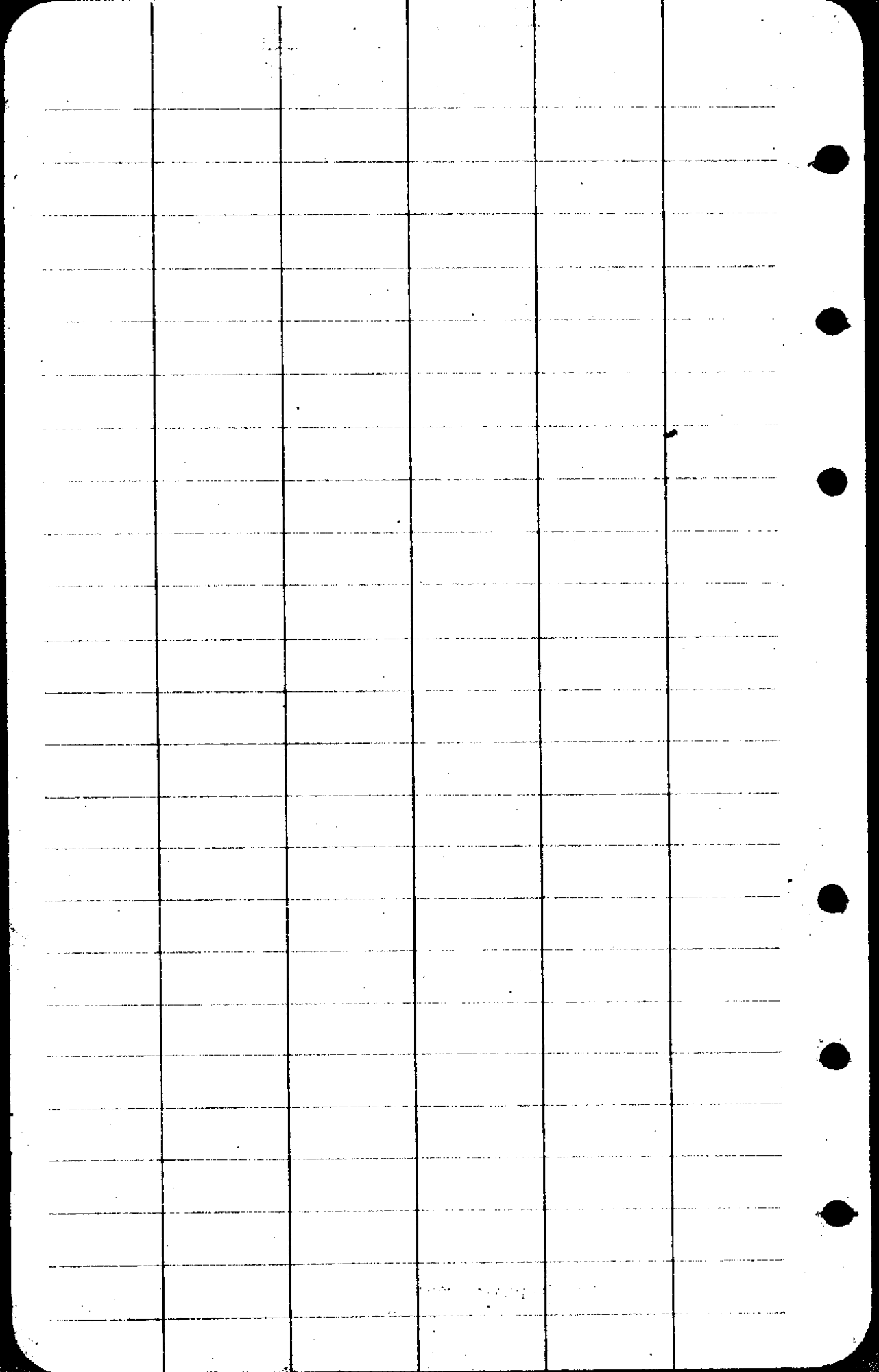
23/28



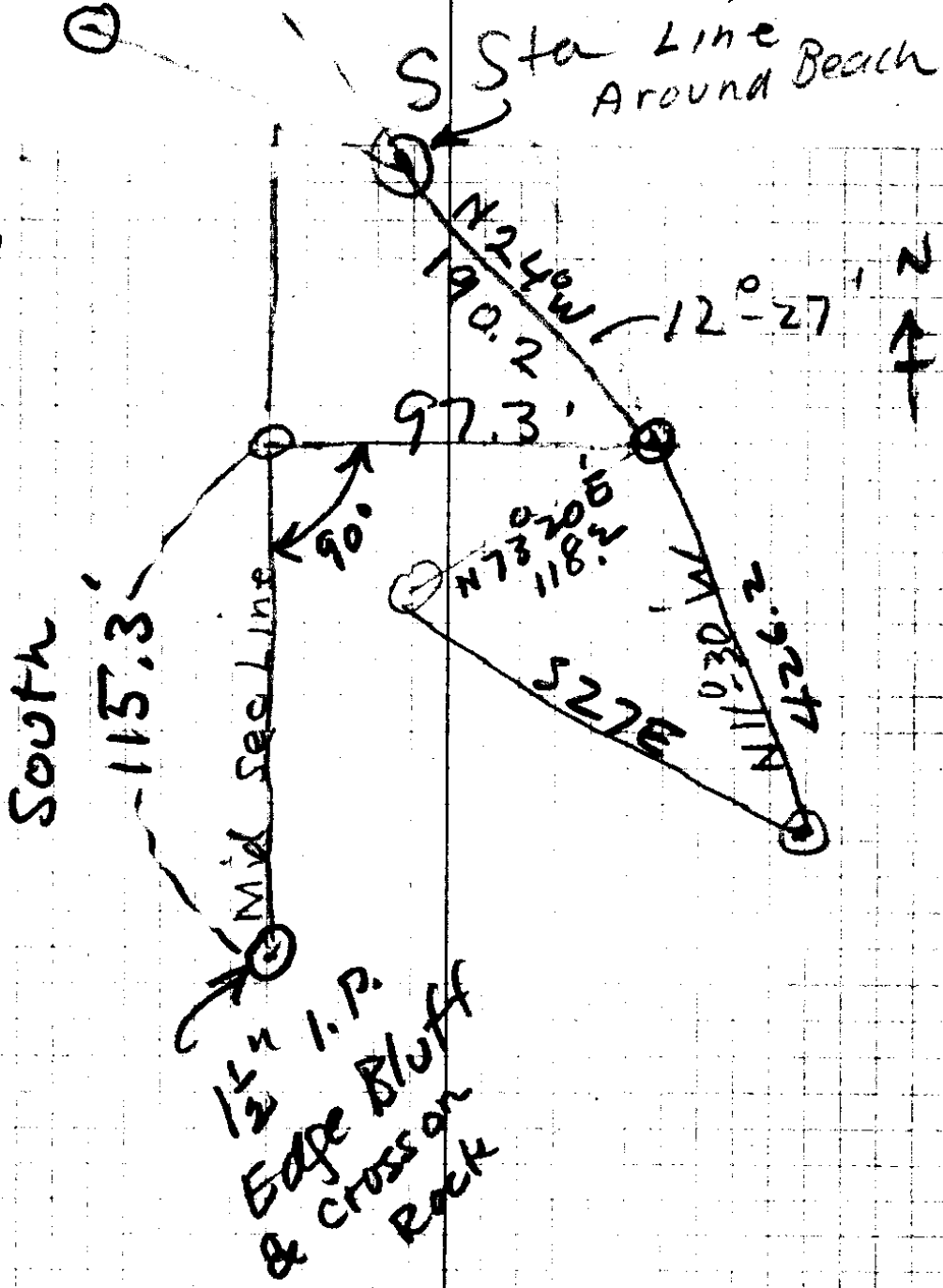
Point to North



23/28



165
200



Point to North

$$\begin{array}{r} N 11^{\circ} 30' W \\ 12^{\circ} 27' \\ \hline N 23^{\circ} 57' W \end{array}$$

23/78

Upper Switch back

Sta	+S	H1	-S	Elev
0+0				100.0
	13.0	113.0		
	T.P.		0.0	113.0
	7.0	120.0		
1+00			5.0	115.0
				97.0
			0.0	120.0
				95.0
2+00			6.3	113.7
				94.0
	T.P.		9.0	
	0.0	113.7	0	
2+50			13.0	100.7
				92.5
			8.5	105.2
	0.0	105.2		
			8.6	96.6
	0.0	96.6		
3+00			8.8	87.8
				91.0
3+50			10.0	86.6
				88.5

Used 3 70

F3.2

F2.0

Sun

00

3

85

C 18.0

C 24.5

C 19.7

C 8.2

F 3.2

F 2.0

Length Rd to Flat
at Bott 2112' ±

$$\begin{array}{r} 100 \\ 86.6 \\ \hline 13.4 \end{array}$$

$$\begin{array}{r} 350 \overline{) 13.40} \quad (370 \\ \underline{1350} \end{array}$$

0
1 +50

$$\begin{array}{r} 100 \\ 45 \\ \hline 95.5 \\ 1.5 \end{array}$$

