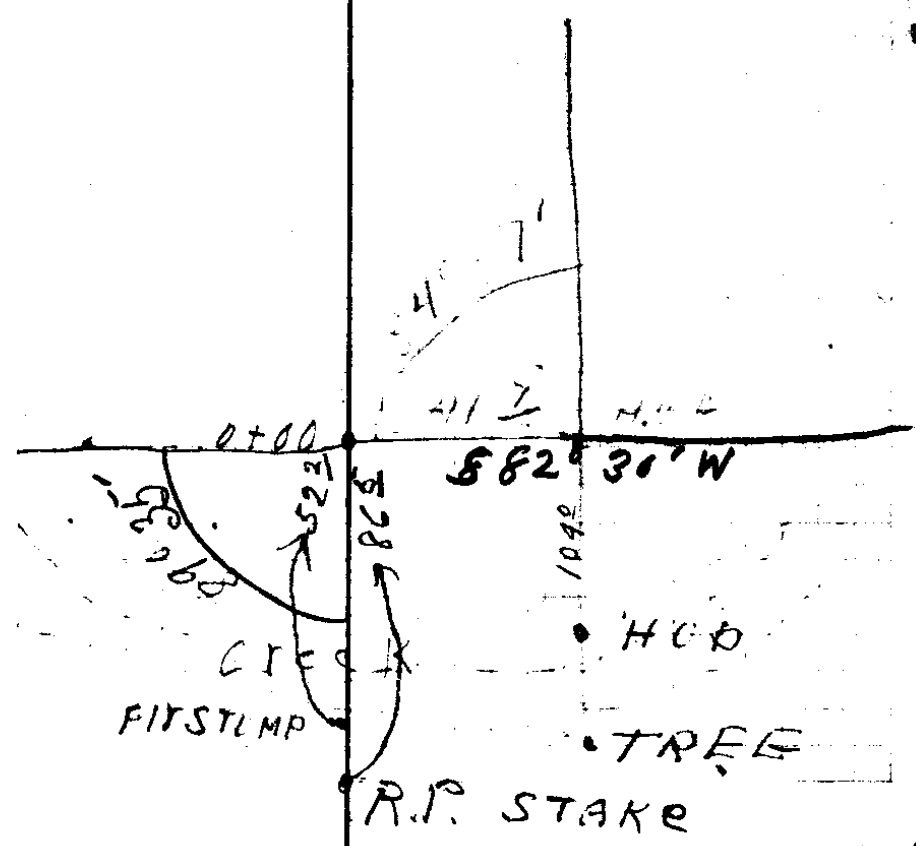


A.S. Wallace

1

17-52

23
R/D.



BM ON FIR TREE

100.00

2

STA

+

⌒

-

ROD

ELV

0.22

100.22

0.22

100

FINISH LEVEL

0+00

~~2.22~~

4.75

95.47

⊙

99.05 1.17

4

14.88 113.93

0+20

5.10 108.83

⊙

113.87 0.06

12.72 126.59

0+37.3

5.10 121.99

0+40

4.70 121.89

⊙

122.32 4.27

14.55 136.87

0+50

5.70 131.17

0+60

1.35 135.52

⊙

136.61 0.26

13.73 150.34

0+70

9.80 140.54

0+80

5.70 144.64

⊙

149.63 0.71

15.02 164.65

1+00

8.50 156.15

1.12

4.47

470
3502
7443

11. 23
10. 22
9. 21

3

1702

STC	+	π	-	ROD	ELV (4)
0		163.04	1.61		
	15.50	178.54			
420				13.20	165.34
1+40				3.00	175.54
0		176.52	2.02		
	15.83	192.35			
1+60				4.70	187.95
0		191.74	0.64		
	15.5	207.21			
1+80				6.60	200.61
0		206.49	1.77		
	16.24	222.68			
2+00				9.70	213.28
2+20				3.55	222.33

63.07	5.09
71.12	6.47
<u>34.19</u>	<u>1.51</u>
11.51	
<u>122.68</u>	
100	
<u>222.68</u>	

O.K.

~~63.07~~
~~70.90~~
~~133.97~~
~~11.51~~
122.46

~~5.04~~
~~6.41~~
~~11.51~~

5
95.47
121.46
~~95.47~~
~~132.92~~
128.44

222.67
95.47
127.20

~~63.07~~
~~70.90~~
~~133.97~~
~~11.51~~
~~122.46~~
~~122.88~~
122.68
10.0
222.68

