

LEVELS

N.E. RICHARDSON

B.A. LANE

MAY 3 1930

18-1

165.67

BM1 MASON'S HALL

BM2 RESERVOIR

STA	+	+	-	ROD	EIV.
					747.30
	5.96	753.26			
		744.89	8.37		
	2.85	747.74			
		743.76	3.98		
	2.33	746.09			
		743.61	2.48		
	15.43	759.04			
		758.69	0.35		
	15.72	774.41			
		774.37	0.04		
	10.54	784.91			
		784.71	0.20		
	14.93	799.64			
		798.23	1.41		
	15.98	814.21			
		813.07	1.14		
	15.97	829.04			
		829.04	0.00		
	15.93	844.97			
		844.97	0.00		
	12.51	857.48			
		857.48	0.00		
	128.15		17.97		

CANYONVILLE

U.S.G.S. B.M. SW. COR MASONS HALL

747.30

767.00 MARKED ON B.M.

12/1

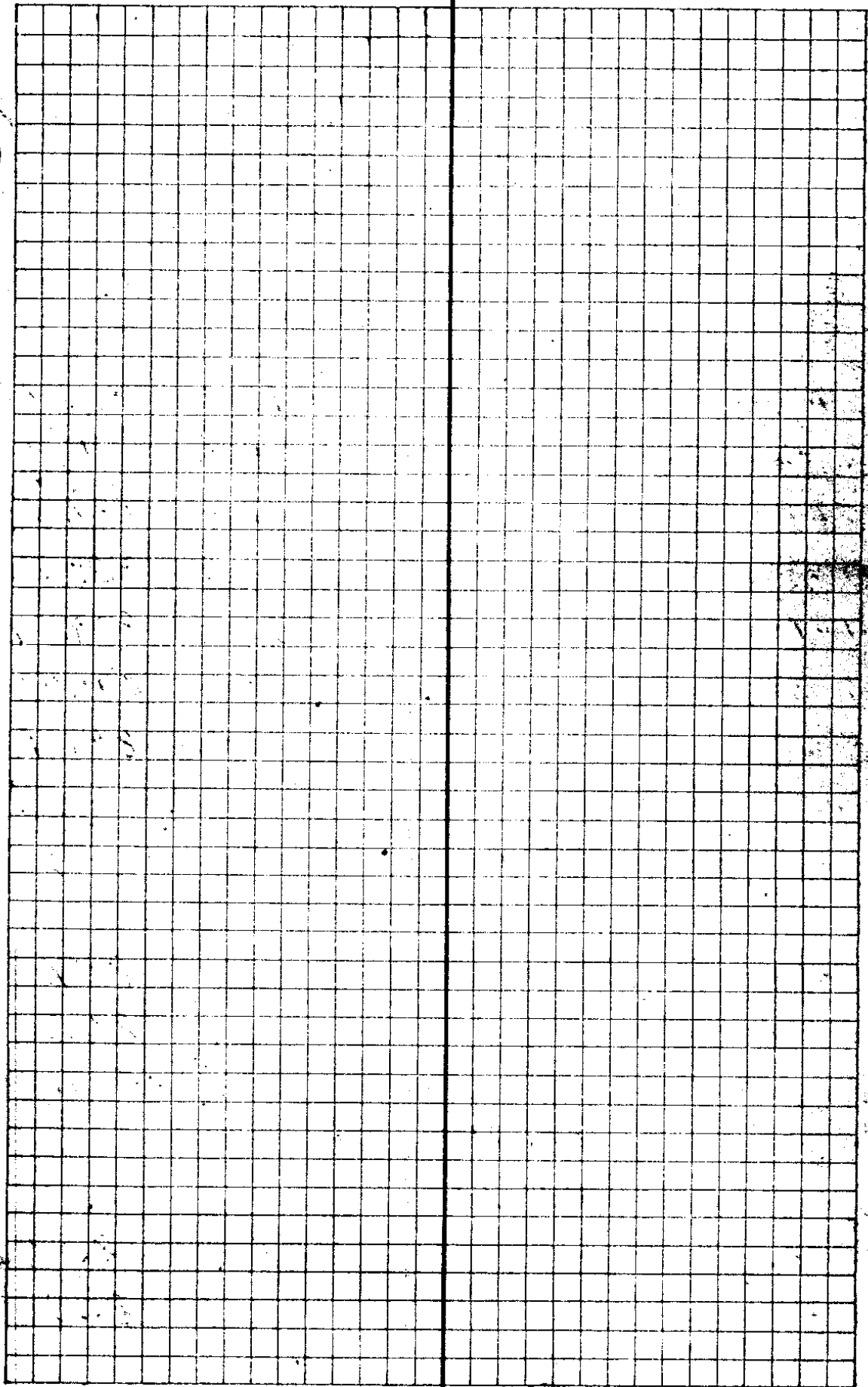
STA	+	⊖	-	ROD	ELV.
		857.48			
	13.11	870.59			
		870.59	0.00		
	14.54	885.13			
		884.42	0.71		
	13.01	897.43			
		896.66	0.77		
	16.46	913.12			
BM*1				0.15	912.97
0+00				12.69	900.43
0+50				14.40	898.72
		898.74	14.38		
	4.73	903.47			
1+00				12.00	891.47
1+50				13.60	889.87
2+00				21.40	882.07
2+12				26.40	877.07
2+50				9.20	894.27
3+00				3.20	900.27
3+17 1/2				2.90	900.57
3+50				3.60	899.87
4+00				13.40	890.07
4+25				16.45	887.02
	61.85		15.86		

B.M. #1 ON WHITE OAK .

30' TO RIGHT STA 0+50

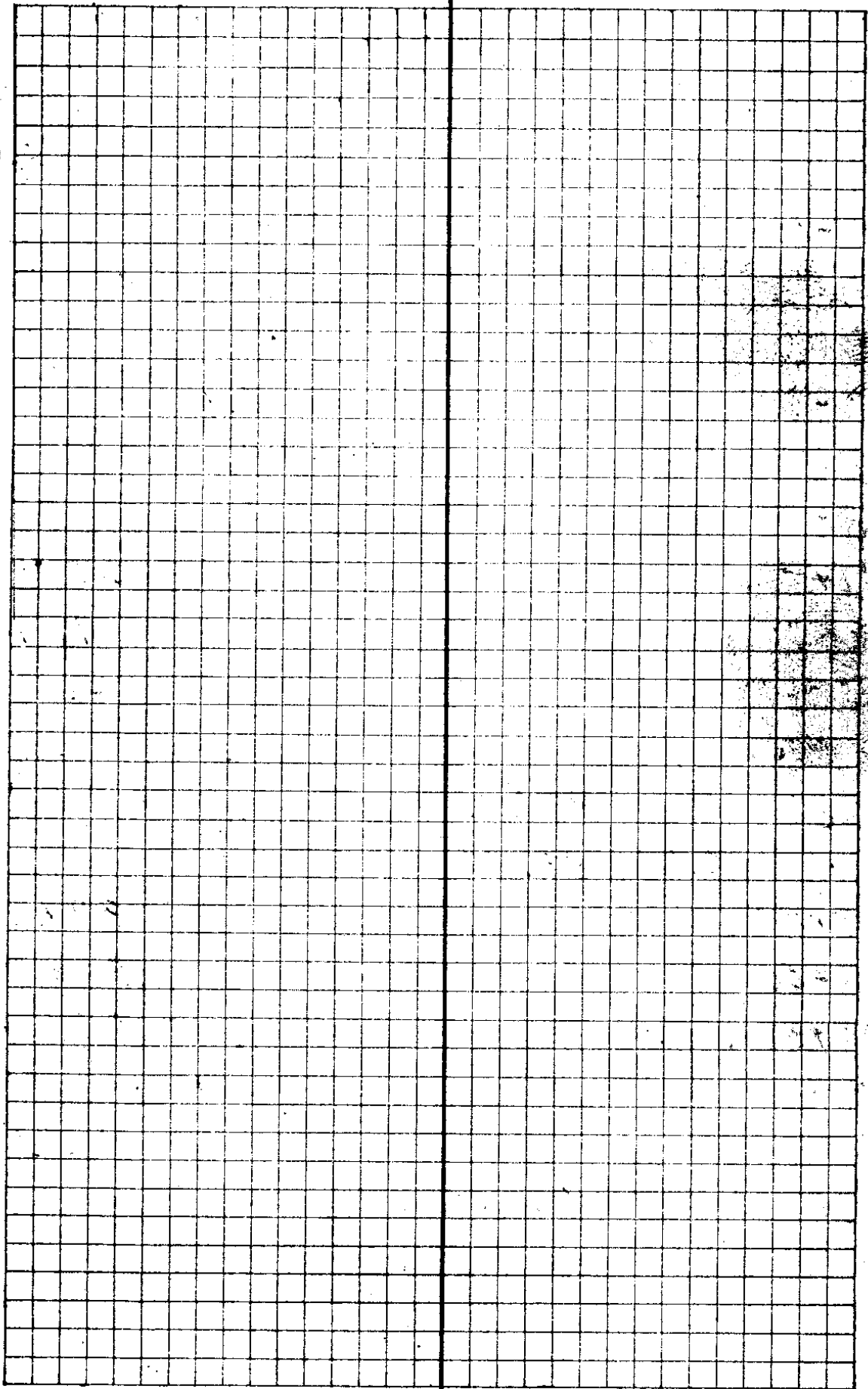
10/1

STA	+	π	-	ROD	EIV
		903.47			
4+50				14.30	889.17
•		889.20	14.27		
	5.56	894.76			
5+00				9.30	885.46
5+50				15.60	879.16
6+00				21.00	873.76
6+50				18.30	876.46
7+00				16.50	878.26
7+50				14.40	880.36
8+00				22.50	872.26
8+50				23.90	870.86
9+00				9.90	884.86
9+50				0.30	894.46
•		894.49	0.27		
	6.39	900.88			
10+00				3.10	897.78
10+50				5.10	895.78
11+00				14.80	886.08
•		886.06	14.82		
	2.00	888.06			
11+10.3				4.50	883.56
11+50				14.55	873.51
	13.95		29.36		



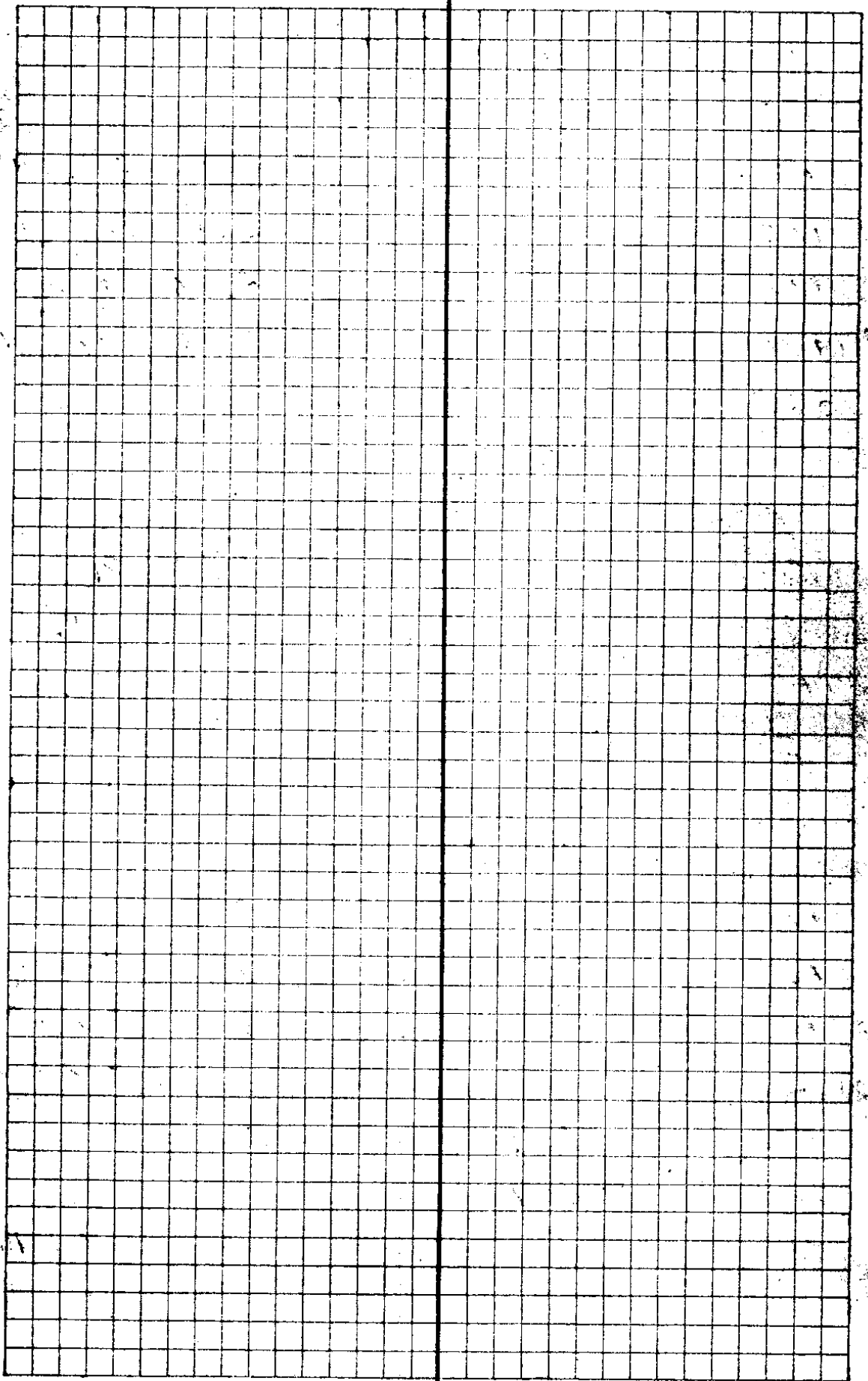
18/1

STA	+	π	-	ROD	EIV
		888.06			
⊙		873.51	14.55		
	0.98	874.49			
12+00				?	?
⊙		861.70	12.79		848.91
	0.29	861.99			
12+50				10.00	851.99
12+92 <sup>5</sup>				14.20	847.79
13+50				17.10	844.89
14+00				23.40	838.59
14+15				27.20	834.79
14+50				20.50	841.49
15+00				17.50	844.49
⊙		847.49	14.50		
	3.57	851.06			
15+50				4.90	846.16
16+00				3.70	847.36
16+50				5.70	845.36
17+00				9.10	841.96
⊙		841.91	9.15		
	8.88	850.79			
17+50				12.50	838.29
18+00				13.10	837.69
	13.72		50.99		