$$\begin{array}{r} 100 \\ 6 \\ \hline 94 \\ 3 \frac{1}{2} \\ 6 \end{array}$$

2 +100

$$\begin{array}{r} 54 \\ 1.5 \end{array}$$

$$\begin{array}{r} 145 \\ 75 \\ \hline 70 \end{array}$$

2 +50

$$\begin{array}{r} 92.5 \\ 11.5 \\ \hline 91.0 \end{array}$$

$$\begin{array}{r} 145 \\ 9 \\ \hline 91 \end{array}$$

$$\begin{array}{r} 100.7 \\ 92.5 \\ \hline 918.2 \\ 874 \\ \hline 3.2 \end{array}$$

$$\begin{array}{r} 3.8 \\ 3 \\ \hline 10.5 \\ 100 \\ 10.5 \\ \hline 89.5 \\ 115 \\ 97 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 89.5 \\ 86.6 \\ \hline 1.9 \end{array}$$

$$\begin{array}{r} 120 \\ 91.5 \\ \hline 24.5 \\ 113.7 \\ 94 \\ \hline 19.7 \end{array}$$

23/10

East Line

	DIST	Vert L	Mag Brq
--	------	--------	---------

F

Tot 240.9 (17' Flat)
 CC=223.9

241° ON 21°40' N49 7/8 E = 223.9
 E Δ = 49°08' R _{cos .929}

59.3 23°06' = 54.5'
_{.920}

D.