~~5.04~~
~~6.41~~
11.51

6

$$\begin{array}{r} 90.7 \\ -9.9 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 96.5 \\ -3.5 \\ \hline 20 \end{array}$$

$$0 + 00 \quad 101.2$$

$$C \quad \frac{11.2}{20}$$

$$\begin{array}{r} 97.90 \\ -2.5 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 109.9 \\ -3.5 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 114.4 \\ +1.0 \\ \hline 20 \end{array}$$

$$0 + 10$$

$$C$$

$$\begin{array}{r} 99.1 \\ -2.3 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 107.9 \\ -1.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 113.1 \\ -1.3 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 120.9 \\ -5.5 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 126.9 \\ -0.4 \\ \hline 20 \end{array}$$

$$0 + 40$$

$$\begin{array}{r} 114.9 \\ -2.5 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 119.8 \\ -2.0 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 123.1 \\ -1.7 \\ \hline 80 \end{array}$$

$$\begin{array}{r} 126.1 \\ -1.4 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 133.5 \\ -6.6 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 139.4 \\ -0.7 \\ \hline 10 \end{array}$$

$$0 + 60$$

$$C$$

$$\begin{array}{r} 120.7 \\ -2.5 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 126.7 \\ -2.5 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 132.7 \\ -1.6 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 137.2 \\ -2.2 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 142.9 \\ -6.3 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 149.2 \\ -0.9 \\ \hline 20 \end{array}$$

$$0 + 80$$

$$C$$

$$\begin{array}{r} 144.2 \\ -1.6 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 147.7 \\ -1.3 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 150.7 \\ -1.0 \\ \hline 80 \end{array}$$

$$\begin{array}{r} 154.2 \\ -6.3 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 158.7 \\ -2.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 161.2 \\ +0.5 \\ \hline 20 \end{array}$$

$$1 + 00$$

$$C$$

$$\begin{array}{r} 152.4 \\ -1.9 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 154.9 \\ -1.5 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 157.9 \\ -1.2 \\ \hline 80 \end{array}$$

$$\begin{array}{r} 162.9 \\ -7.0 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 167.9 \\ -2.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 170.4 \\ +0.3 \\ \hline 20 \end{array}$$

$$1 + 20$$

$$C$$

$$\begin{array}{r} 160.6 \\ -1.9 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 166.6 \\ -1.3 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 169.1 \\ -1.1 \\ \hline 80 \end{array}$$

$$\begin{array}{r} 173.6 \\ -6.5 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 175.6 \\ -4.5 \\ \hline 40 \end{array}$$

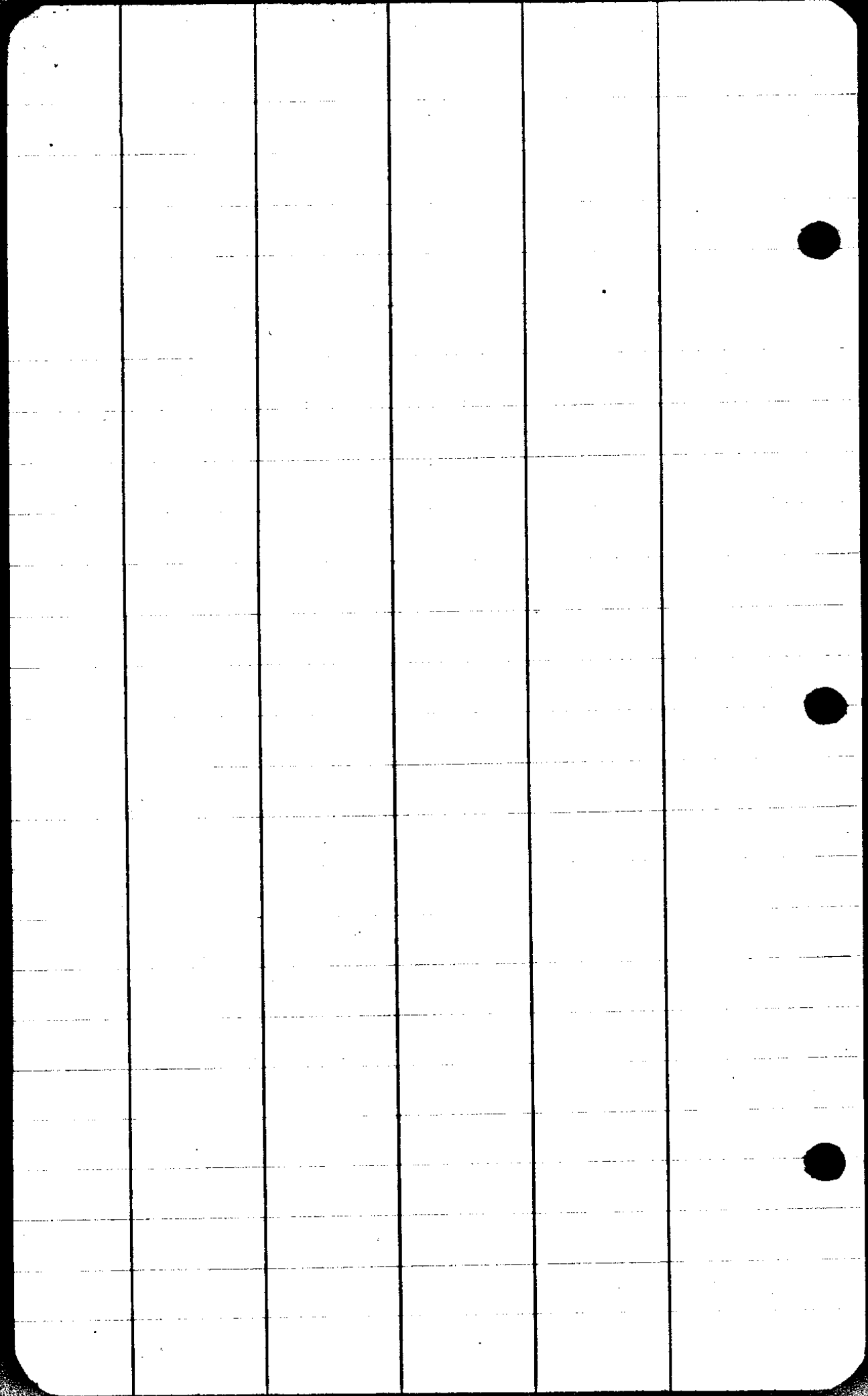
$$\begin{array}{r} 178.6 \\ -1.5 \\ \hline 20 \end{array}$$