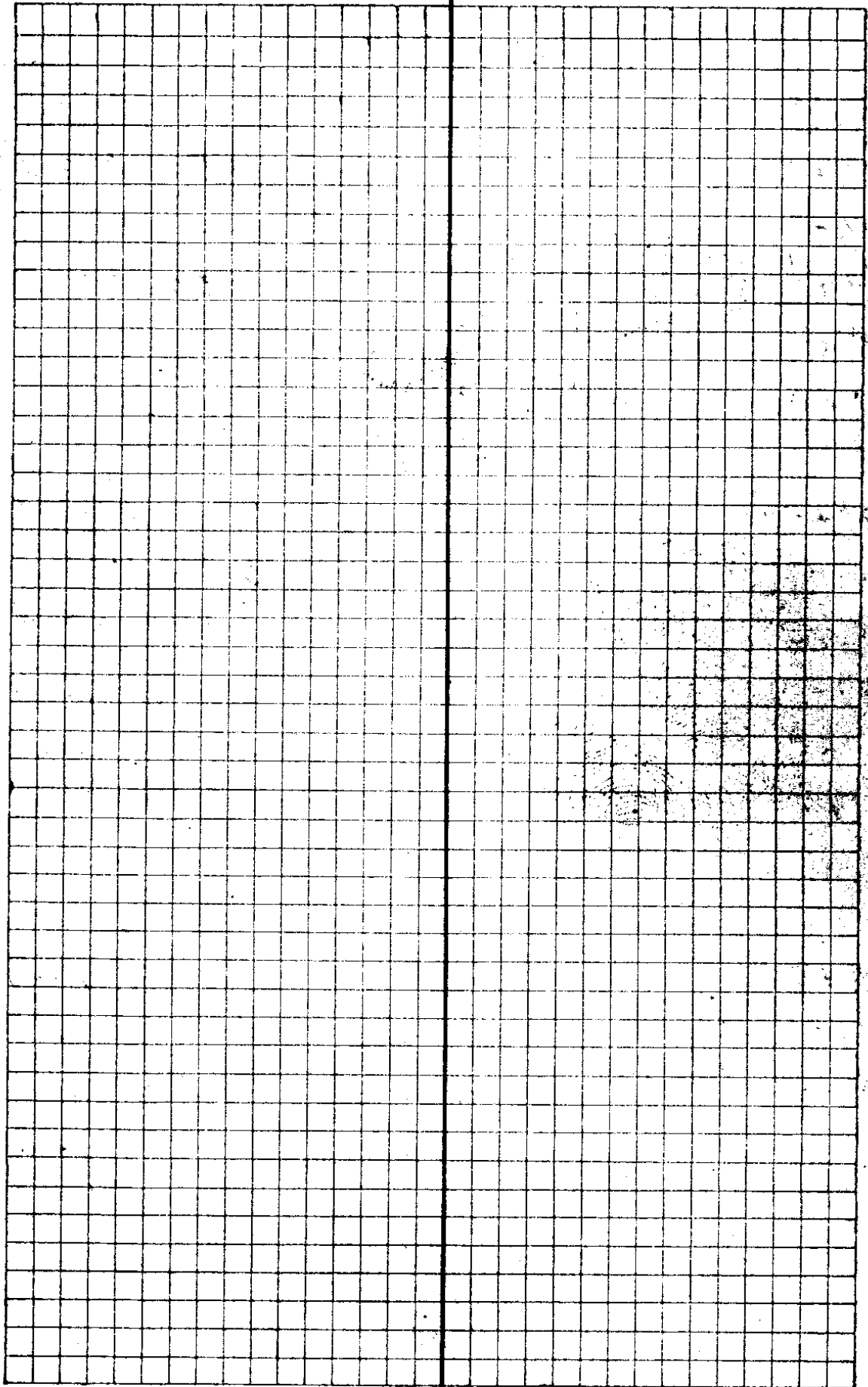
1/31

STA	+	π	-	ROD	ELV.
		850.79			
18+46 <sup>4</sup>				12.80	837.99 ●
19+00				9.80	840.99
19+50				5.20	845.59
20+00				3.70	847.09
20+50				3.90	846.89
○		846.91	3.88		
	8.80	855.71			
21+00				8.80	846.91
21+50				12.80	842.91
22+00				15.50	840.21 ●
22+50				20.80	834.91
○		840.56	15.15		
	2.32	842.88			
22+73 <sup>8</sup>				8.65	834.23
23+00				9.15	833.73
23+56 <sup>3</sup>				9.55	833.33
24+00				12.40	830.48
24+50				17.60	825.28
○		826.39	16.49		●
	0.82	827.21			
25+00				5.90	821.31
	11.94		35.52		



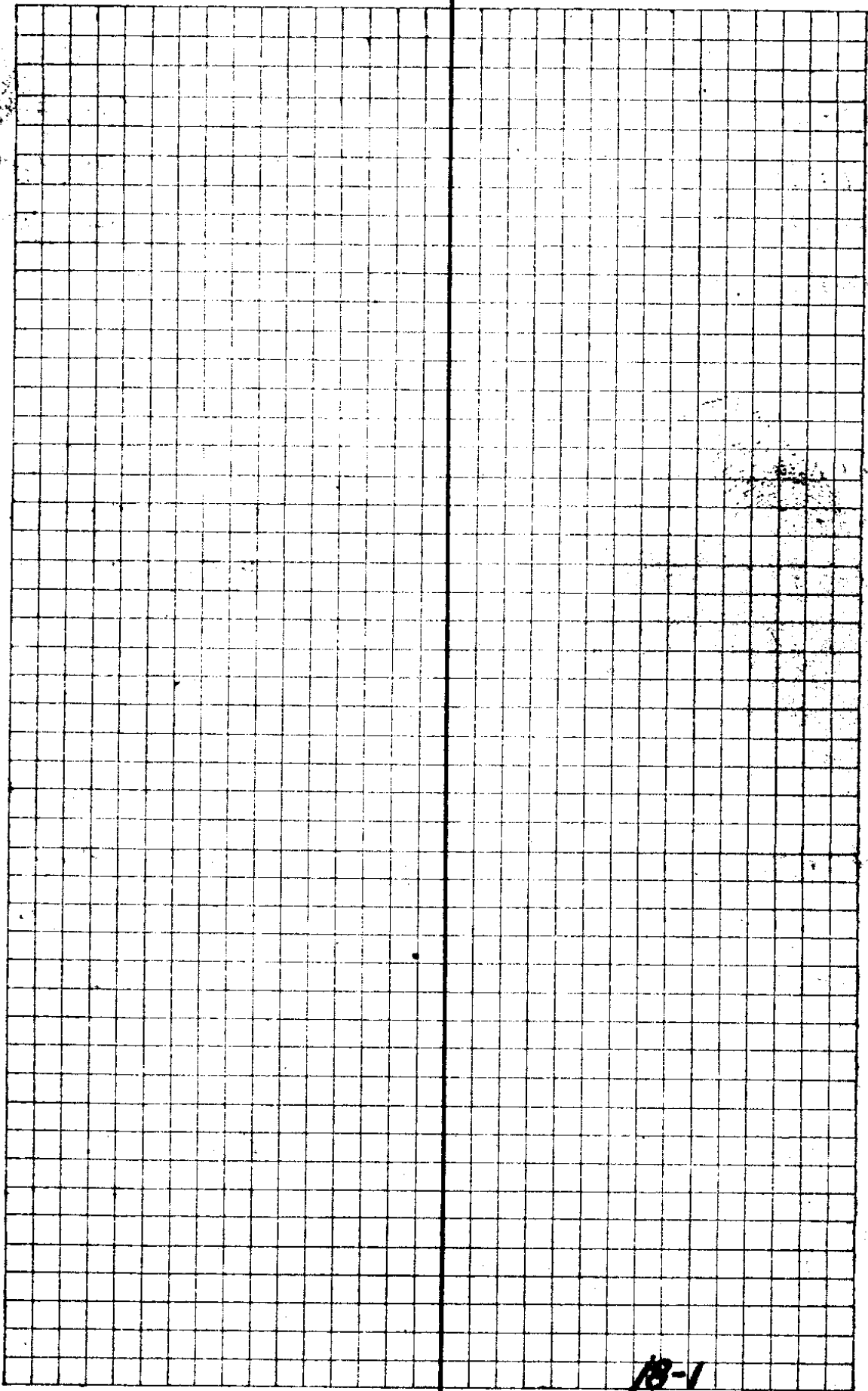
15/1

STA	f.	$\pi$	-	ROD	ELY.
		827.21			
25+50				9.75	817.46
26+00				12.40	814.81
26+50				15.20	812.01
27+00				14.80	812.40
o		812.46	14.75		
	0.95	813.41			
27+50				3.20	810.21
28+00				5.20	808.21
28+50				8.40	805.01
29+00				11.10	802.31
29+50				7.35	806.06
30+00				4.30	809.11
o		809.13	4.28		
	5.50	814.63			
30+50				4.50	810.13
31+00				4.50	810.13
31+50				9.10	805.53
o		804.13	10.50		
	3.23	807.36			
32+00 ✓				5.20	802.16
32+50				5.50	801.86
	9.68		29.53		



18/1

STA	+	π	-	ROD	ELV
		807.36			
33+00				5.10	802.26
33+50				4.50	802.86
34+00				3.80	803.56
34+50				3.20	804.16
⊙		804.18	3.18		
	6.20	810.38			
35+00				5.30	805.08
35+50				4.50	805.88
36+00				3.50	806.88
36+50				2.70	807.68
37+00				2.50	807.88
⊙		808.02	2.36		
	4.87	812.89			
37+50				3.90	808.99
38+00				4.90	807.99
38+50				5.20	807.69
39+00				5.60	807.29
39+50				5.00	807.89
40+00				3.60	809.29
40+50				2.20	810.69
⊙		810.65	2.24		
	7.88	818.53			
	18.95		7.78		



18-1

STA	+	π	-	ROD	BLV
		818.53			
41+00				7.60	810.93
41+50				6.10	812.43
42+00				4.00	814.53
⊙		817.28	1.25		
	6.27	823.55			
42+43 <del>8</del>				6.55	817.00
42+97 <del>5</del>				4.30	819.25
43+50				4.20	819.35
44+00				4.50	819.05
⊙		819.76	3.79		
	5.50	825.26			
44+50				5.80	819.46
45+00				5.20	820.06
45+50				3.90	821.36
45+74 <del>6</del>				3.30	821.96
46+00				1.30	823.96
⊙		825.10	0.16		
	7.68	832.78			
46+50				6.70	826.08
47+00				4.50	828.28
47+50				3.70	829.08
48+00				3.60	829.18
	19.45		5.20		

45+746 ON GROUND

18-1

STA	+	π	-	ROD	ELV.
		832.78			
		(OK) HERE			
⊙		831.85	0.93		
	7.28	839.13			
48+49 <del>9</del>				7.70	831.43
49+00				5.50	833.63
49+50				1.90	837.23
⊙		838.66	0.47		
	7.88	846.54			
50+00				5.60	840.94
50+50				1.80	844.74
⊙		846.09	0.45		
	9.29	855.38			
51+00				7.30	848.08
51+50				3.40	851.98
52+00				2.50	852.88
52+50				4.60	850.78
52+70				12.60	842.78
53+00				3.90	851.48
53+11 <sup>9</sup>				4.20	851.18
53+30				18.70	836.68
53+50				6.50	848.88
54+00				8.90	846.48
⊙		846.50	8.88		
	2.36	848.86			