59.2 16°45' = 56.6'
_{.957}

C = Iron pipe

50.4 Flat North

B

71.5 8°55' North = 70.6'
_{.988}

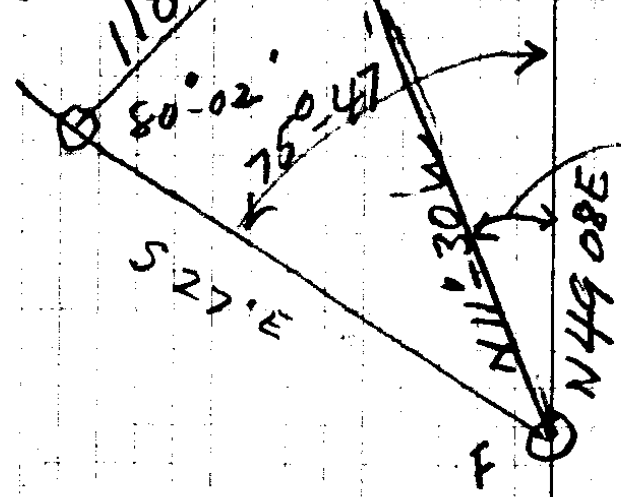
"
 A = 940' N of S & cor Sec 6

70.6
 50.4

 121.0

Wed AM. - Nov 10
 1962 x 12:27'
 84°-50'

90.60
11-30
68-30
11-30

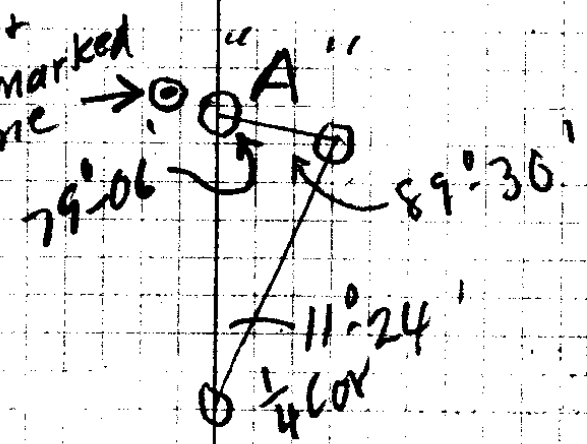


60° 38'
 vert L = 17° 35'

26° N on midsec line
 = vert L to water.

5" Alder → N 78° W 29'
 C = 1 1/2" x 36" I.P.

snag 12' N +
 1.0. w marked
 midsec line →



940
70.6
504
1061

23/2

Line from N End
w. Bay to recon

4 Cor Stake N5°-03'E
 N6°E 259.9 on 15°-0' corr = 9639
 corr = 251.04
 13+25? Δ = 27°-30'R Power Pole

MC. { N21½W N22°-27'W
 N25°W + 39.0 Flat }
 N25°W on [9°-20' 300 =] 335.0
 corr = 296.0

98865 Δ = 1°-49' R
 3330 129W

N23¼W, 226.3 N24°-16'W
 7602 Δ = 13°-51'L
 26+44.1 N9½°W 160.2 N10°-25'W

6+00 Δ = 30°-25'L
 28+04.3 86.9 N21°E = ½ Bdwy N20°E
600 513.1' = 26+91.2

0+0 5th + Bdwy
 = 34+04.3

Sun

46
46

44
82.2
1.2
226.2

966
260

5796
1932
251.1

orig BT.
40"

