

BRITTON SURVEY

Lots 10 Block 1 - WAITS ADD to ROSEBURG
Beg @ Monument @ Benson St & Blakley St.

Set on Monument Int. Benson + Blakley St.

Back sight on Monument at Int. of Blakley

and Jackson St turned $90^{\circ}24'$ to left.

Chained North along @ Benson St. $105'$

to point on @ of Benson St. opposite

S.W. Cor. Lot 10.

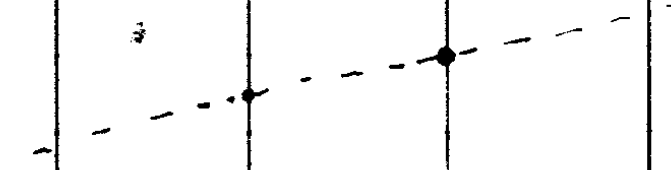
$90^{\circ}24'$

17

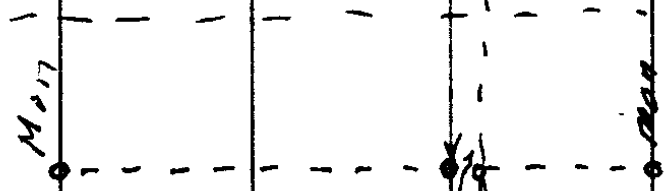
17

17

17-48



Pipe
in place
752'



M-17

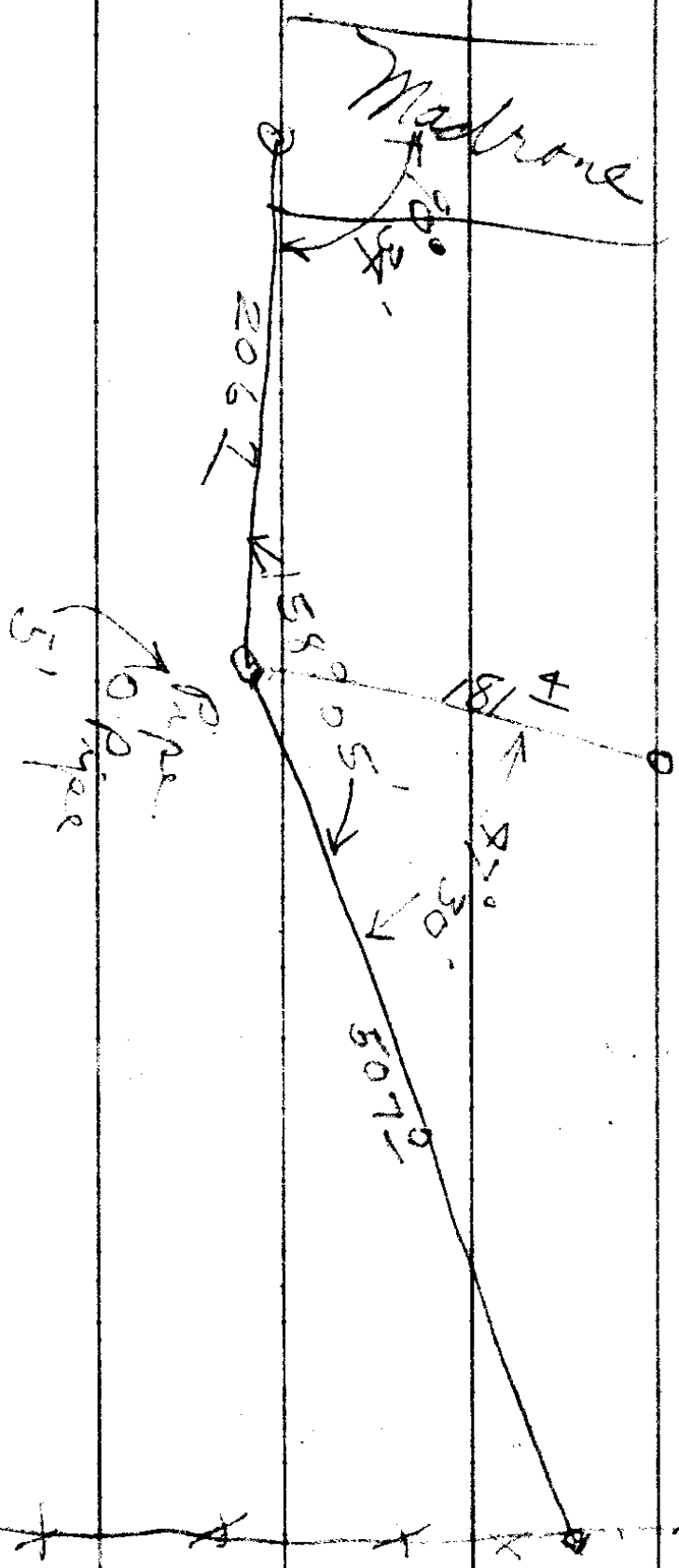
200

100

890-08'