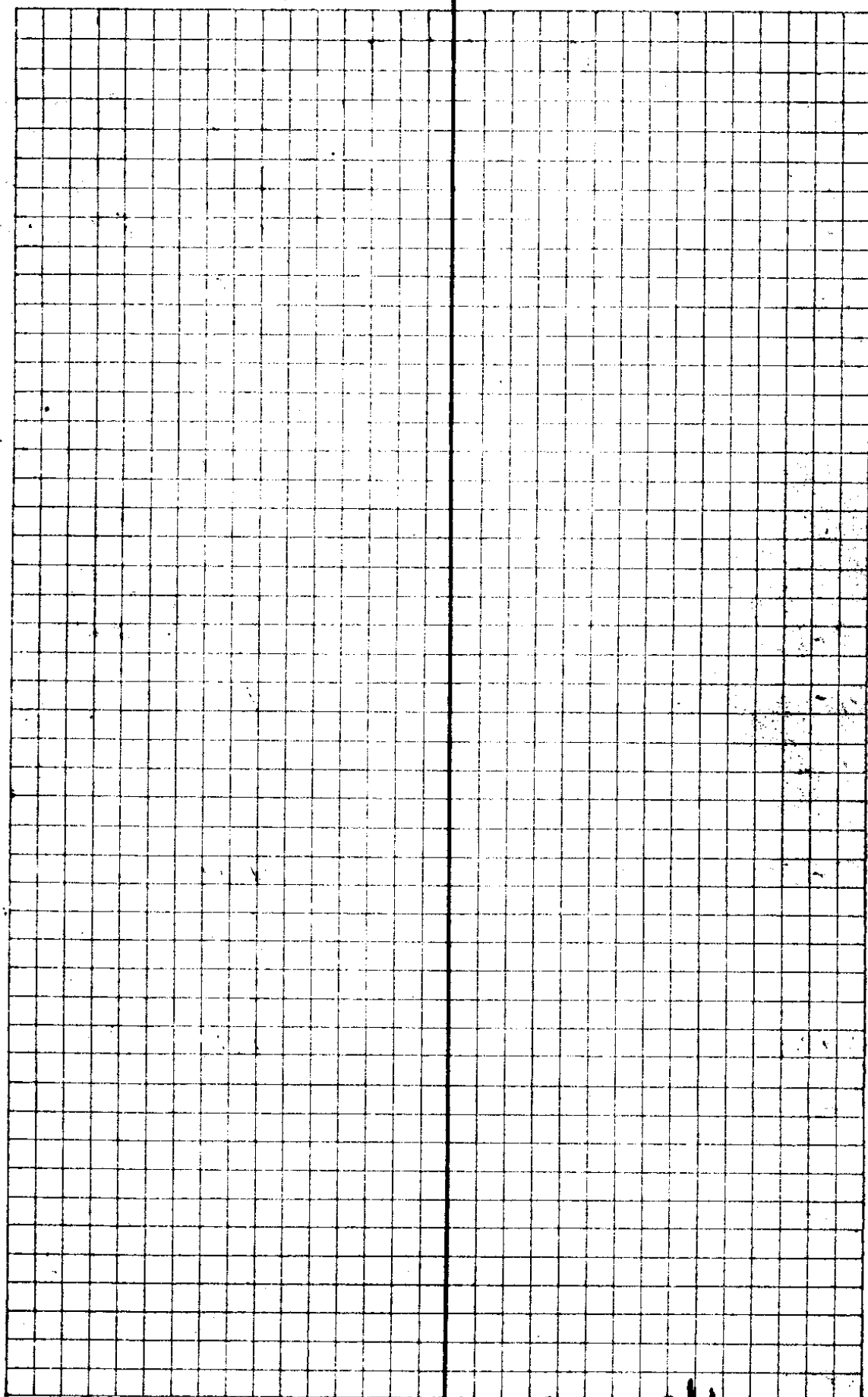
T.P. ON Cedar 2" left of Sta 48+00

53+30 DEEP DRAW

18-1

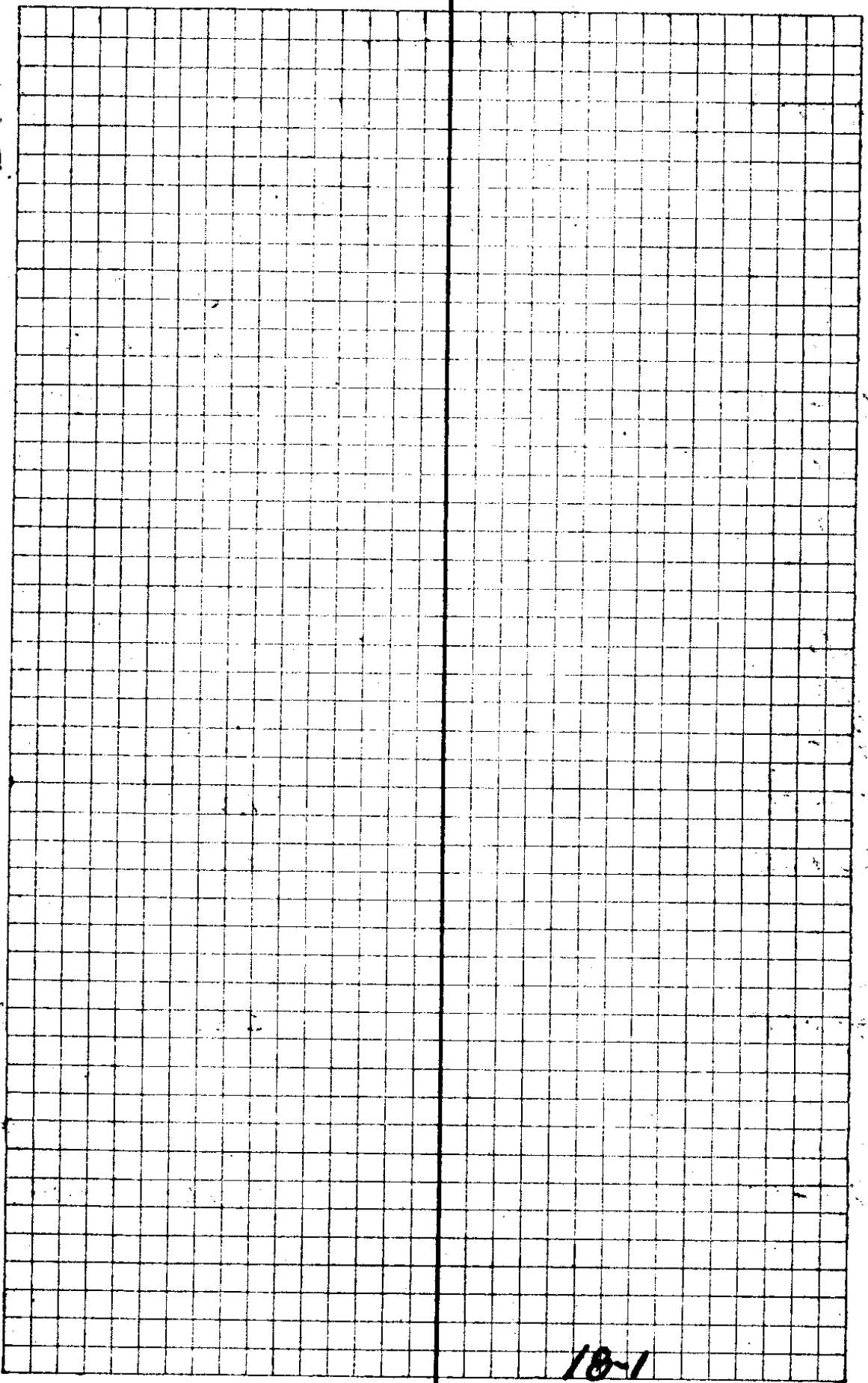
STA	+	∩	-	ROD	ELV
		848.86			
54+50				4.90	843.96
55+00				5.50	843.36 ●
55+51.9				3.20	845.66
56+00				1.90	846.96
○		847.17	1.69		
	7.32	854.49			
56+50				5.70	848.79
57+00				5.30	849.19
57+50				6.60	847.89
58+00				7.50	846.99
58+50				4.90	849.59 ●
○		854.24	0.25		
	9.40	863.64			
59+00				4.20	859.44
59+50				2.70	860.94
59+60				3.00	860.64
59+80				16.60	847.04
○		851.43	12.21		
	4.94	856.37			
60+00				9.30	847.07 ●
60+50				6.90	849.47
61+00				7.10	849.27

122  
46



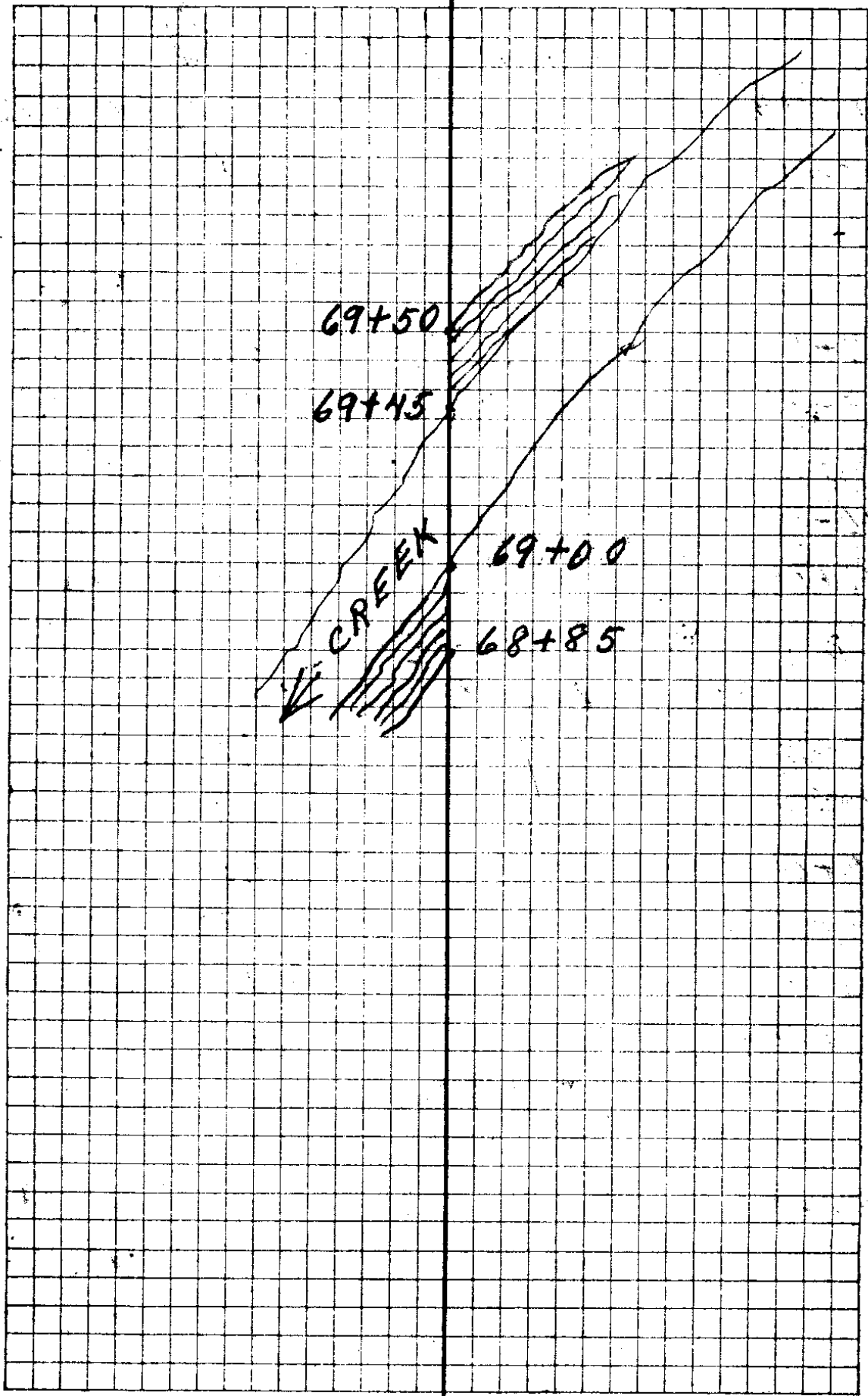
G. S. B. No. 18/1

STB	+	π	-	ROD	ELV.
		856.37			
61+45 <del>5</del>				3.70	852.67
⊙		852.71	3.66		
	6.79	859.50			
61+98 <del>5</del>				5.50	854.00
62+50				4.40	855.10
63+00				3.80	855.70
63+33 <del>3</del>				2.70	856.80
⊙		856.75	2.75		
	8.22	864.97			
63+50				8.00	856.97
64+00 <del>5</del>				7.20	857.77
64+50				5.00	859.97
65+00				4.00	860.97
65+50				2.90	862.07
⊙		862.06	2.91		
	8.08	870.14			
66+00				6.40	863.74
66+50				5.10	865.04
66+93 <del>5</del>				4.30	865.84
67+50				2.50	867.64
⊙		868.96	1.18		
	4.76	873.72			