12 + 86
39

13 25

6 00

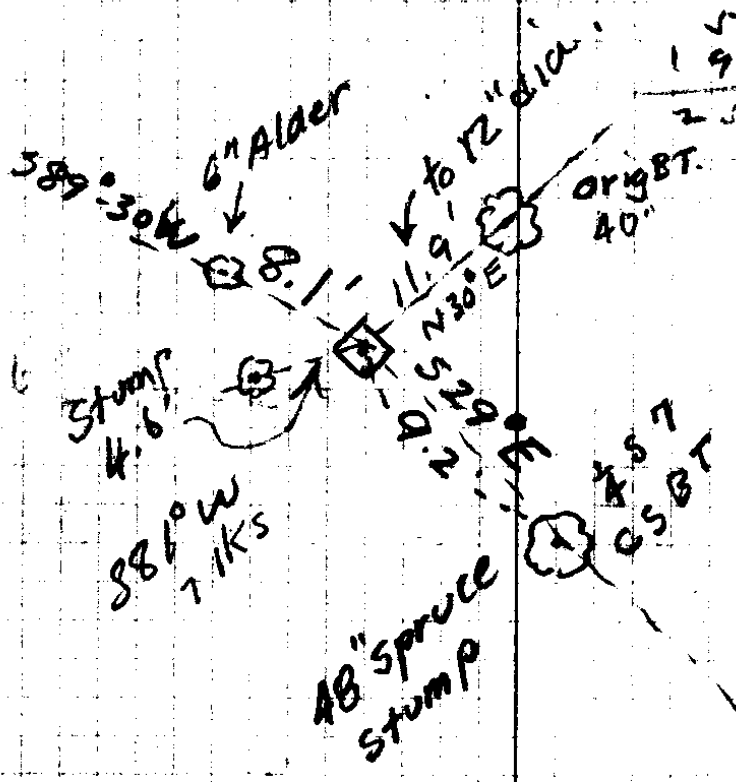
5 13.1

86.9

7 + 602

226.3

9 + 865



stump
4.6

88°W
1 KS

48" spruce
stump

487
CS BT

leave → 9 + 865
red survey

26 + 44.1
160.2

~~839~~

28 + 043

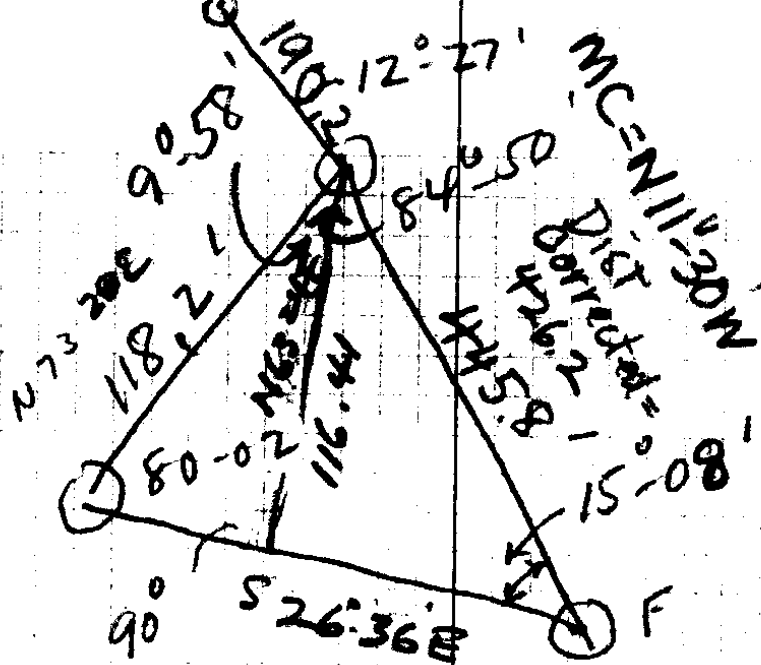
23/28

445.8	3
<u>956</u>	<u>2</u>
26748	(6)
22290	
40122	
<u>426.1848</u>	1

90	73-30
27	63
<u>63</u>	<u>10</u>
84-50	
11-30	
<u>73-20</u>	

11-30	90 60
<u>15 08</u>	26-36
26 36	<u>63-24</u>

73-20
<u>63 24</u>
9-56



75 47
 60 38

 15-09
 84 50
 80 02
 15 09

 180-01

180 60 CH
 80-02 958 = .9849 3

 99-58 19698
 90 60 78792
 80-02 9849

 9-58 116.41518
 80-02
 90

2611 | 116.41 (445.8

 10444

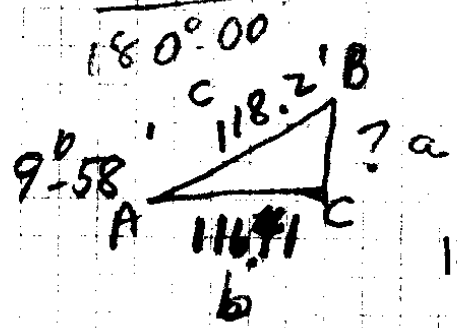
 11970
 10444

 15260
 13055

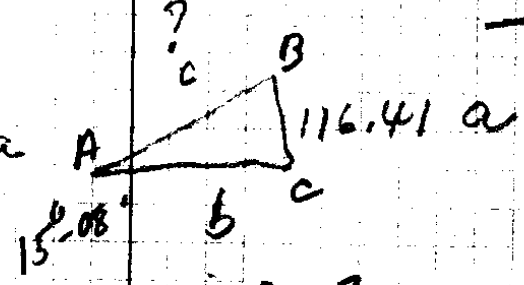
 22050
 20888

 1162
 4458

 2956



$\sin A = \frac{a}{c}$
 $\cos A = \frac{b}{a}$
 $b = c \cos A \times c$



$\sin A = \frac{a}{c}$
 $c = \frac{a}{\sin A}$
 $\frac{116.41}{.2611}$

23/18

89-30
2

98196 = $\cos 10^{\circ} 54'$
190.7

179 00

687372

8837640

98196

11-24

59-30

187259772

100-54

$\cos 13^{\circ}$

97437

964.7

682059

389748

584622

876933

939974739

180 60

100-54

79-06

79.06
36.06

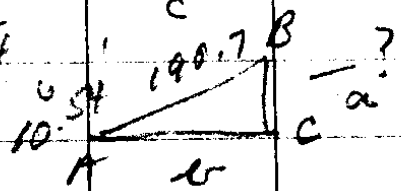
190.7

10.54'