$$1 + 40$$

$$C$$

192.5	190.5	188.0	184.5	178.5	174.0	169.5	165.5	160.0 (9)
$\frac{-20}{20}$	$\frac{-45}{40}$	$\frac{-80}{60}$	$\frac{-140}{80}$	$\frac{-185}{100}$	$\frac{-230}{120}$	$\frac{-270}{140}$	$\frac{-320}{160}$	
2026	199.6	193.6	190.1	186.1	180.1	174.1	172.6	
$\frac{-20}{20}$	$\frac{-55}{40}$	$\frac{-115}{60}$	$\frac{-150}{80}$	$\frac{-190}{100}$	$\frac{-250}{120}$	$\frac{-310}{140}$	$\frac{-325}{160}$	
216.3	214.3	208.8	204.8	200.8	195.3	190.3	186.8	
$\frac{-15}{20}$	$\frac{-35}{40}$	$\frac{-90}{60}$	$\frac{-130}{80}$	$\frac{-170}{100}$	$\frac{-220}{120}$	$\frac{-275}{140}$	$\frac{-310}{160}$	

225.9	223.9	220.4	214.9	208.9	206.4	198.4	194.9
$\frac{-10}{20}$	$\frac{-30}{40}$	$\frac{-65}{60}$	$\frac{-120}{80}$	$\frac{-180}{100}$	$\frac{-225}{120}$	$\frac{-285}{140}$	$\frac{-320}{160}$



140.0 99.0 96.5 93.0 90.0
113.4 119 110.4 105.4 104.4 100.4 98.4

$\frac{12}{400}$ $\frac{-3.5}{60}$ $\frac{-7.0}{80}$ $\frac{-10.2}{100}$
 $\frac{11.5}{26}$ $\frac{-3.0}{40}$ $\frac{-8.2}{60}$ $\frac{-9.0}{80}$ $\frac{-13.0}{100}$ $\frac{+15.0}{120}$
126.4 124.4 121.4 113.9 108.4 105.9 103.4
 $\frac{-2.0}{20}$ $\frac{-5.0}{40}$ $\frac{-12.5}{60}$ $\frac{-18.2}{80}$ $\frac{-20.5}{100}$ $\frac{-23.0}{120}$

140.1 136.1 132.1 129.1 123.6 117.6 112.1 108.1
 $\frac{4.0}{20}$ $\frac{-8.0}{40}$ $\frac{-11.0}{60}$ $\frac{-16.5}{80}$ $\frac{-22.5}{100}$ $\frac{-28.2}{120}$ $\frac{-32.0}{140}$

149.2 146.7 144.7 139.2 132.7 128.7 123.2 117.7
 $\frac{-2.5}{20}$ $\frac{-4.5}{40}$ $\frac{-10.2}{60}$ $\frac{-16.5}{80}$ $\frac{-20.5}{100}$ $\frac{-26.0}{120}$ $\frac{-31.5}{140}$

160.7 159.7 155.7 152.2 145.2 142.2 136.2 130.7 125.7
 $\frac{-1.2}{20}$ $\frac{-5.0}{40}$ $\frac{-8.5}{60}$ $\frac{-15.5}{80}$ $\frac{-18.5}{100}$ $\frac{-24.5}{120}$ $\frac{-30.0}{140}$ $\frac{-35.2}{160}$

169.9 169.9 167.4 165.4 158.9 152.4 145.4 138.4 134.4
 $\frac{-0.0}{20}$ $\frac{-2.5}{40}$ $\frac{-4.5}{60}$ $\frac{-11.0}{80}$ $\frac{-17.5}{100}$ $\frac{-24.5}{120}$ $\frac{-31.5}{140}$ $\frac{-35.5}{160}$