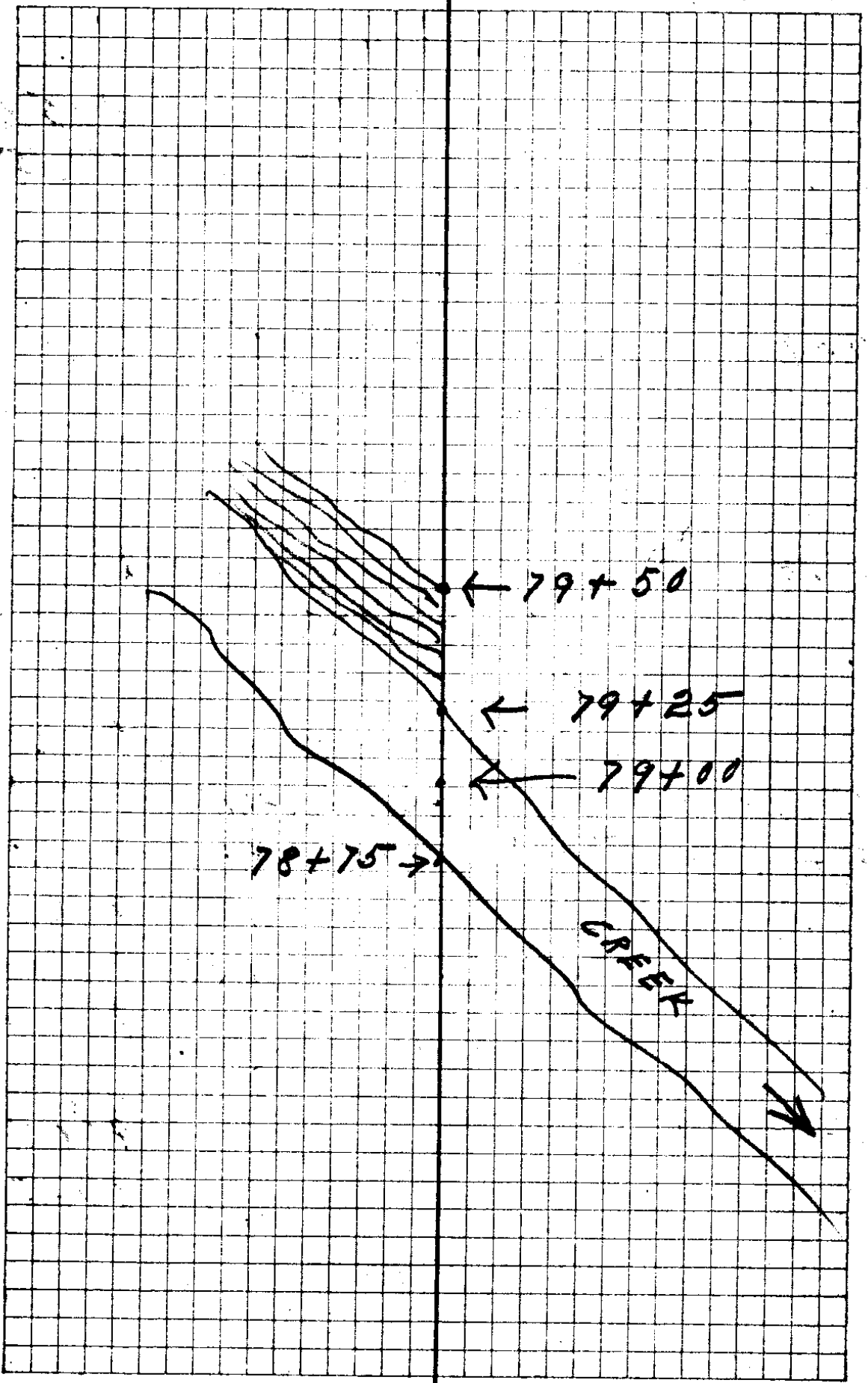


18-1

STA	+	π	-	ROD	ELV.
		873.72			
67+77 <del>8</del>				5.40	868.32
68+27 <del>8</del>				4.40	869.32
68+77 <del>9</del>				5.10	868.62
68+85				6.10	867.62
69+00				10.50	863.22
69+45				9.10	864.62
69+50				6.10	867.62
70+00				3.50	870.22
70+50				0.60	873.12
⊙		873.11	0.61		
	10.94	884.05			
71+00				9.50	874.55
71+50				7.70	876.35
72+00				4.30	879.75
72+50				4.70	879.35
73+00				4.10	879.95
<del>73+43</del>				<del>3.40</del>	
⊙		880.68	3.37		
	7.27	887.95			
73+50				4.50	883.45
74+00				2.00	885.95
74+50				3.00	884.95

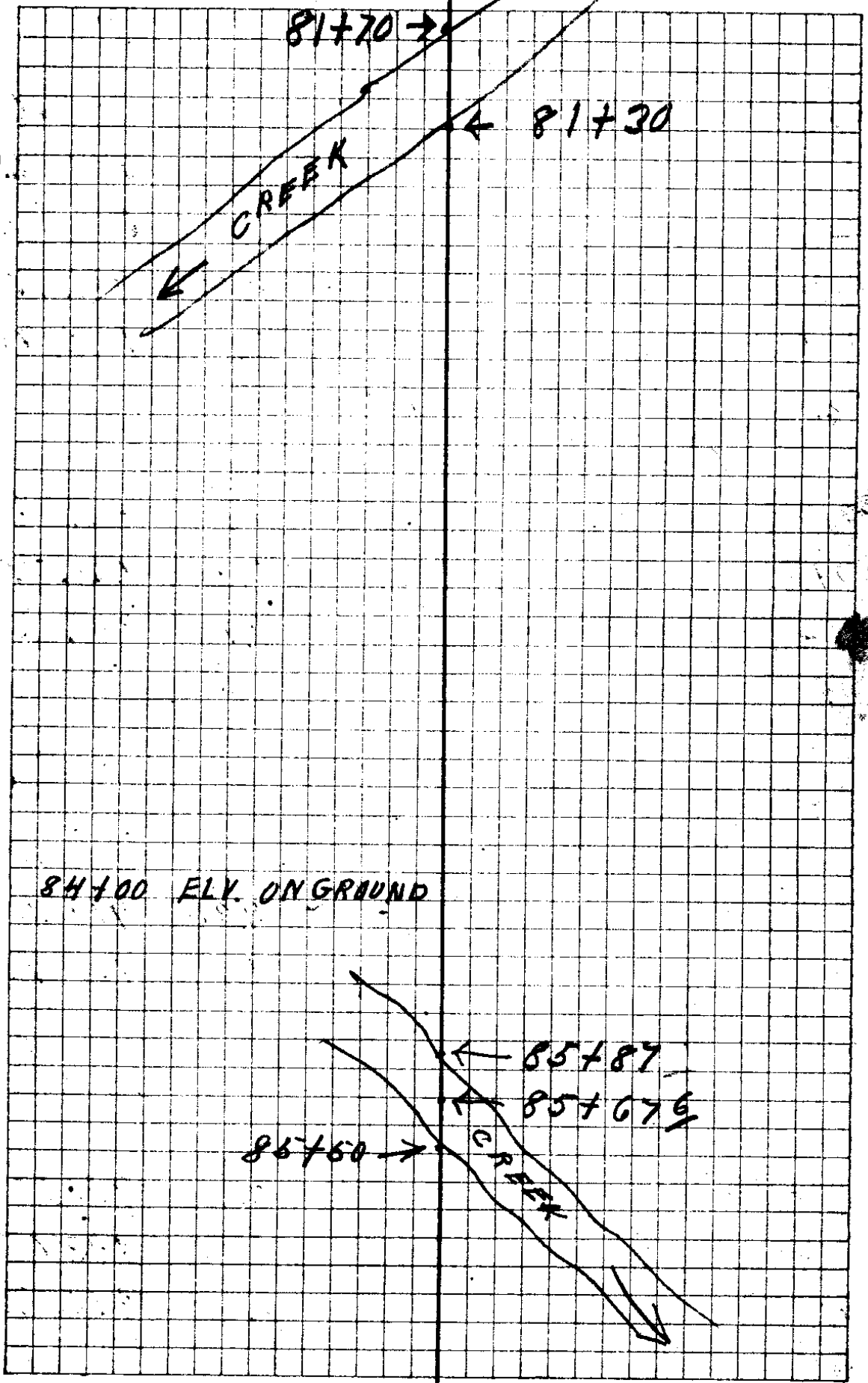


STA	+	π	-	ROD	ELV.
		887.95			
74+69 <sup>4</sup>				2.10	885.85
75+00				2.20	885.75
⊙		885.48	2.47.		
	6.50	891.98			
75+50				3.90	888.08
75+84 <sup>4</sup>				5.20	886.78
76+00				5.10	886.88
76+50				4.70	887.28
77+00				3.00	888.98
⊙		888.95	3.03		
	8.04	896.99			
77+50				5.90	891.09
77+82 <sup>5</sup>				4.80	892.19
78+00				4.30	892.69
78+50				4.50	892.49
78+75				11.70	885.29
79+00				11.80	885.19
79+25				10.90	886.09
79+50				6.60	890.39
80+00				0.80	896.19
⊙		896.19	0.80		
	8.27	904.46			

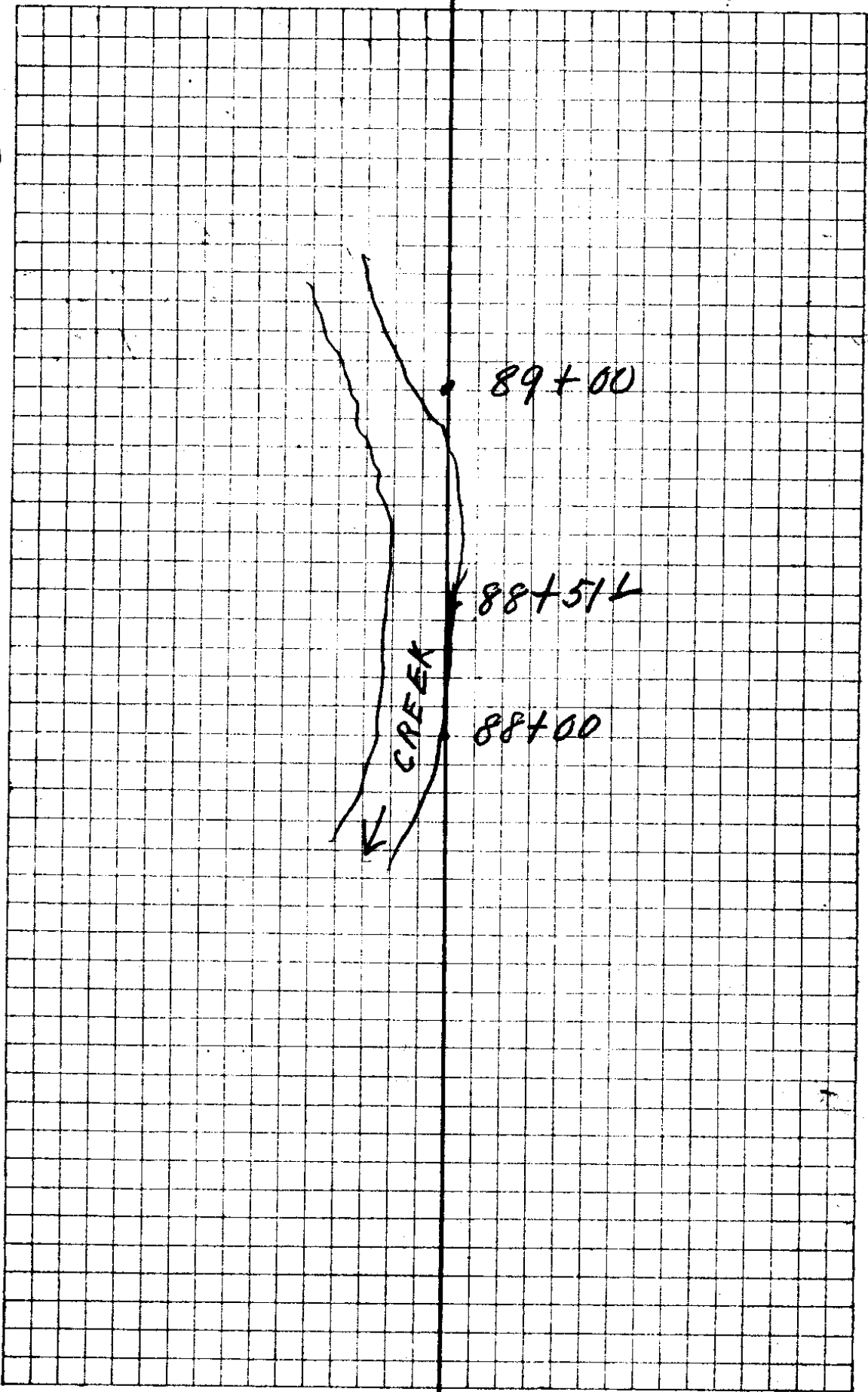


15-1

STA	+	⌊	-	ROD	ELK
		904.46			
80+39 <del>9</del>				6.30	898.16
80+74 <del>8</del>				4.00	900.46
81+00				5.40	899.06
81+30				9.40	895.06
81+77 <del>7</del>				4.70	899.76
⊙		899.72	4.74		
	9.70	909.42			
82+00				6.00	903.42
82+50				4.30	905.12
83+00				1.80	907.62
⊙		907.67	1.81		
	9.20	916.81			
83+37 <del>7</del>				4.70	912.11
83+50				5.10	911.71
84+00				4.20	912.61
84+50				4.80	912.01
⊙		911.99	4.82		
	2.44	914.43			
85+00				5.30	909.13
85+50				7.20	907.23
85+67 <del>6</del>				7.40	907.03
86+00				2.00	912.43



STA	+	π	-	ROD	ELV.
①		914.31	0.12		
	7.35	921.66			
<del>86+319</del>				<del>5.50</del>	
86+50				4.70	916.96
86+97 <sup>6</sup>				3.30	918.36
②		921.07	0.59		
	6.08	927.15			
87+50				4.30	922.85
87+85				3.40	923.75
88+00				8.70	918.45
88+51 <sup>4</sup>				10.50	916.65
89+00				6.70	920.45
③		920.46	6.69		
	12.87	933.33			
89+50				8.90	924.43
90+00				5.20	928.13
90+50				2.30	931.03
④		931.93	1.40		
	6.99	938.92			
90+80 <sup>6</sup>				5.80	933.12
91+00				5.00	933.92
91+50				2.60	936.32