187.26

928.6

11.24'



$$\sin A = \frac{a}{c}$$

$$a = \sin A \times c$$

.1891
190.7

13237

17019

1891

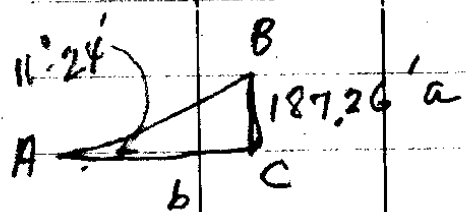
36.06137

928.6

36.1

964.7

$$\cos A = \frac{b}{c}$$



$$\tan A = \frac{a}{b}$$

$$b = \frac{a}{\tan A} = \frac{187.260}{.20164} = 928.6$$

181476

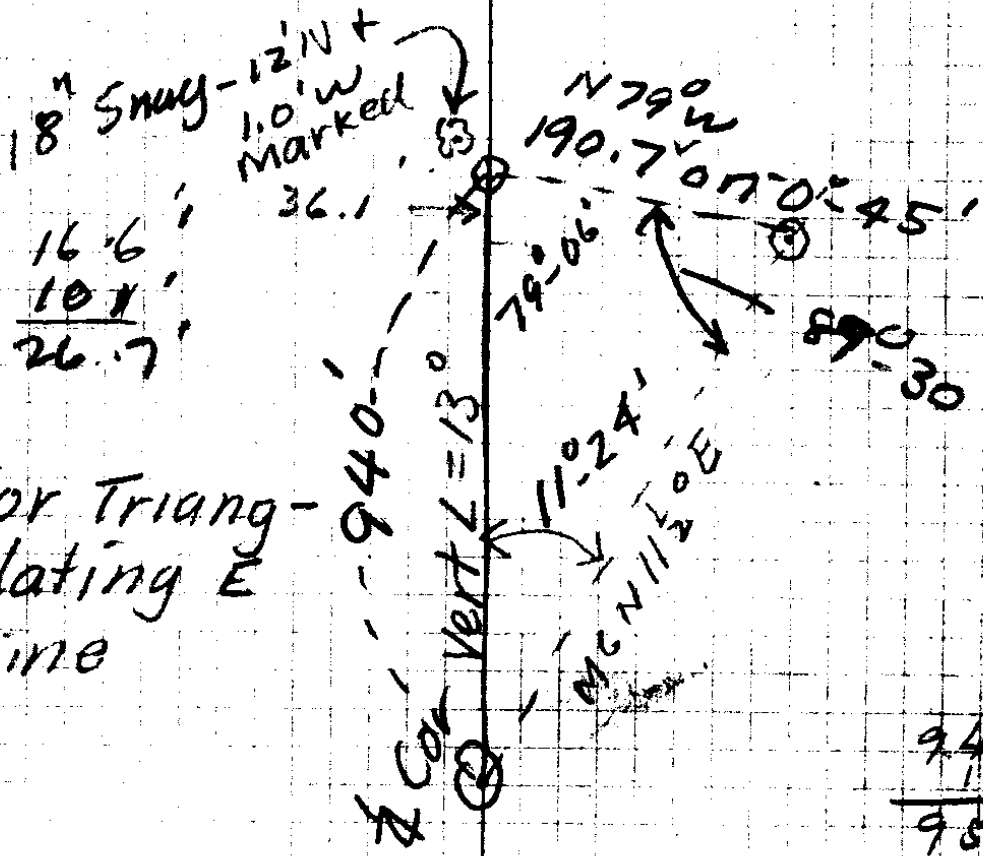
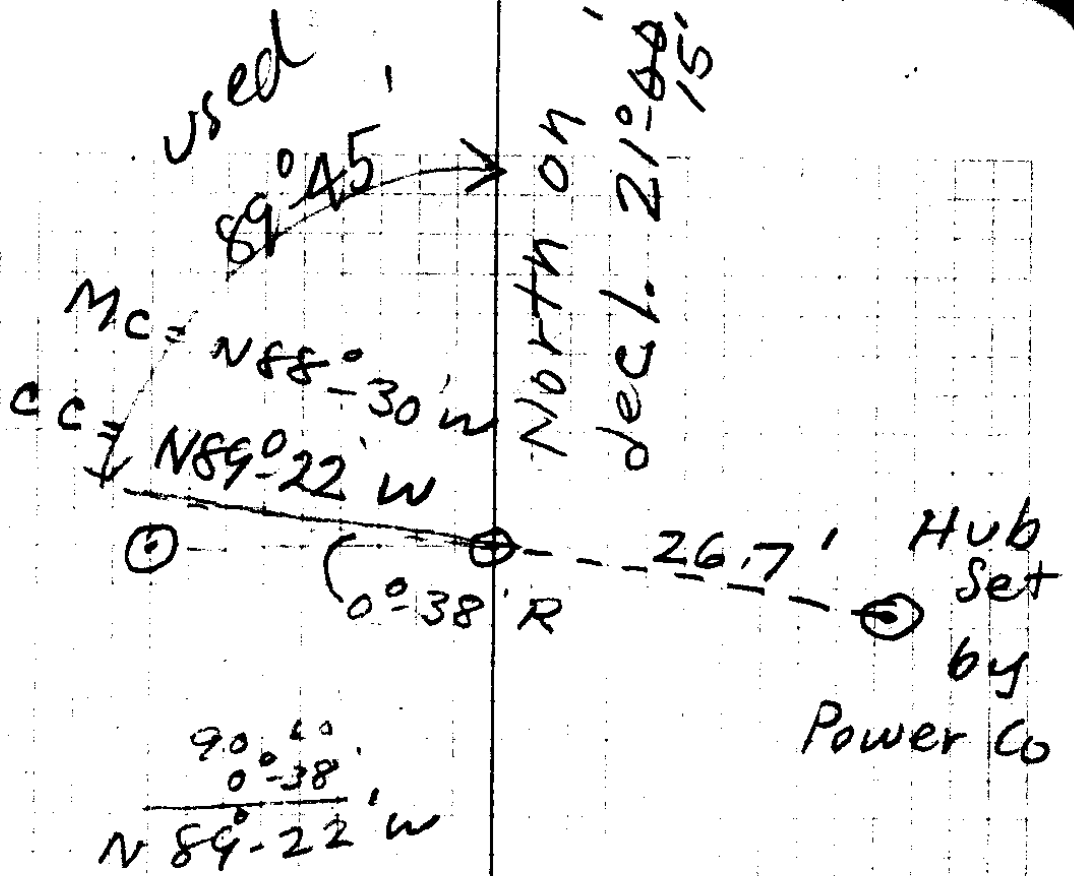
59840