180.1 181.1 178.1 174.6 168.0 165.1 158.1 154.1 148.1
 $\frac{+1.0}{20}$ $\frac{-2.0}{40}$ $\frac{-5.5}{60}$ $\frac{-11.5}{80}$ $\frac{-15.0}{100}$ $\frac{-22.0}{120}$ $\frac{-26.0}{140}$ $\frac{-32.0}{160}$

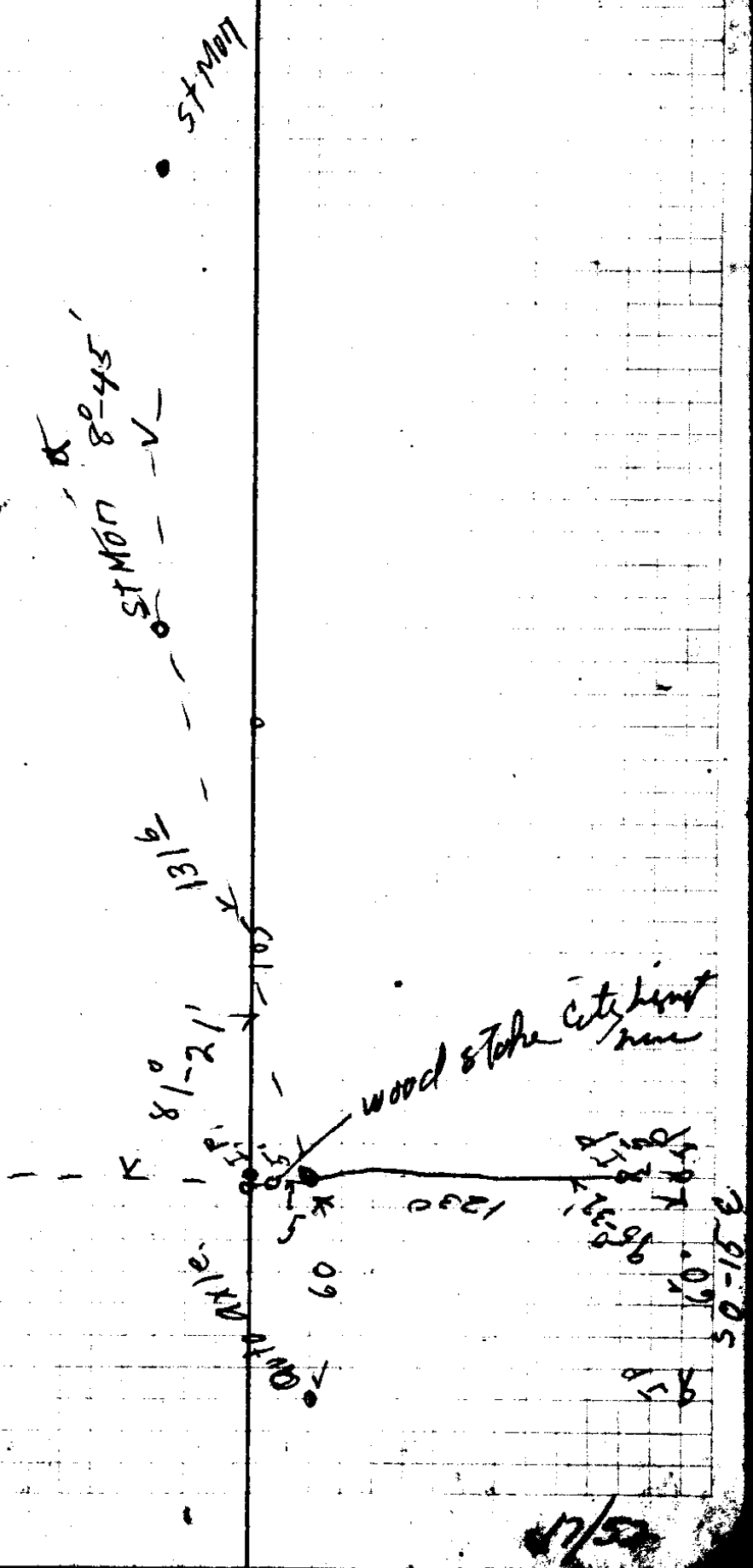
n/a

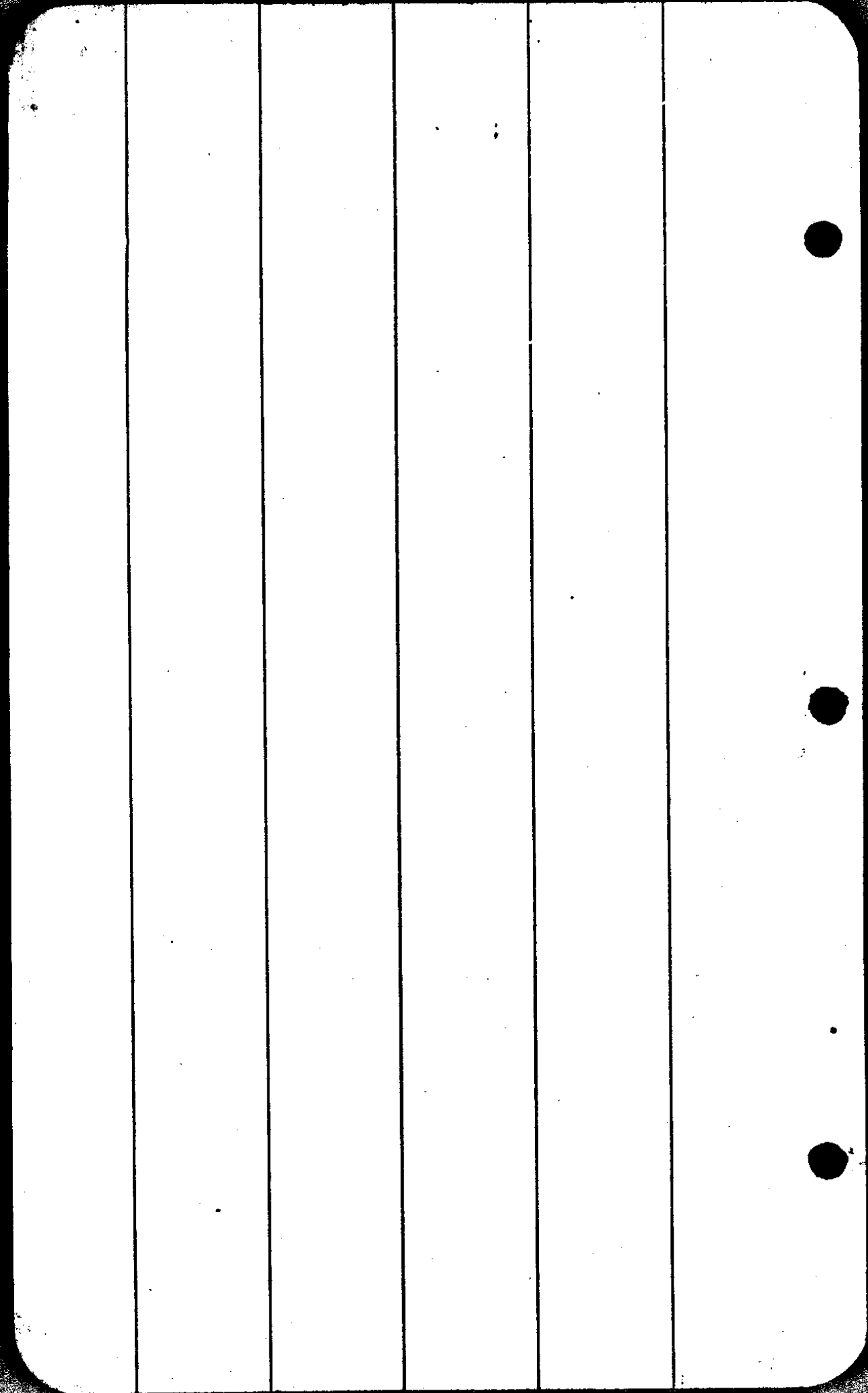
②

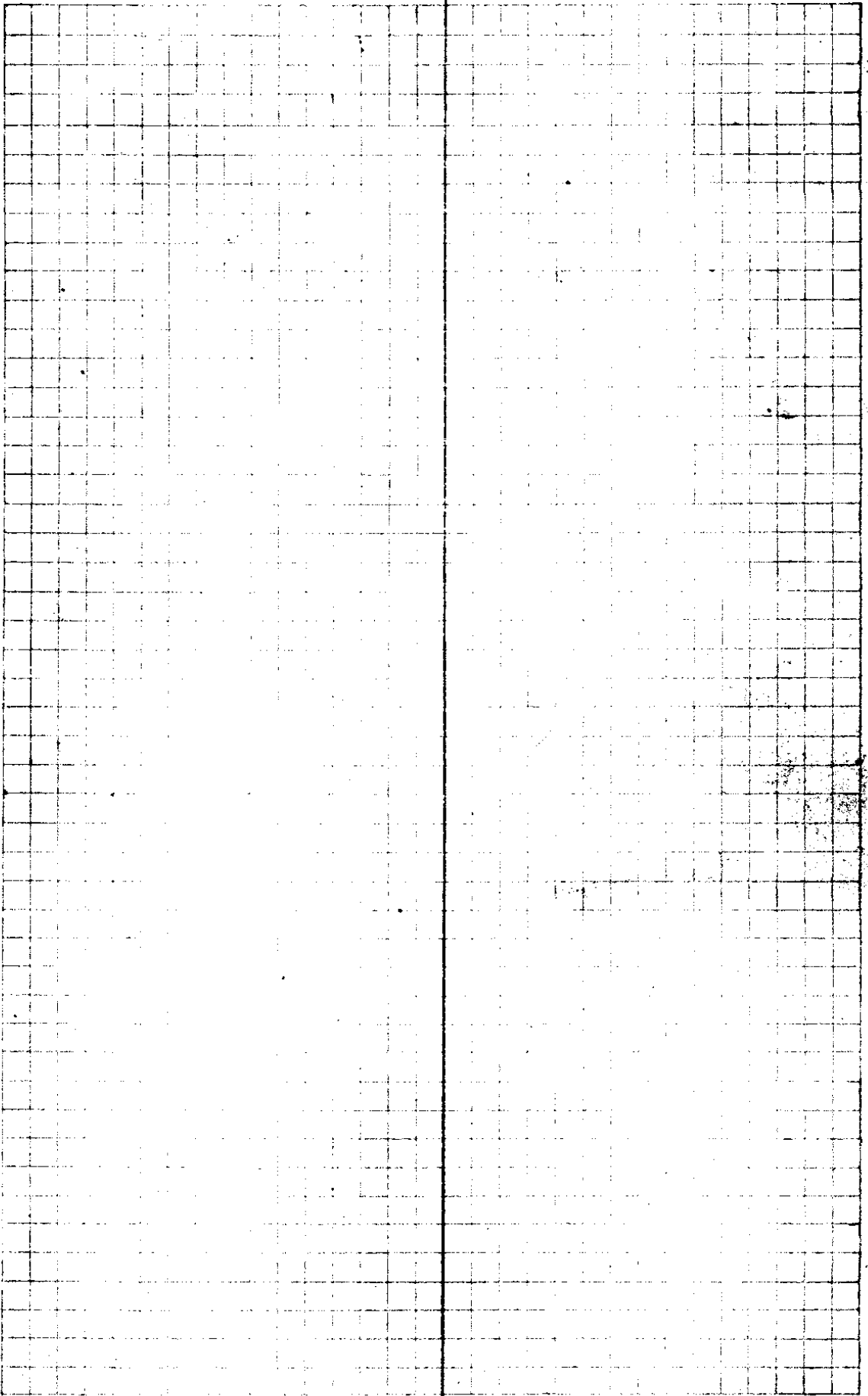