17-48A

North



102 Hub on W. Bridg

101
II

• Pipe C 100

• Pipe B

• Pipe A
Snyders
Lot

↕ Riverside

17-1039

BIW
F.S. Cou Camb $349^{\circ} 49' 30''$ 748.95

$54^{\circ} 02' 00'' E$

π 103 $159^{\circ} 39'$

B.S. 102 $349^{\circ} 49'$

$N 6^{\circ} 08' 30'' E$

Iron
Pipe $337^{\circ} 53'$ 160.45

$S 15^{\circ} 58' 30'' E$

π 103 $315^{\circ} 46'$

B.S. 102 $337^{\circ} 52'$

F.S. 103 $273^{\circ} 42' 30''$ 262.7

$S 6^{\circ} 08' 30'' W$

π 102 $187^{\circ} 25'$

B.S. Pipe C $273^{\circ} 42'$

$N 57^{\circ} 34'' W$

~~F.S. ^{Watta}~~

~~F.S. 103~~

~~π 102~~

~~B.S. Pipe C $87^{\circ} 19'$~~

~~200.02~~

F.S. 102

$0^{\circ} 00'$

67.4

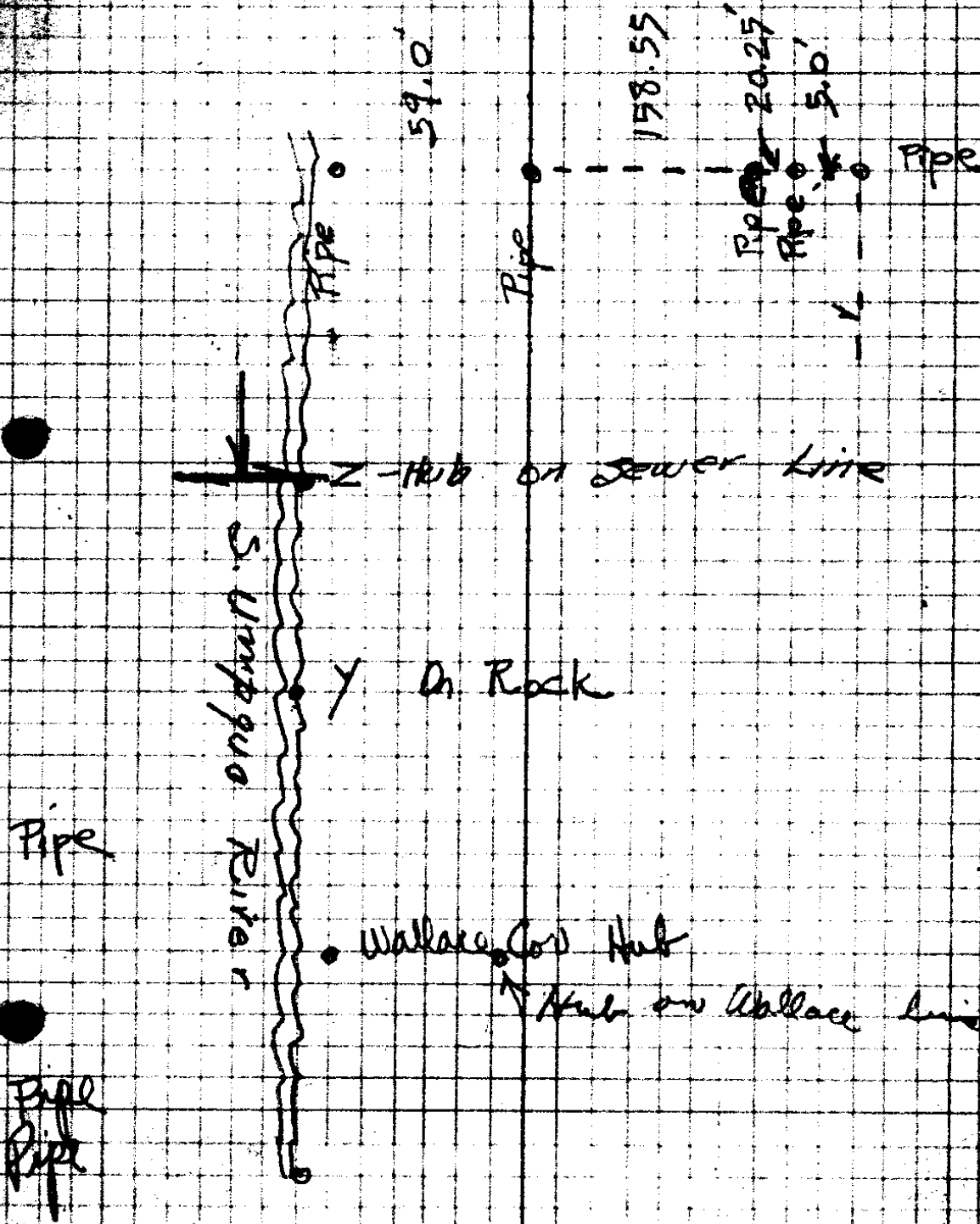
A Pipe C

B.S. Pipe A

All Angles are
Deflection to the Right

Bowler
Wolford
Dillon

Manu



17-460

F.S. 101 270° 30.0'

T Pipe C

B.S. Pipe A

F.S. 100 90° 20.0'

T Pipe C

B.S. Pipe A

F.S. ^{Grav} ~~Co~~ 255° 03'

T ^{Ch Riv} ~~Wallace~~ 150° 06'

B.S. ^{SE} ~~Co~~ 255° 03'

51604-1500

R Riverside 300° 23' 15" 277.6

558-588

Wallace
T SE Co 240° 46' 30"

B.S. ^{Wallace} ~~Co~~ 300° 23'

Wallace
F.S. ^{SE} ~~Co~~ 0° 31' 173.95