40328

175170

161312

13808



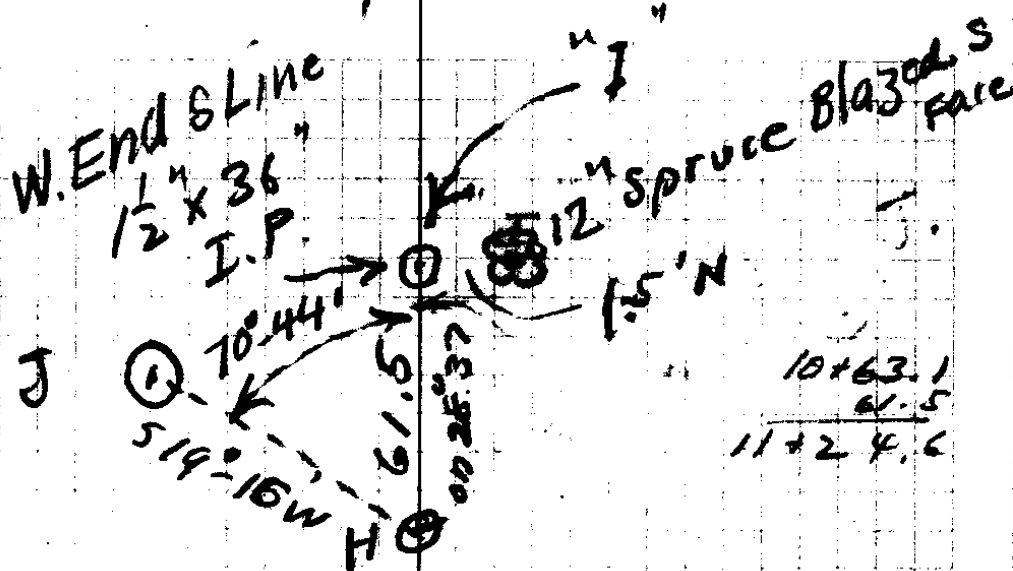
For Triangulating E Line

23/78

S. Line -

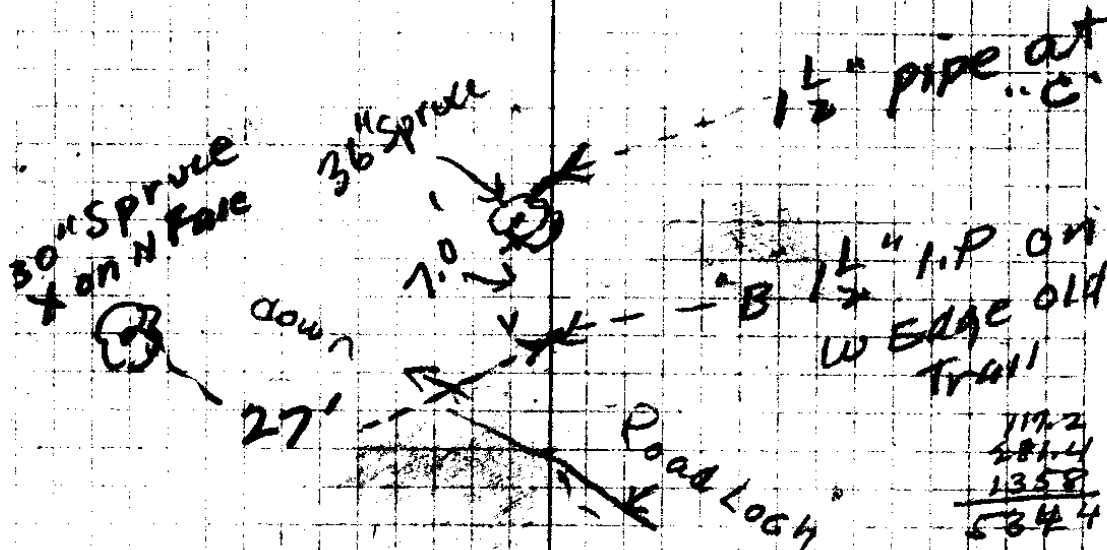
Sta	Dist	vert L	Mag. Brg
" " west " " End. I - S. Line	61.5	28°-37'	54.0
H = 10 + 63.1	136.5	24°-45'	123.9
G	76.7	11°-15'	75.2
F	107.6	Flat	107.6
E	51.4	18°-35'	48.7
D	165.3'	25°-33' W.	149.1
C	24.2	Flat	24.2
B on old Trail	(534.4' W. of $\frac{1}{2}$ Cor 145.2 + 20°-47'		Summit 135.8
P.O.I. A - Top Stump	300. + 20°-16'	West	= 281.4
O to $\frac{1}{4}$ Cor.	131.0'	26°-28' West 895	117.2'