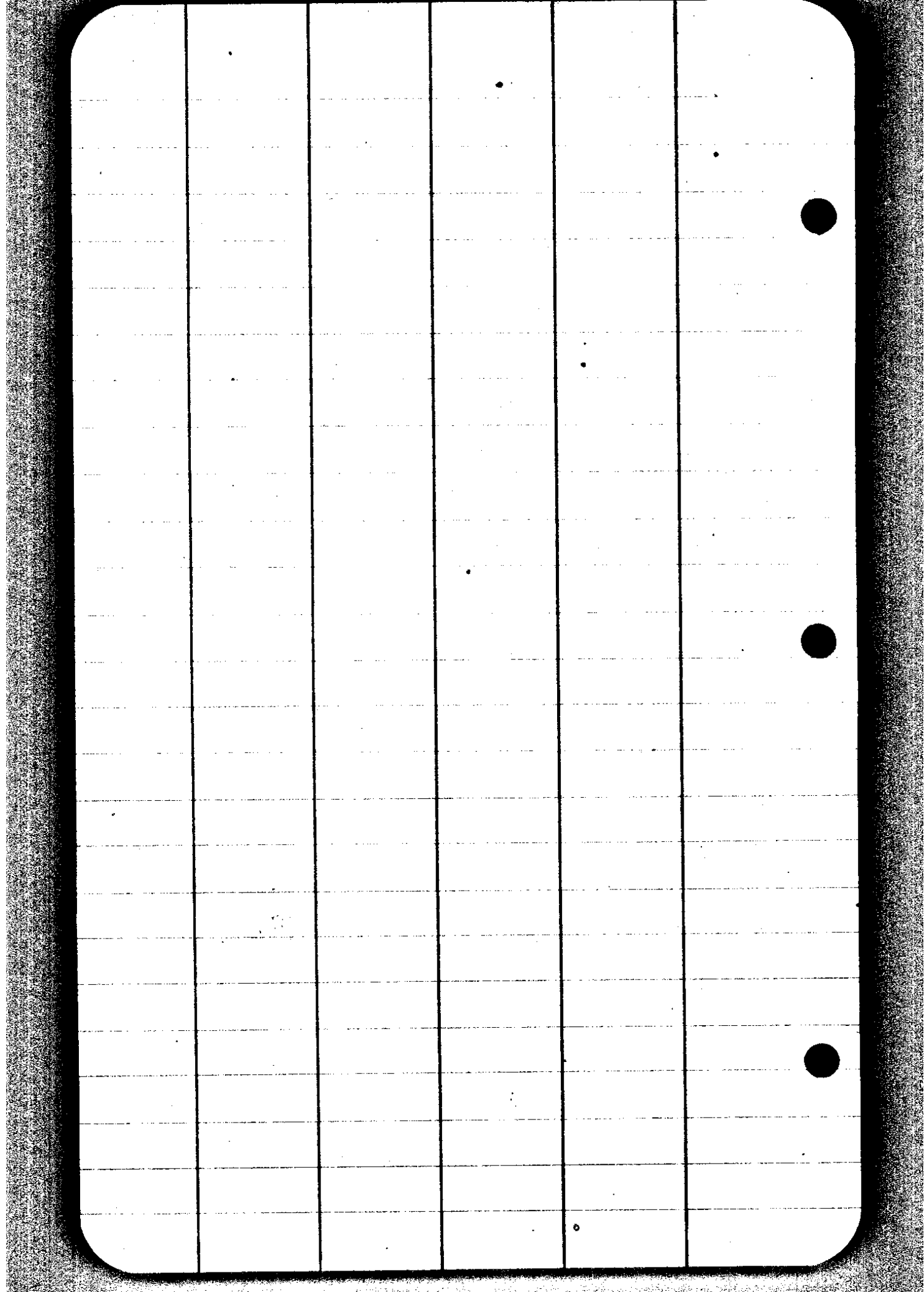


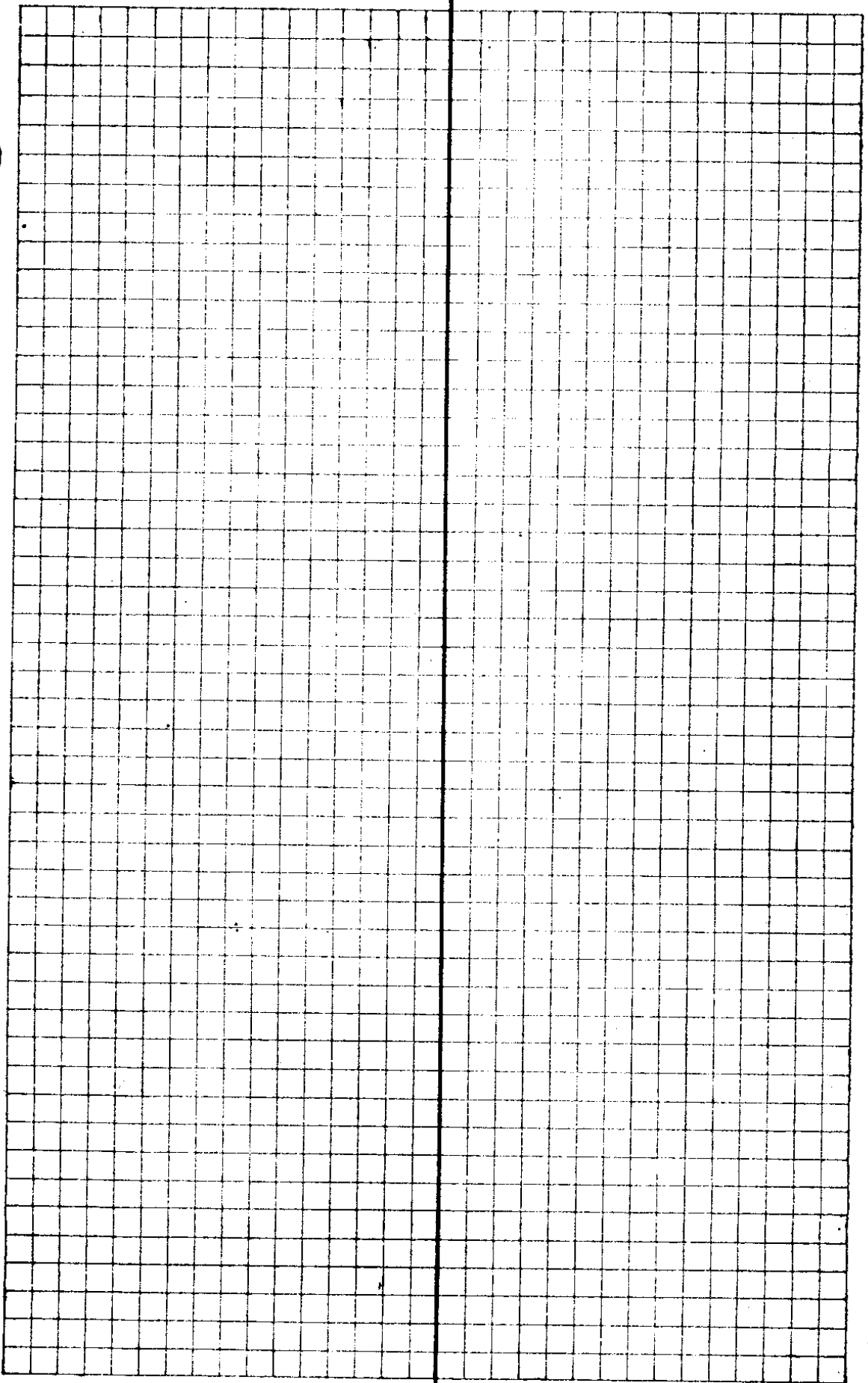
STA	+	$\pi$	-	ROD	FLV
		938.92			
92+00 <del>8</del>				5.70	933.22
92+50				7.90	931.02
93+00				6.80	932.12
93+27 <del>3</del>				5.20	933.72
B.M.				4.17	934.75

BM. ON 8 INCH ALDER

10 FEET TO RIGHT STA 92+75

$$\begin{array}{r} 832.78 \\ 106.14 \\ \hline 938.92 \end{array} \text{ K}$$
$$\begin{array}{r} + 171.97 \\ 65.83 \\ \hline 106.14 \end{array}$$

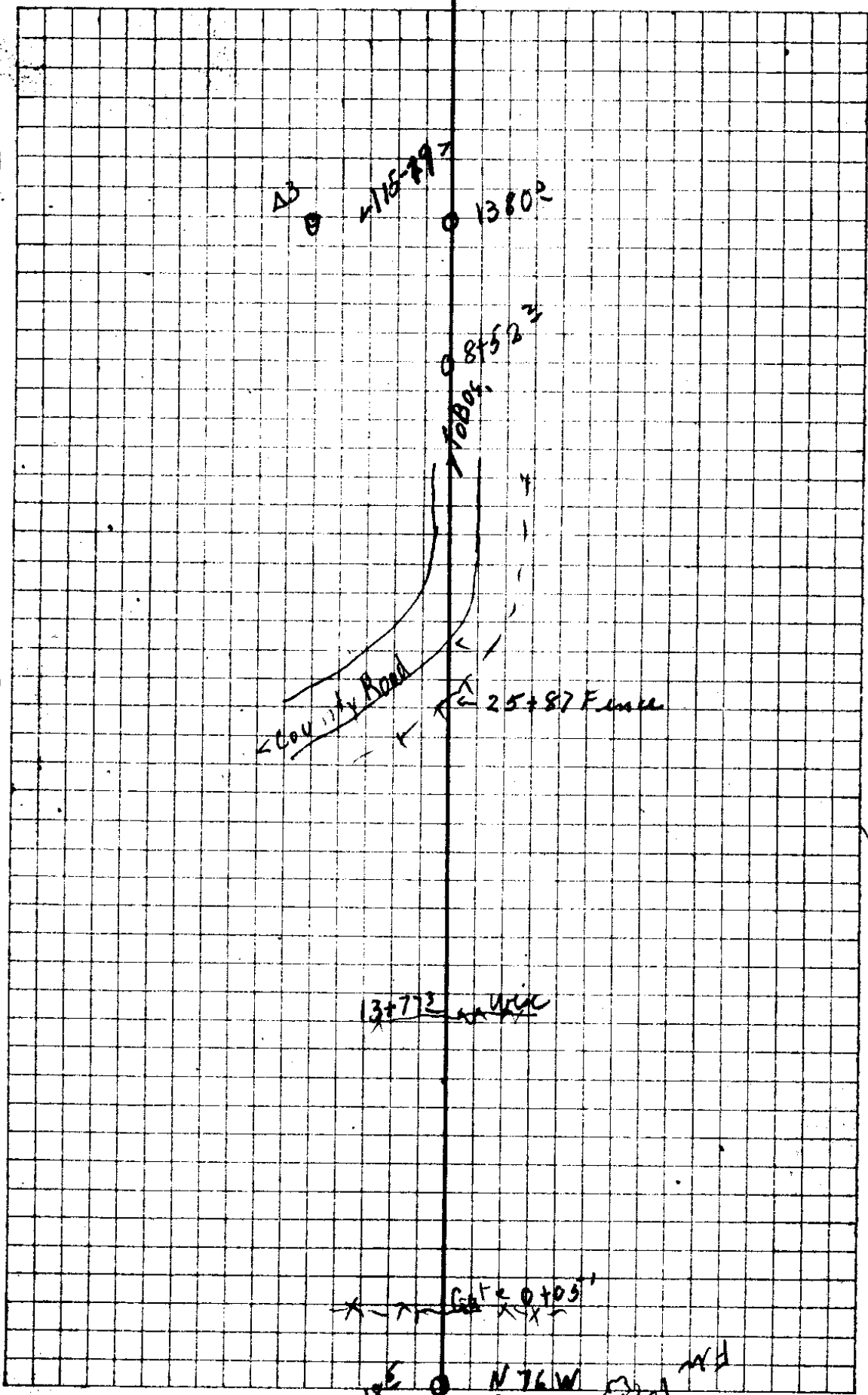




187

M<sup>o</sup> C / in tock Gateway Road.

Sta $\Delta 13$ $+80^3$	579	3-45L	N 86 30 W	S 87-02 E
$\Delta 3$	1000	10-20 L	N 83 W	S 83-17 E
20-30 100°				
$\Delta 2$	3870		47°-01	N 81-30 W S 81-57 E
-24° 100°				
$\Delta 1$	1193		S 51-30 W	N 51-02 E
Cor $\frac{23}{15}$				
26+00 End.				
			44-06 R	N 84-00 W N 84-55 W
25+17 1/2			18°-09 R	S 52 W S 51-04 W
24+30 1/2				
	720	2-53 L	S 33-30 W	S 32-55 W
17+10 1/2 in root			7-31 R	S 36 W S 35-48
13+80 1/2	528 1/2			
9+00 POT $\frac{1}{2}$			19-47 R	S 28-30 W S 28-17 W
8+52 1/2				
5+29 1/2	372		0-32 R	S 8°-30 W S 8-30 W
6+00				S 8° W S 8°-00' W