50° 39' 00"

T ^{Wallace} ~~Co~~ 1° 14'

B.S. ^{Wallace} ~~M.P.~~ 0° 37'

50° 02' 00"

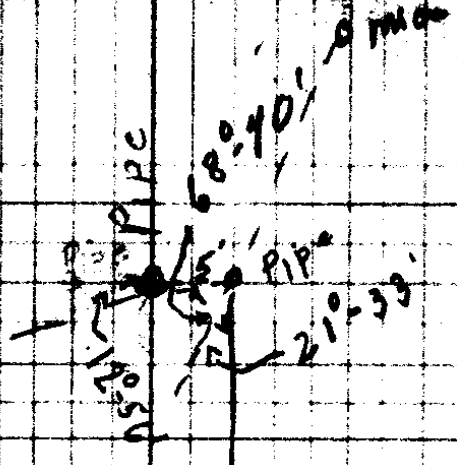
Wallace
F.S. ^{M.P.} ~~Co~~ 19° 46' 30" 68.15

T ^{Wallace} ~~Co~~ 39° 33'

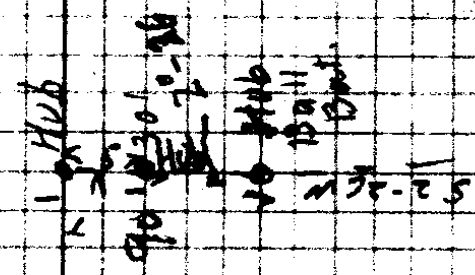
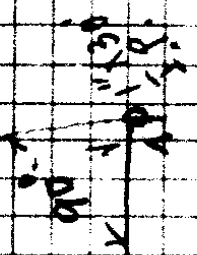
B.S. ^{Wallace} ~~Co~~ 19° 46'

⁵⁰²
~~576-926~~
K79-0744

Pipe Snider



N 87° 34' W



21720
118

200

17-40

DIST. *

On Wallaw
F.S. line 259° 09'
Wallaw
T. Cor 158° 18'
ES. Y 259° 09'

50° 02W
~~52° 20W~~

Wallaw
F.S. Cor 325° 25' 124.25
T Y 290° 50'
Z 325° 24'

N79-07W
~~N75-33W~~

F.S. Y 19° 20' 30" 109.0
T Z 38° 41'
B.S. Syd Cr 19° 21'

N49-32W
~~N40-58W~~

F.S. Z 280° 04' 118.8
T Syd Cr 200° 08'
B.S. Syd Cr 280° 03'

~~N63-53W~~
~~N60-18W~~

F.S. Syd Cr 100° 59.0
K. Syd Cr
B.S. & Pir.

N16-03E
~~N15-3730E~~

F.S. Syd Cr 81° 29' 30" 183.80
T & Kives 162° 59'
B.S. Mon 81° 29'

N16-03E
~~N15-3730E~~

~~N65-52W~~
~~N65-76W~~

17-40A

Mon

500.6

306.67N

890.20

206.6

SP

890.20

506.18

910.47
118

291.6

10-32 R

Handwritten notes and scribbles in the top right corner, including the number "1112" and some illegible characters.