MON NOV 9 9th TUES NOV 10



10 + 63.1
 21.5
 11 + 24.6

100' in of water



117.2
 281.4
 135.8
 534.4

254.2 on 26° 20'

238.9

23/18

117.2
 356.1

S	$\Delta 84^{\circ}-18'R$	640.8	$345^{\circ}-15'E$	349.1	CC
R	$\Delta 15^{\circ}-34'R$	270.5	N80 ^L 2E	N81 ^L -08 ^L E	
Q	$\Delta 10^{\circ}-05'R$	212.7	N65 ⁰⁰ -34 ^L E	N65 ⁰⁰ -34 ^L E	
P	$\Delta 2^{\circ}-47'R$	128.8	N53 ⁰⁰ E	N55 ⁰⁰ -29 ^L E	
D	Cornwall Point $\Delta 23^{\circ}-23'R$	342.3	N62 ⁰⁰ E	N52 ⁰⁰ -42 ^L E	
N	$\Delta 18^{\circ}-0'R$	573.8	N28 ⁰⁰ -30 ^L E	N29 ⁰⁰ -20 ^L E	
M	$\Delta 40^{\circ}-18'R$	427.2	N10 ⁰⁰ -45 ^L E	N11 ⁰⁰ -20 ^L E	
L	$\Delta 27^{\circ}-14'L$	300	N28 ⁰⁰ -58 ^L W	N29 ⁰⁰ -30 ^L W	
K	$\Delta 42^{\circ}-28'R$	132.0	N2 ⁰⁰ -15 ^L W	N1 ⁰⁰ -40 ^L W	
J	Jon Beach $\Delta 116^{\circ}-36'R$	132.0	N44 ⁰⁰ -45 ^L W	N44 ⁰⁰ -08 ^L W	
H		132.6	S19 ⁰⁰ -15 ^L W	S19 ⁰⁰ -16 ^L W	

corr = 91.3 .689

File

OC = N 14 3/4 M Cove
 S 315-155 Hub

349.1 90 60
 70 44

19-16-78
 29-30

N 10-48 E

Line 90 60
 70-44

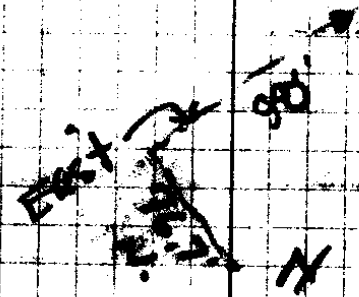
19-16
 116-36

135-52

180 60

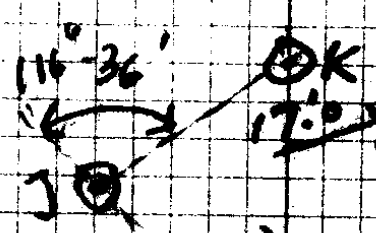
135-52

44-08



sect
 sect

Cross on
 Rock



West
 136.5
 132.5
 130.5
 128.5
 126.5
 124.5
 122.5
 120.5
 118.5
 116.5
 114.5
 112.5
 110.5
 108.5
 106.5
 104.5
 102.5
 100.5
 98.5
 96.5
 94.5
 92.5
 90.5
 88.5
 86.5
 84.5
 82.5
 80.5
 78.5
 76.5
 74.5
 72.5
 70.5
 68.5
 66.5
 64.5
 62.5
 60.5
 58.5
 56.5
 54.5
 52.5
 50.5
 48.5
 46.5
 44.5
 42.5
 40.5
 38.5
 36.5
 34.5
 32.5
 30.5
 28.5
 26.5
 24.5
 22.5
 20.5
 18.5
 16.5
 14.5
 12.5
 10.5
 8.5
 6.5
 4.5
 2.5
 0.5

1+00	Grade		
+25	C 0.18 =	C 2 $\frac{1}{4}$ '	
+50	F 0.3 =	F 3 $\frac{5}{8}$ "	
+75	C 0.05 =	C 5 $\frac{1}{8}$ " $\frac{1}{4}$ "	
2+00	C 0.3 =	C 3 $\frac{5}{8}$ "	

93/78

P 58 - 1931

EI. 16.043

90 60

20-44

19-16

116-36

135-52

180 60

N 44-68 W

42-28

N 1-40 W

29-30

31-10

132.6

1689

11934

10608

7956

91.3614

929

241

929

3716

1858

223.889

100

705

295

116-36

19-16

135-52

180 60

135-52

N 44-68 W

42-28

N 1-40 W

27-14

N 28-58 W

40-78

28-58

N 11-20 E

10-41

35

.9999

190.7

69993

89991

9999

190.68093

169-40

84-52

169-40

23/11

17 + 76
56

18 - 32
52

S 19 - 16 W

116 - 36

135 - 52
154 60

135 52

44 - 68
42 - 28

2 - 48
27 14

30 - 02

40 - 18

30 - 02

10 - 16

44 68

42 - 28

1 - 40
27 - 14

28 - 54

N 11° - 20' E

18°
N 29° - 20' E

23 22

52 - 42

52 47

15 - 29

255
87.6

167.4 from
S West to
E Line

116 - 36

19 - 15

135 - 51
180 65

135 - 51

44 - 69
42 - 28

N 1 - 41 W

N 55 29 E

10 05
N 65 34

15 - 34

81 - 08

223.9

17

240.9

Andre Fouchy
Civil Engineer
U.S. Coast Guard
Government Island
Oakland, Calif

1527
147.6
5.1

23/74

John Ashburn

Debelvis

86.9
513.1
600.0

77
43
120

Cor 22°05'