△ 115-79  
○ 13802

○ 8552

County Road

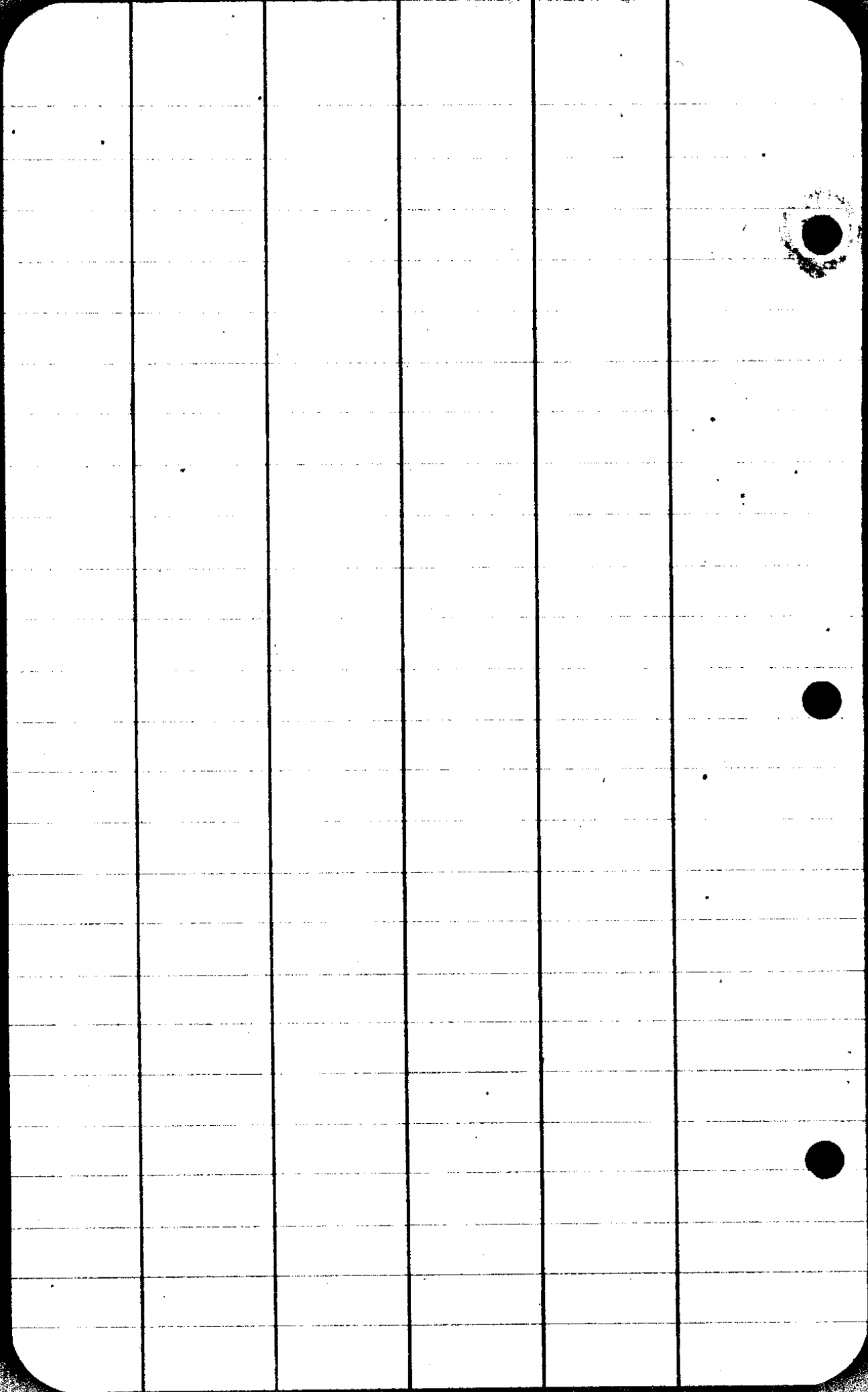
△ 25+87 Fence

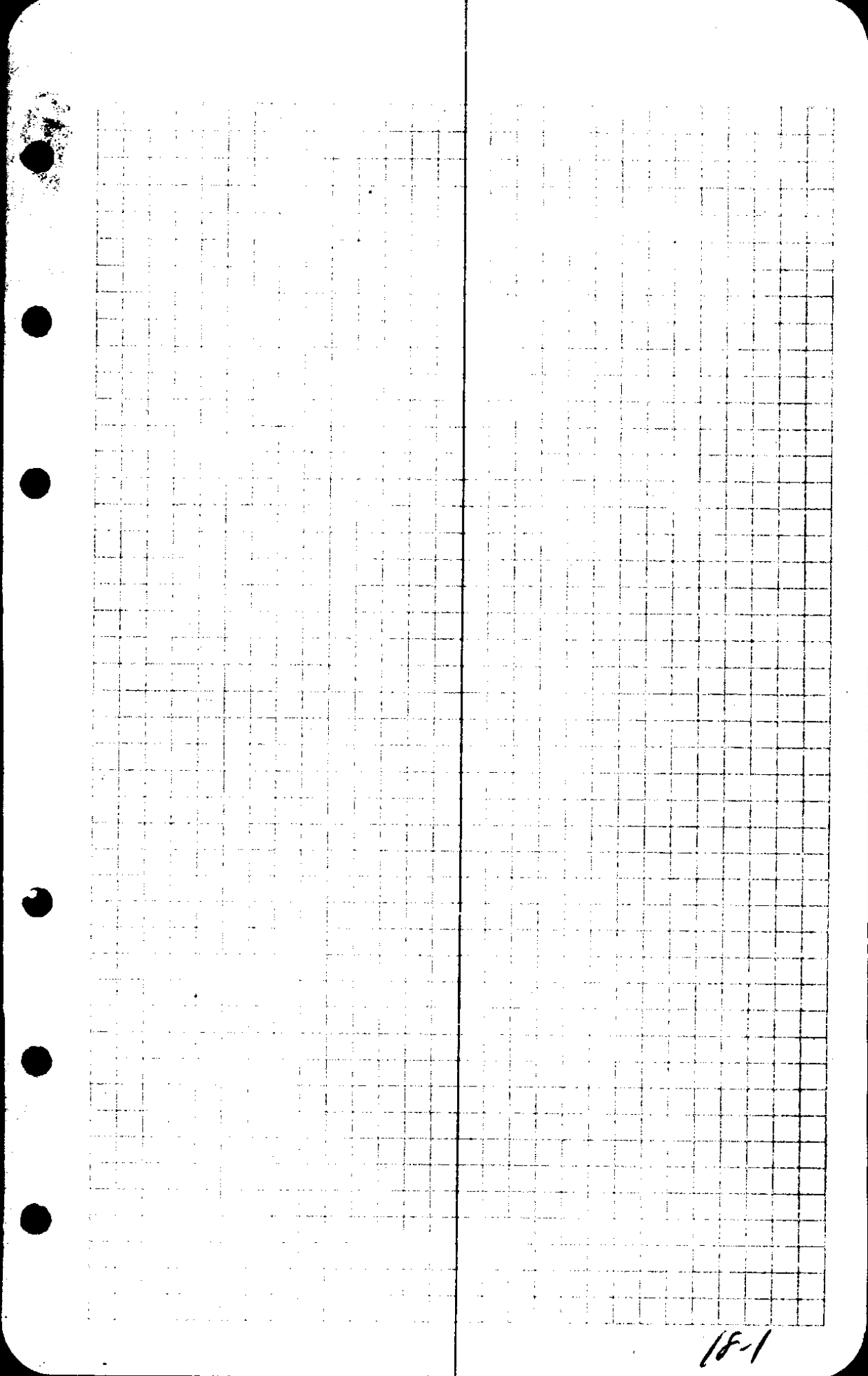
13+77

X 585

○ 585  
N 76 W  
151

○ 151  
151





18-1

① A

Left + Right  
CANYONVILLE  
Pipe Line

# 10

# 9

# 8

156<sup>8</sup>

21°48' N6°W S11-38E

# 7

109<sup>2</sup>

00°21' N34°W S33-26E

# 6

91<sup>0</sup>

10°58'

N39°W S33-47E

# 5

138<sup>0</sup>

25°25'

N22°W S22-49E

# 4

96<sup>3</sup>

14°58' N3°E S2-36E

# 3

299<sup>5</sup>

43°38' N11½°W S12-22E

# 2

175<sup>0</sup>

N56°W S56E

# 1

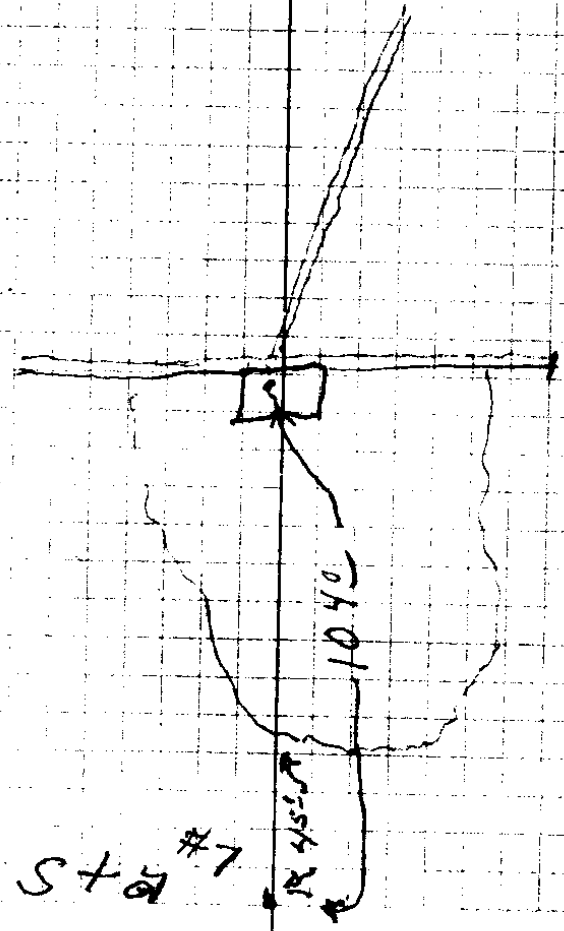
Red Fir 12  
24 Fir  $\odot$  N 63 3/4 W - 30 feet  
S 14 1/2 W 28 feet.

$\odot$  30" Fir  
N 20 5 feet  
S 30 1/2 E

PIPE

Vec 18 Fir  $\odot$   
~~32-30~~ 22  
22-30  
S 62 E

Sta #8



Sta #7

3A

Left Right  
9 feet to sta 74#00  
S.E.

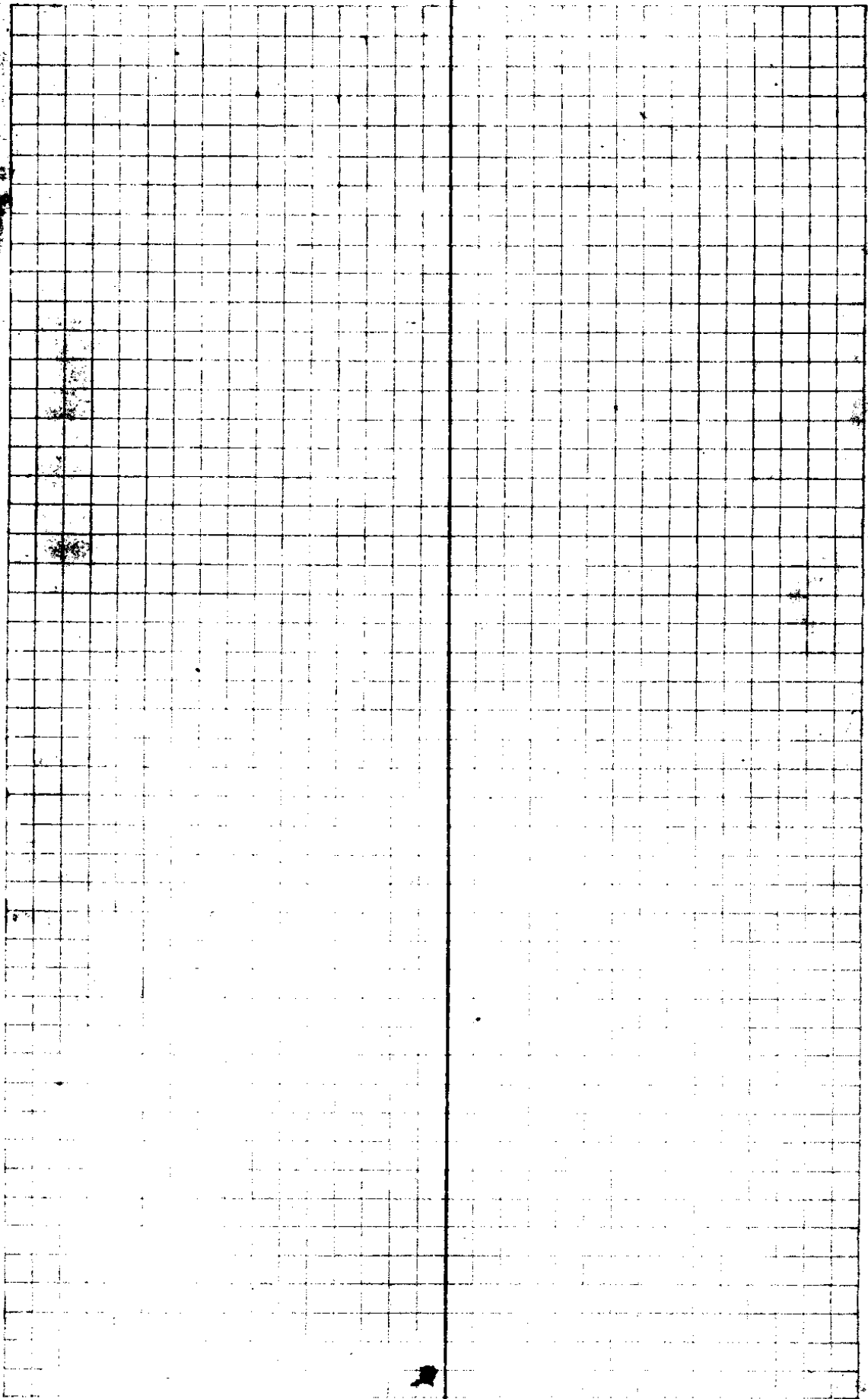
#9	(937)			
26-45	104 <sup>9</sup>		20-47	S20W S20-30W
#8	(1349)			
193 <sup>0</sup>	143 <sup>L</sup>		13-34	South SO-17E
#7				
	170 <sup>3</sup>	10-52		S14E S13-51E
#6				
	95 <sup>8</sup>	2°08'		S2°E S2-59E
#5				
	57 <sup>9</sup> 8	(573)	00°58'	South SO-51E
#4				
	15 <sup>8</sup> 40-15	(312)	12°38'	S1½E S1-49E
#3				
	28 <sup>9</sup>	11°56'		S14°E S14-27E
#2				
	64 <sup>9</sup>	4-61	4°01'	S2°E S2-31E

Hub #1

(172 <sup>0</sup> )				S1½W S1-30W
180 <sup>0</sup>				<del>S1020E</del>
17-07				

Sec cor.	26	25
	35	36

Tie  
wire



184

STA	R	L	MC	①
	P.O.T.			
36+00				
	P.O.T.			
32+00				
	P.O.T.			
31+00				
	P.O.T.			
23+563 <sup>POT</sup>				
	33° 18'		S 82° 30' E	S 83° 35' E
21+389 <sup>PI</sup>				
	P.O.T.			
20+349				
	P.O.T.			
18+464				
	11° 53' R		N 64° E	N 63-07 E
16+403				
	P.O.T.			
12+925				
	9° 30' R		N 52° E	N 51-14 E
10+313				
	2° 14' R		N 42° 30' E	N 41-44 E
3+174				
			N 39° 30' E	N 39-30 E
0+00				
X				

P.I. 21+38

$\Delta 33^{\circ}18'$   
12° C.R.