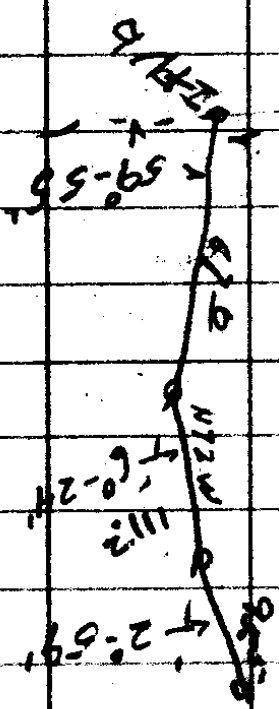
CHANDLER
B.P.O.F.

CLASS
1852

Handwritten notes and scribbles in the bottom right corner, including the number "1112" and some illegible characters.

2415

17-48



174
 75
 944
 687

Mollace

Fince Post Bagged

Fince Post Bagged

Willy Survey

Δ 3

3.51

Δ 2

4.00

Δ 1

2.99

SW
Cov 1/3

S 89-30E

East 589-58E

89-30T used from line
ahead. N 8-35E

on
Cov 1/2

12

8-17

N 7-30W N 8-25W

Δ 7

10.12
10-15' 151'

N 3W N 0-02E

Δ 6

3.92

1-26

N 1° 30E N 1-53E

Δ 5

17.35

on
Δ 4

8.83

464

1° Nt.

N 0-23E N 0-27E

Δ 23.97

1.66

Δ 1

231

North N-0-33W

Cov
H 1

15.99

10 + 14.2

Cross Beginning 90 + 00

End of 9 + 10

End of 8 + 20.3

7 + 50.3

End of BV

50° - 19'

Fit top Brake out.

Rock

SLOPE
34%

Beginning

17 + 00

Handwritten notes and scribbles at the bottom left.

Young

Sta Dist LA RA M, C,

$\Delta 11$
17-30 420 782

$\Delta 10$
17-30 436 416

$\Delta 9$
3406

$\Delta 8$
12-30 95 922

$\Delta 7$
34-30 2262 1864

$\Delta 6$
155

$\Delta 5$
230 592 550

$\Delta 4$
120 1469 1378

$\Delta 3$
230 404 372

$\Delta 2$
13-30 1960 1906

$\Delta 1$
293 43 lbs

West

row
T 29 30 S - R 10 W

off set 5' North

300⁰⁰ 42⁰⁰

off set 5 Back, on line

5' off set South

Found old B.T. & Stone

1/4 Cov.