$\frac{16^{\circ}}{120}$	$\frac{12^{\circ}}{120}$	$\frac{8^{\circ}}{80}$	$\frac{5^{\circ}}{60}$	$\frac{7^{\circ}}{40}$	$\frac{10^{\circ}}{20}$	
176.5	180.5	189.5	187.5	191.5	193.5	1760
$\frac{15^{\circ}}{120}$	$\frac{10^{\circ}}{100}$	$\frac{10^{\circ}}{80}$	$\frac{4^{\circ}}{60}$	$\frac{20^{\circ}}{40}$	$\frac{10^{\circ}}{20}$	C
190.1	194.6	197.1	200.6	203.1	205.1	
$\frac{18^{\circ}}{120}$	$\frac{13^{\circ}}{100}$	$\frac{7^{\circ}}{80}$	$\frac{7^{\circ}}{60}$	$\frac{3^{\circ}}{40}$	$\frac{10^{\circ}}{20}$	285.1
199.3	204.8	208.3	210.8	214.3	216.8	
$\frac{7^{\circ}}{120}$	$\frac{4^{\circ}}{80}$	$\frac{2^{\circ}}{60}$	$\frac{1^{\circ}}{60}$	$\frac{0.5^{\circ}}{40}$	$\frac{0.5^{\circ}}{20}$	2100
219.9	222.9	224.4	225.4	226.4	226.9	217.8
						C
						2120
						226.9