66
8
528

9267
600
~~536.0200~~
528
28.
18

26°-28' 895 1310 117.2

20°-16' 938 300.0 281.4

20°47' 935 1452 - 135.7

895
131 (2)
895
2685
895
117.245

938
300
281.400

145.2
935
7260
4356
13068
135.7620
66
528

~~N 26° E~~

N 26° 46' E - 174.0

N 3° 04' W 280.0

cos 4504

.9986 .0535

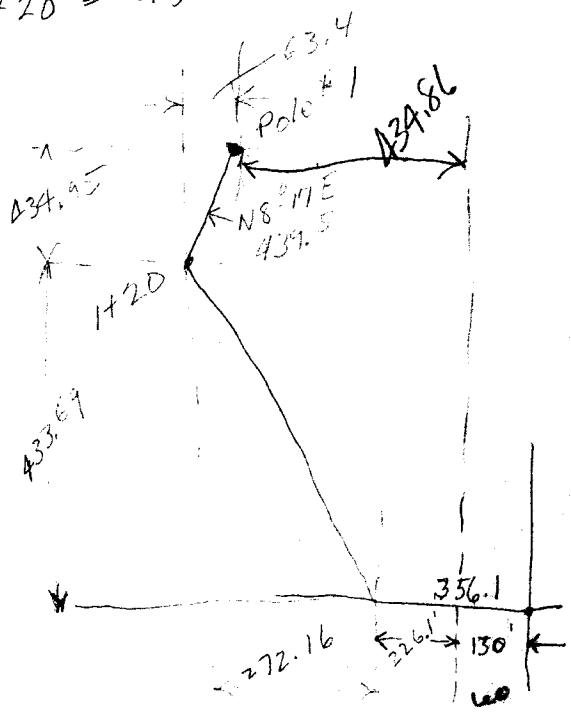
N	E	W
151.78	76.56	
3.57	1.80	
155.35	78.36	
279.60	14.98	1457
434.95	63.38	
	434.95	
	198850	
	173980	
	248700	
	217475	

N	E	W
155.35	7837	
279.60		
434.95		

N 8° 17' E
439.5

0 + 0 = 6 + 12.7

1 + 20 = 433.69 N W 272.16



434.95² = 189181.5025

63.38² = 4017.0244

19'3 198.52'69 (439.5)

4² 16

331

83 249

8298

869 7821

47752

87.8

3561

130

226.1

434.86) 868.640 (1997

43486
433780
391374
424060
391374
326860
304402

434.86² = 189103.2196

868.64² = 754535.4496

94'36"38.6692

90
63.38
N 26° 36' W

9² 94'36"38.6692 (971.45)

81

1336

187 1309

1841 2738

1841 1841

89366

19424 77696

1167092

19428

356.1

272.16

628.26

63.4

564.86

130

434.86 W

433.69

434.95

868.64 N

94'36"38.6692 (971.4)

81

1336

187 1309

1841 2738

1841 1841

89766

19424 77696



OFFICE OF
ASSOCIATE CIVIL ENGINEER
CONSTRUCTION AND REPAIR

TREASURY DEPARTMENT

UNITED STATES COAST GUARD

Room 219, Administration Building,
Government Island, Oakland, Calif.

February 11th, 1937.

Mr. Arthur Boyer,
Deputy County Surveyor,
Douglas County,
Roseburg, Oregon.

Dear Sir:

Your letter of 9th inst. relative to survey of Coast Guard reservation and road in Sections 6 and 7, Near Winchester Bay, Oregon, received.

The tracing of survey of the S.W. quarter of Section 6 was received when I was away from the office. In view of the necessity of having plat show the accurate location of the West Coast Power Co. right of way across said S.W. quarter of Section 6, no action could be taken to prepare the deed, for transferring the property to the Coast Guard.

The blue print of your later survey, showing the power line across the S.W. quarter of Section 6 does not tie with either the station site survey, station 1 plus 20, or initial starting point, or station 0 plus 0, of road survey to Winchester Bay. I am returning the tracing, and it is requested that you complete same by showing exactly where and how the 100 ft. strip of the power company is located; also indicate the relative position of Pole No. 1 of power line, to station 1 plus 20 of Coast Guard Station site survey, giving distance and bearing, also acreage in power line strip. According to my measurements this pole No. 1 is 438.3' from station 1 plus 20 but according to your revised plan showing power line, it appears to be only 426.15' from station 1 plus 20.

The above information is needed to prepare the deed, and it is essential to know just where the Coast Guard property is.

Please return the tracing which I am sending under separate cover, with above corrections, so that I can have several prints made of the official survey for recording, and I will return the tracing for your files.

I regret that the receipt of tracing of Coast Guard Survey, and of blue print of power line was not acknowledged before.

Please expedite the information and oblige.

I presume you received your check all right.

Yours truly,

Andre Fourchy
Andre Fourchy,
ASSOCIATE CIVIL ENGINEER.

AF:Jo. C. S. File No. 23/78

CS FILE FOLDER

CONTAINS

MORE

INFORMATION