T 1426

L 2775

BC 19+963

EC 22+738

19+963  
0°13'  
20+00  
3°13'  
20+50  
6°13'  
21+00  
9°13'  
21+50  
12°13'  
22+00  
15°13'  
22+50  
18°39'  
22+738

$\Delta 11^{\circ}53'$   
6° C.R.

T 993

L 1982

BC 15+413

EC 17+393

P.I. 16+403

ENTER  
MR. GREEN

15+41 - 5°56'  
15+50 - 5°40'  
16+00 - 4°10'  
16+50 - 2°40'  
17+00 - 1°10'

$\Delta 9^{\circ}30'$

T 793

L 1583

6° C.R.

BC 9+519

EC 11+103

P.I. 10+313

Mr. Sailer

9+519 1°27'

10+00

10+50 2°57'

11+00 4°27'

11+103 4°45'

Mr. Gross

6+50

20+40

0+00

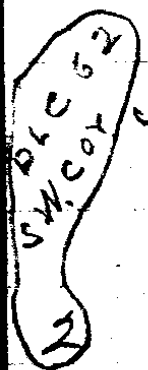
14'

(3)

R L MC

# Tie LINE

B.S. on Sta 10+31.2  
64°07'

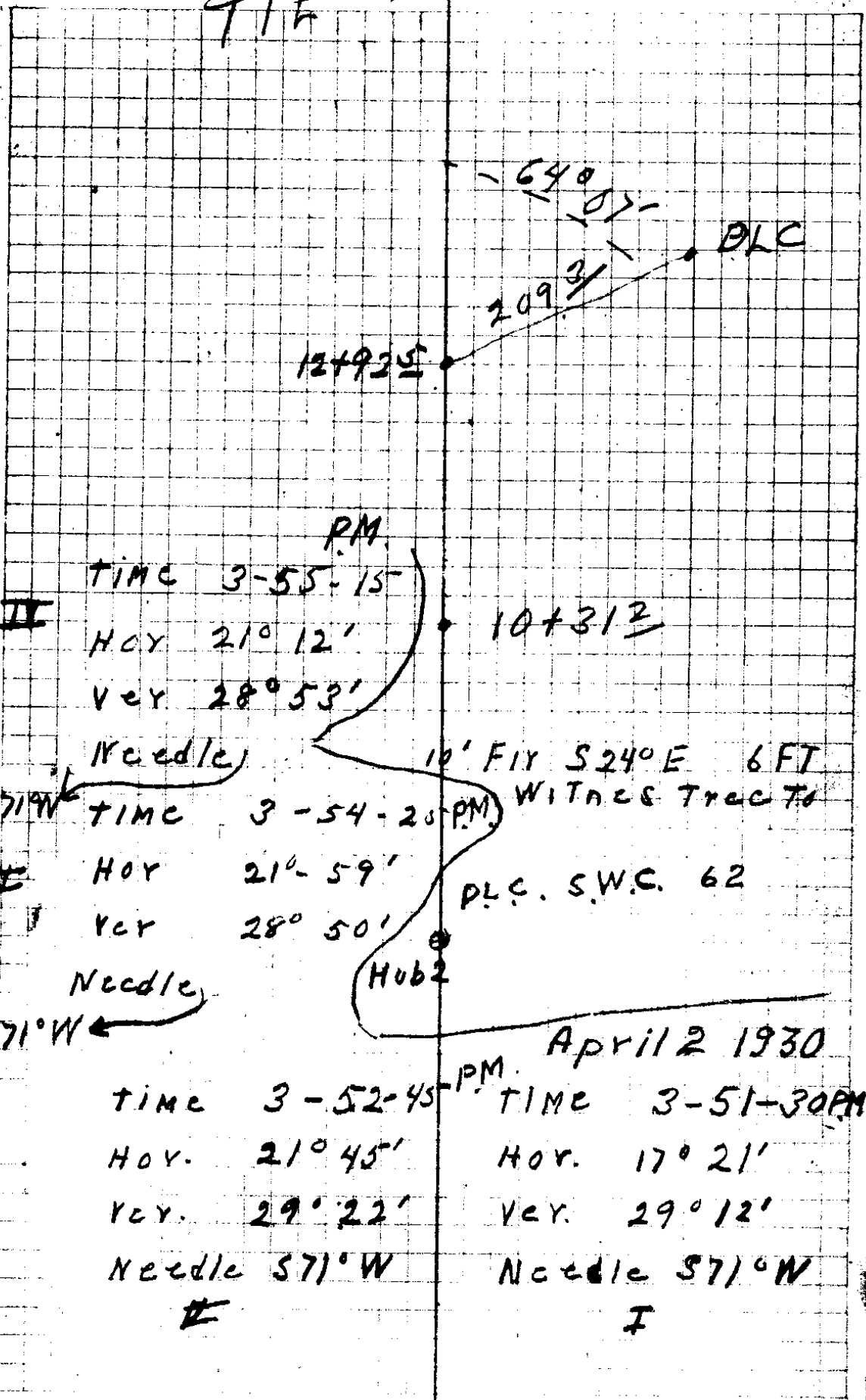


3	2093	19°11'	N64°W	N61-39W
2	100' 19° 415' 137'	41°11'	N44°30W	N42-28W
1	25' 8' 14' 30' 105'		N3°W	N1-19W

1/2' Iron Pipe Sec. Coy <del>26-27-34-35</del>	24' Fir	S88°E	69'
	18' W Oak	S77°E	26'
	28' W Oak	S9°W	33'
	30' B. Oak	N7°W	34'

# TIE LINE

(4)



PM.  
 TIME 3-55-15  
 HCY 21° 12'  
 VCY 28° 53'

10+312

Needle  
 S71°W  
 TIME 3-54-20 PM  
 HCY 21° 59'  
 VCY 28° 50'

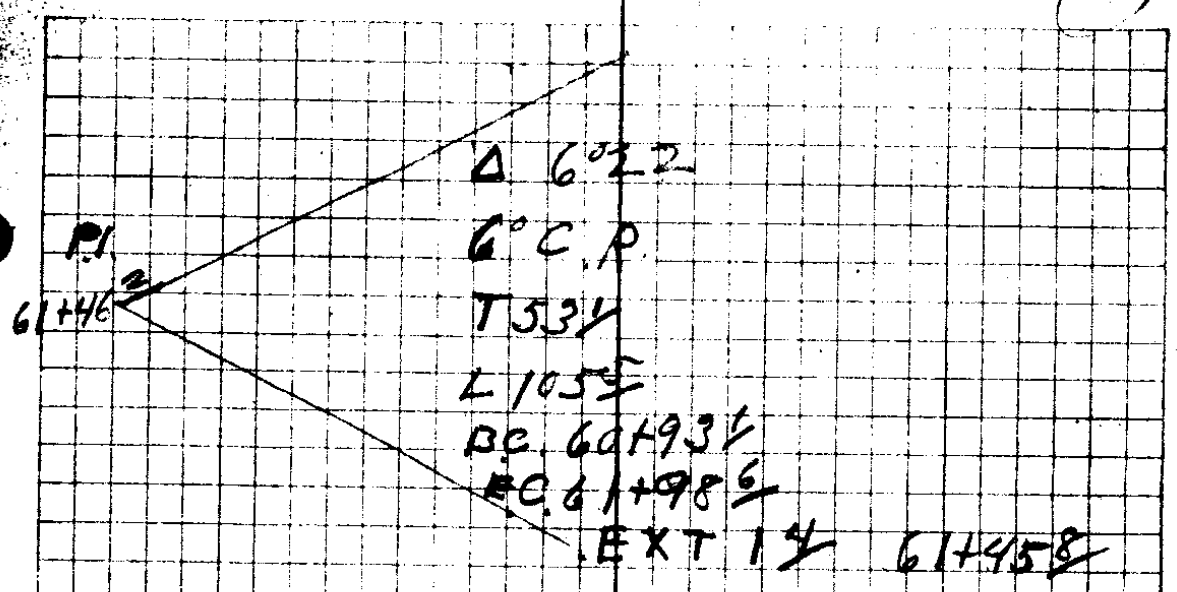
10' FIX S24°E 6 FT  
 WITNES TRACT  
 PLC. S.W.C. 62  
 Hub 2

Needle  
 S71°W  
 TIME 3-52-45 PM  
 HCY 21° 45'  
 VCY 29° 22'  
 Needle S71°W

April 2 1930  
 TIME 3-51-30 PM  
 HCY 17° 21'  
 VCY 29° 12'  
 Needle S71°W

Sta.	R.	L.	M.C.	(5)
			0° 44'	S 57° E 557-23E
63+33 $\frac{1}{2}$			6° 22'	S 56° E 556-39E
61+46 $\frac{1}{2}$			0° 34'	S 62° 30' E 563-01E
59+34 $\frac{1}{2}$			1° 09'	S 62° E 562-27E
55+51 $\frac{1}{2}$			6° 14'	S 61° E 561-18E
53+63 $\frac{1}{2}$			0° 10'	S 67° E 567-32E
51+16 $\frac{1}{2}$			3° 28'	S 67° E 567-42E
48+49 $\frac{1}{2}$			3° 34'	S 64° E 564-14E
45+74 $\frac{1}{2}$			1° 20'	S 67° E 567-48E
42+97 $\frac{1}{2}$			1° 37'	S 66° E 566-28E
42+43 $\frac{1}{2}$			15° 30'	S 67° 30' E 568-05E
39+56 $\frac{1}{2}$				
36+00	P.O.T.			

IV



$\Delta 15^{\circ}30'$   
 $5^{\circ} C.P.$   
 $L 310'$   
 $T 155'$   
 $B.C. 38+00'$   
 $E.C. 41+10'$

P.I.  
 $39+56.2'$

$38+00'$	-	$1^{\circ}14'$
$38+50'$	-	$2^{\circ}29'$
$39+00'$	-	$3^{\circ}45'$
$39+50'$	-	$4^{\circ}59'$
$40+00'$	-	$6^{\circ}14'$
$40+50'$	-	$7^{\circ}29'$
$41+00'$	-	$7^{\circ}45'$
$41+10'$	-	

EC 68+77<sup>2</sup>

EX 68+27<sup>8</sup>

S43-32E

BC 67+77<sup>8</sup>

66+93<sup>5</sup> EC 4-44'

+50 3<sup>0</sup>-39'

+5+00 2-2+

+35 1-9'

65+04<sup>3</sup> BC

S47-55E

Hob 65+99<sup>1</sup> = 11+87<sup>4</sup> Cap Line

Hob 65+33<sup>2</sup>

L 2<sup>0</sup>-14

Tie

164<sup>8</sup>

93-41L

S59E

S59-37E

Δ4

164<sup>8</sup>

10-40L

S34W

S34-04W

Δ3

228<sup>8</sup>

41-49L

S45W

S44-44W

Δ2

330<sup>8</sup>

35-33L

S86-30W

S86-33W

Δ1

211<sup>0</sup>

1<sup>0</sup>-01'L

N58W

N57-56W

3<sup>0</sup>0V

42<sup>0</sup>

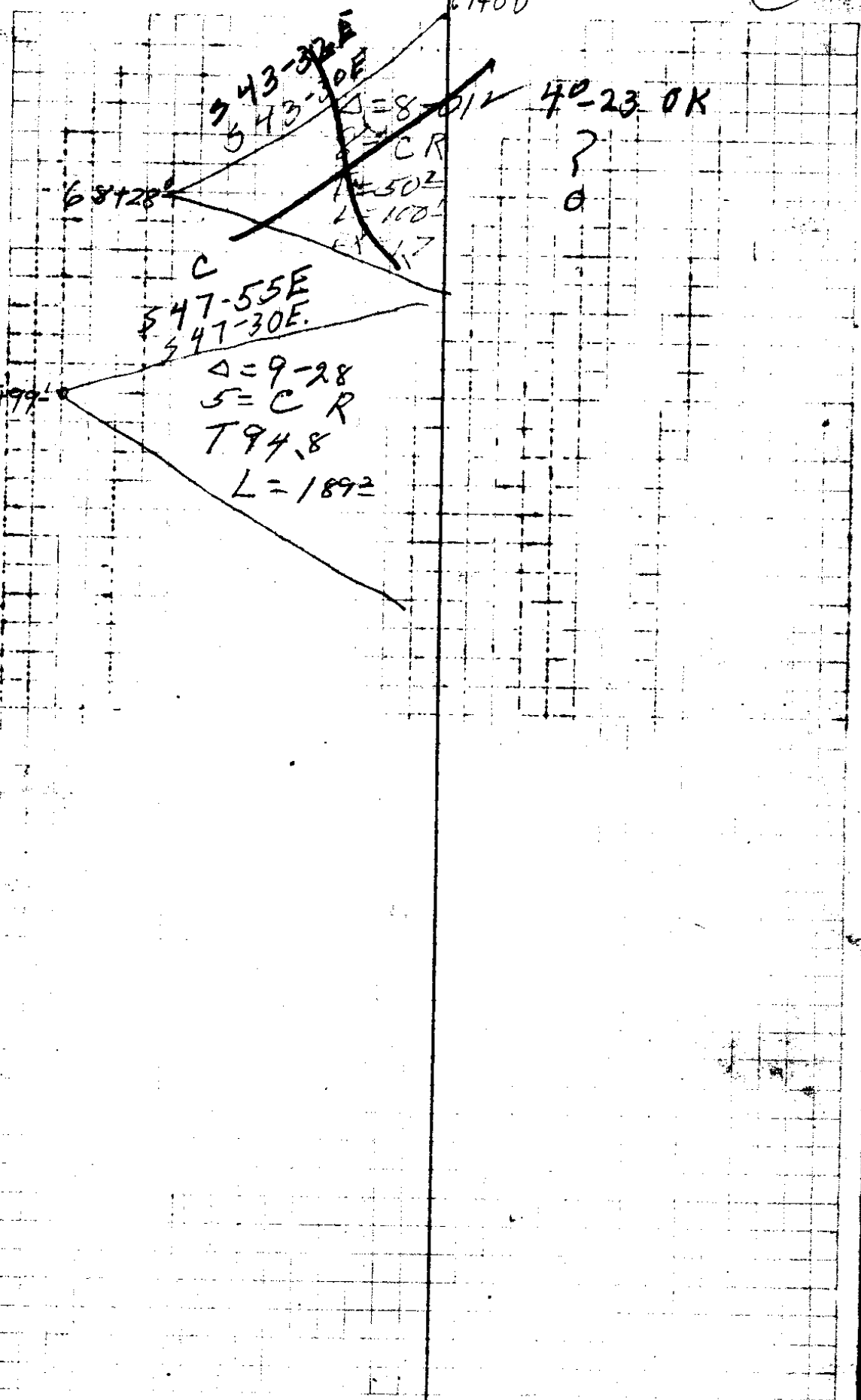
N56W

N56-55W

10<sup>0</sup> 410 EX

dt 10  
creek O'Hay  
1970

8



543-32E  
543-30E

$\Delta = 8-01$   
 $S = CR$   
 $T = 502$   
 $L = 100$   
 $EA = 17$

40-23 OK

?