Near Drain

Orie Wallace





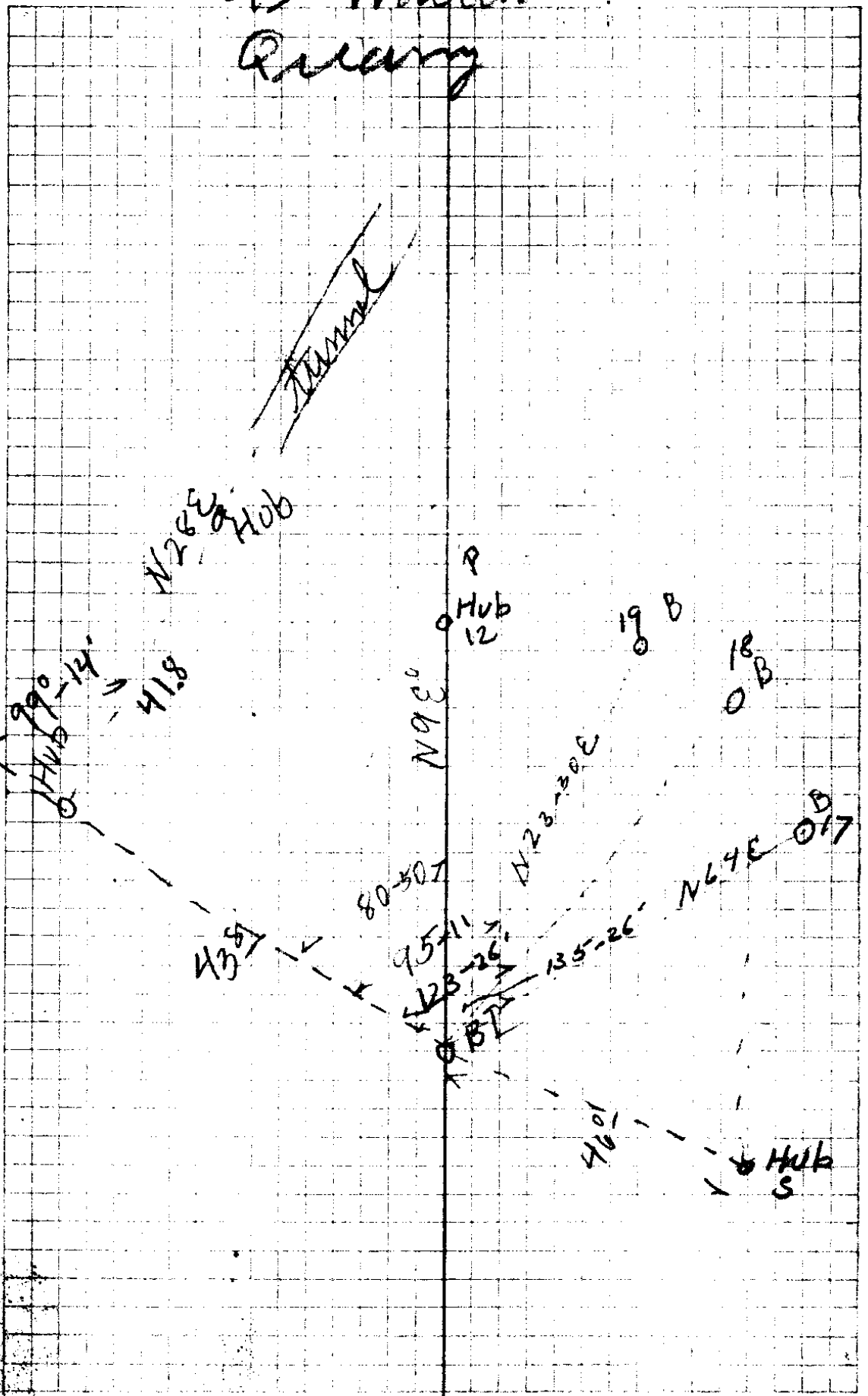


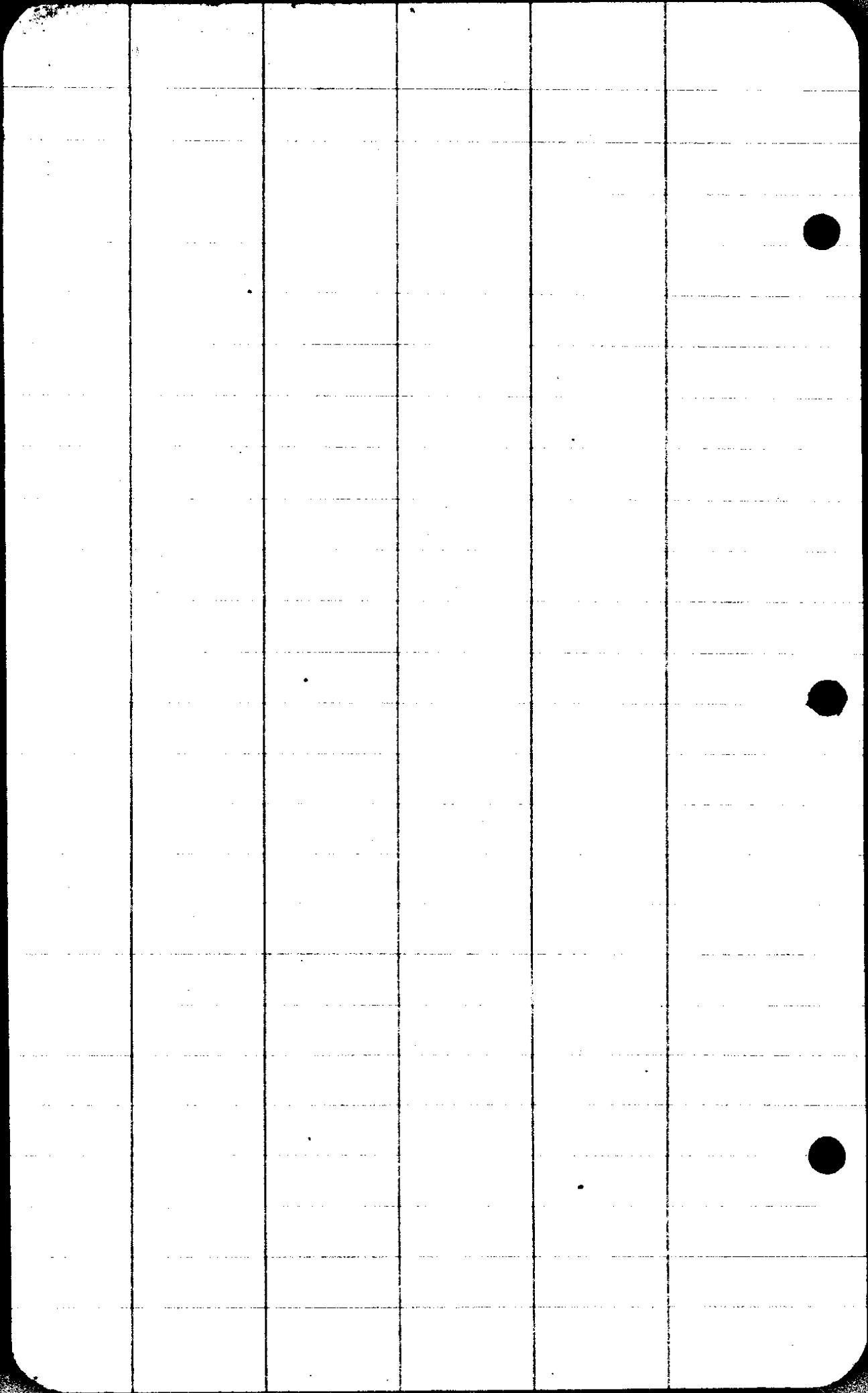
17/52

LT		E		RT	
67 ⁶	77 ⁶	78 ²	76 ⁶	73 ⁶	68 ⁰
$\frac{40+16}{100}$	$\frac{16.7}{80}$	$\frac{15}{60}$	$\frac{12}{41}$	$\frac{16.4}{20}$	$\frac{61.4}{20}$
44 ⁶	52 ¹	53 ⁶	54 ²	49 ⁶⁴	42 ⁶
$\frac{-5.0}{80}$	$\frac{+2.5}{60}$	$\frac{+4.0}{40}$	$\frac{+4.6}{20}$	$\frac{24.0}{20}$	$\frac{-7.0}{20}$
36 ²	37 ¹	38 ²	37 ¹⁴	29 ⁷	26 ⁶
$\frac{-1.0}{60}$	$\frac{9/0}{40}$	$\frac{+1.1}{20}$	$\frac{37-}{20}$	$\frac{-7.4}{20}$	$\frac{-11.5}{40}$
25 ⁴	25 ⁴	26 ¹	26 ¹⁴	18 ¹	12 ⁶
$\frac{-0.7}{60}$	$\frac{-0.7}{40}$	$\frac{0/0}{20}$	$\frac{37.00}{20}$	$\frac{-8.0}{20}$	$\frac{-13.5}{40}$
					55 ⁶
					48 ⁶
					39 ⁶
					26 ⁶
					$\frac{6.0}{40}$
					$\frac{-1.3}{60}$
					$\frac{-2.2}{80}$
					$\frac{-3.5}{100}$
					41 ⁶
					47 ¹
					33 ⁶
					$\frac{8.0}{40}$
					$\frac{-3.5}{60}$
					$\frac{-1.6}{80}$
					16 ⁹
					$\frac{-20.2}{60}$

W. Wallace
 Quinn

as Wallace Quarry





The image shows a sheet of graph paper with a grid pattern. A vertical line runs down the center of the page. On the left side, there are three circular binder holes. The grid is composed of small squares, and the entire page is mostly blank.

17/52

	Wallace			Elv.
0+00				15.0
		16.00	16.00	
17 1/2 hrs HOB.				16.50 - 0.50
T.P.	2.60	28.30	14.90	30.90
"	0.21	43.19	15.10	43.40
"	0.25	55.54	12.50	55.69
"	5.20	51.14	0.90	56.34
0+00				15.30 35.84
0+20				10.40 40.74
0+40			+	4.00 47.14
0+60	2.10	47.14	8.00	53.14
0+80	2.00	52.94	12.50	63.54
1+00	0.00	63.54	12.50	76.04
1+20	0.50	75.54	12.00	87.54
1+40	1.40	86.14	12.50	99.64
1+60	3.10	95.54	12.00	107.54
1+80	3.70	103.84	12.00	115.84
2+00	13.90	101.94	2.00	103.94
2+20	19.20	84.74	0.00	84.74
2+40	23.10	84.74	0.00	61.64
2+60	12.00	61.64	0.00	49.64
2+80	12.50	49.64	0.00	37.14
3+00	11.00	37.14	0.00	26.14
3+20	10.00	26.14	0.00	16.14
3+40	2.50	16.14	0.00	13.64