68+28

C  
547-55E  
547-30E

65+99

$\Delta = 9-28$   
 $S = CR$   
 $T 94.8$   
 $L = 1892$

81+77<sup>2</sup> EC  
6-54

+30 5-33

81+00 3-03

+30 0-33'

BC 80 +399

81+09<sup>2</sup> PI

80+14<sup>2</sup> POTST

77+82<sup>2</sup>

1-51 L

S55W S54-51E

EC

75+844 10-43'

75+30 4-13'

75+00 6-06'

BC 74+624

EC

74+33<sup>0</sup> 90-50'

74+00 8-51'

+30 5-51

73+00 2-51

BC 72+52<sup>2</sup>

72+87<sup>2</sup> POT.  
S.T.

S41-04E

S53-00'E

S65-12E

S43-32E

541-04E  
 541E  
 81+09<sup>2</sup>      Δ = 13-47  
                   D = 10 R  
                   T = 693  
                   L = 137<sup>8</sup>      81+00

79+00  
 Crub

553-00E  
 553E  
 75+23<sup>8</sup>      Δ 12-12  
                   D = 10 R  
                   T = 61.2  
                   L = 122<sup>0</sup>

565-12C  
 565C  
 Δ = 21-40  
 12Ck  
 T = 91.3  
 L = 180<sup>8</sup>  
 73+33<sup>8</sup>  
 72+87<sup>3</sup>

93+27<sup>3</sup> EMD

S7-09E

S37-12E

S53-52E

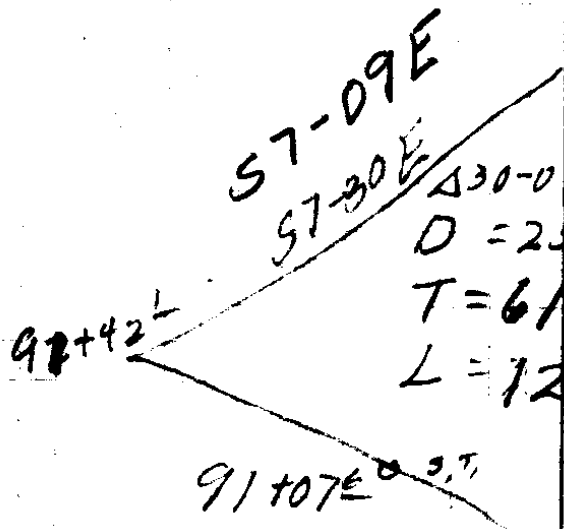
86+31<sup>8</sup>

2-31R

S38-30E S38-33E

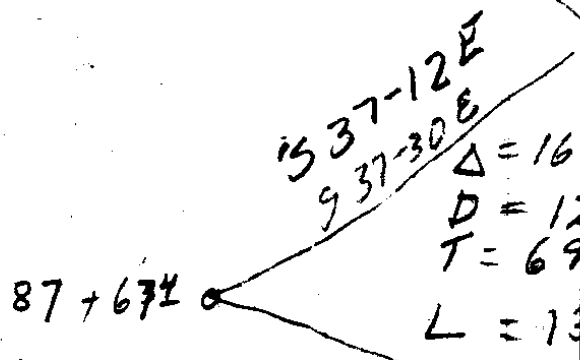
83+37<sup>7</sup>

91+42L  
645  
90+806



D = 25R  
T = 615  
L = 120

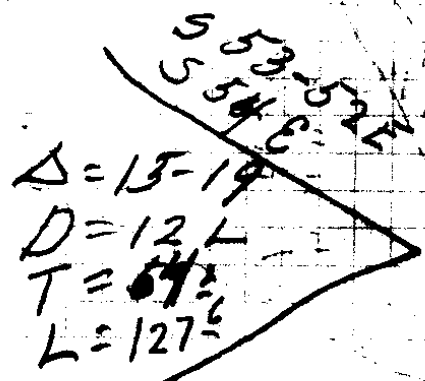
EC 92+00E  
1502  
92+50 8-41  
92+00 2-20  
BC = 90+80E



D = 120R  
T = 69E  
L = 138

EC 88+36L  
8°18'  
88+00  
87+50 6-8  
87+00 3-08  
BC = 86+97E

EC 86+95E 2-43  
+50 5°43'  
86 7°40'



D = 12L  
T = 54  
L = 127

BC 85+67E in Creek  
86-31E

81

54-59 R N 86 W

0100

Bank right on 3+ Hob



795

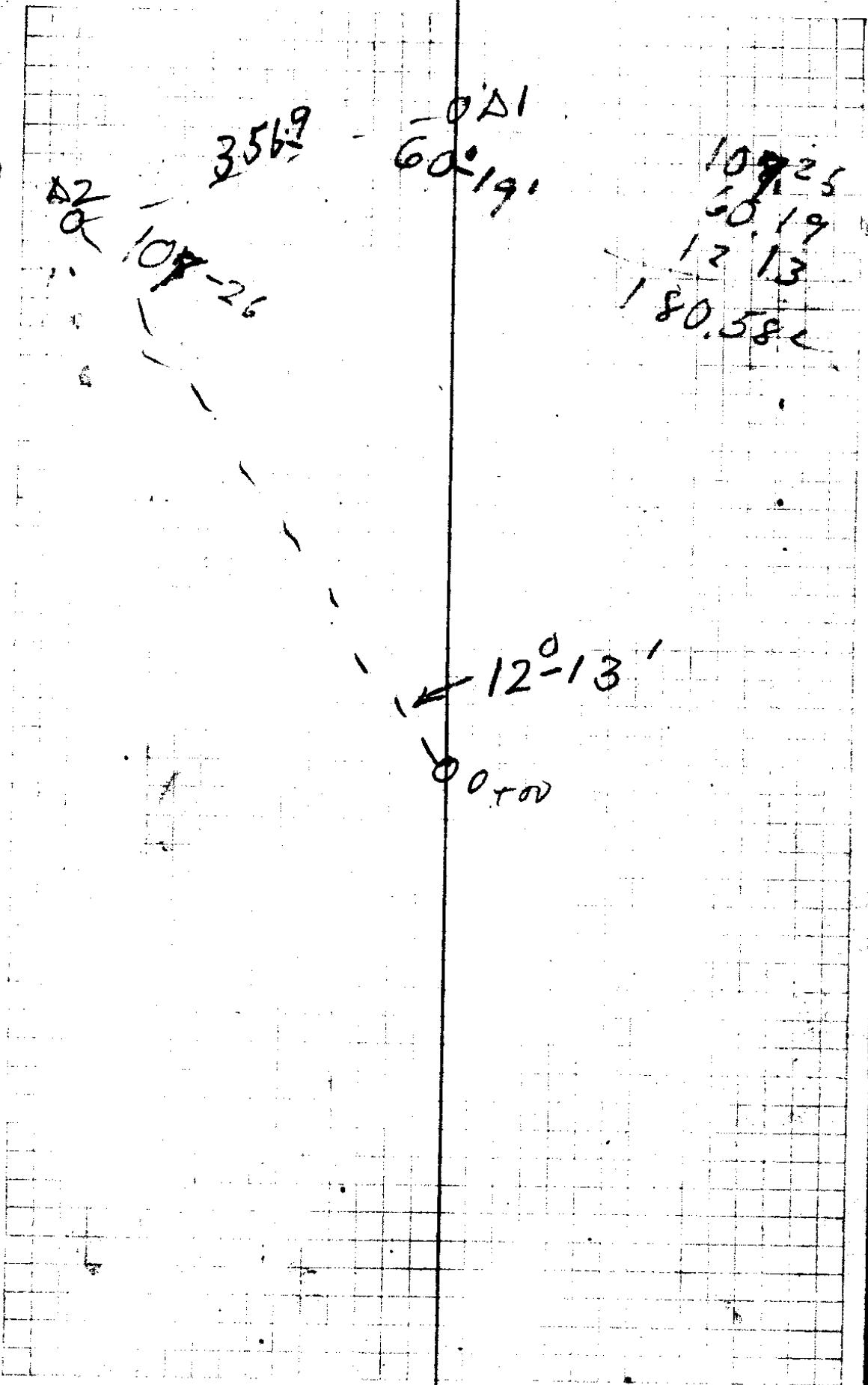
8100

675

2 14 1/2 1/2

pipeline





A2  
Q

107-26

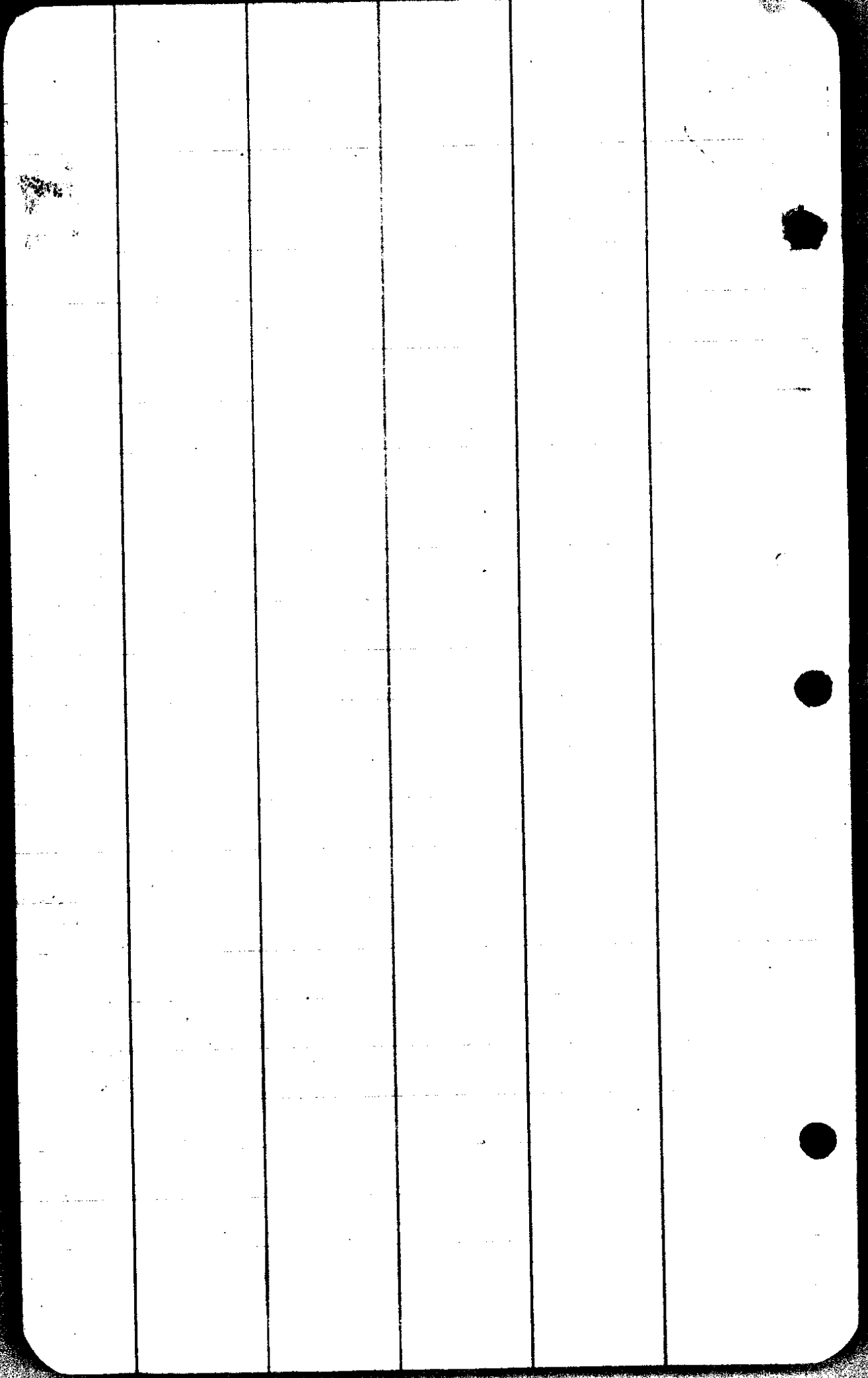
356-9

0-01  
60-19

107-25  
50-19  
12-13  
180.584

12-13

0-00



CS FILE FOLDER

CONTAINS

MORE

INFORMATION