122⁹

Δ 20

19⁰ 165³

156³

Δ 19

14⁻³⁰ 109⁶

103⁹

Δ 18

04³⁰ 185⁵

184⁹

2256²

04⁻³⁰ Δ 17

149²

149²

13⁰ Δ 16

167²

163⁴

01⁻⁴⁵ Δ 15

129⁶

129⁵

-5⁰ Δ 14

177⁰

176³

3⁰ Δ 13

188³

188⁰

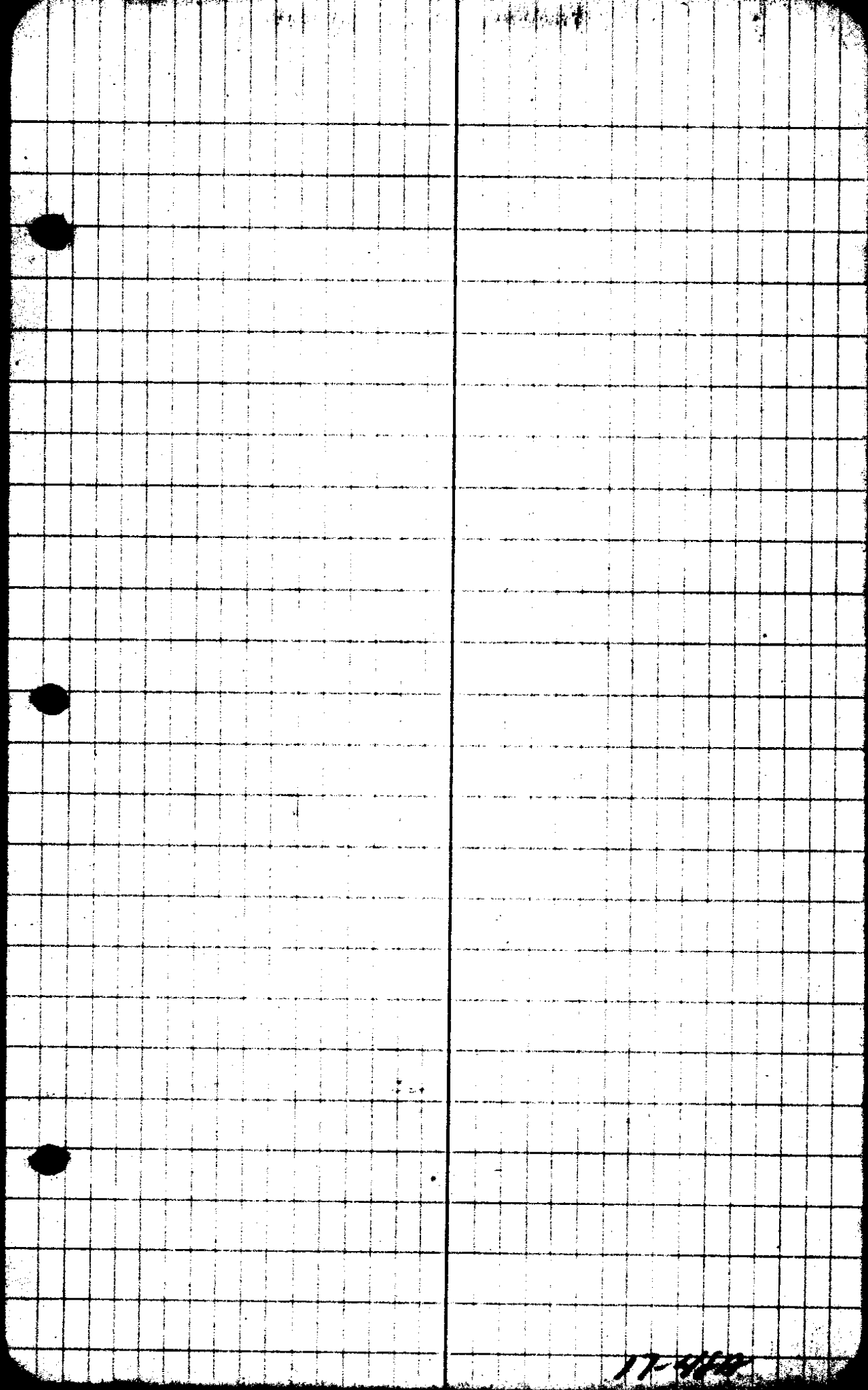
Δ 12

53⁷

Δ 11

Edd Walker.
Whipple

17-108



17-900

sta

LA

Cor Oakton House

135²

117°-03'

N19W N18-47W

Δ 2

1494

17-50

382 E 58 1° 44E

Δ 1

407

70-59

N80 E N80-26E

Δ TK

Back right Δ 6

Δ 6

214
9'

213⁵

129-15

#

54-30W 54-35W

NW Cor

267

50-45

N46-45W N46-10W

N.E. Cor.

77⁴

Δ 5

118¹

30
Δ 4

80³

Δ 3

197.8

2 Δ

52²

N40-30E N40-35E

Δ 1
0+00

Mbr.

60° 60°

var. walk 6.5

15° SIDEWALK
10°

91°

91° OAK

66°

25

12

25

16

curb wall

Breasing

16.3
11.3

77° 76°

DRIVEWAY

sidewalk

ROSE

07421

91°

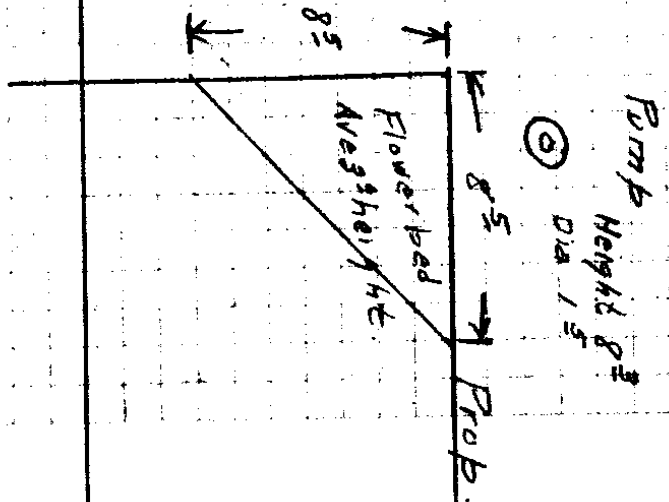
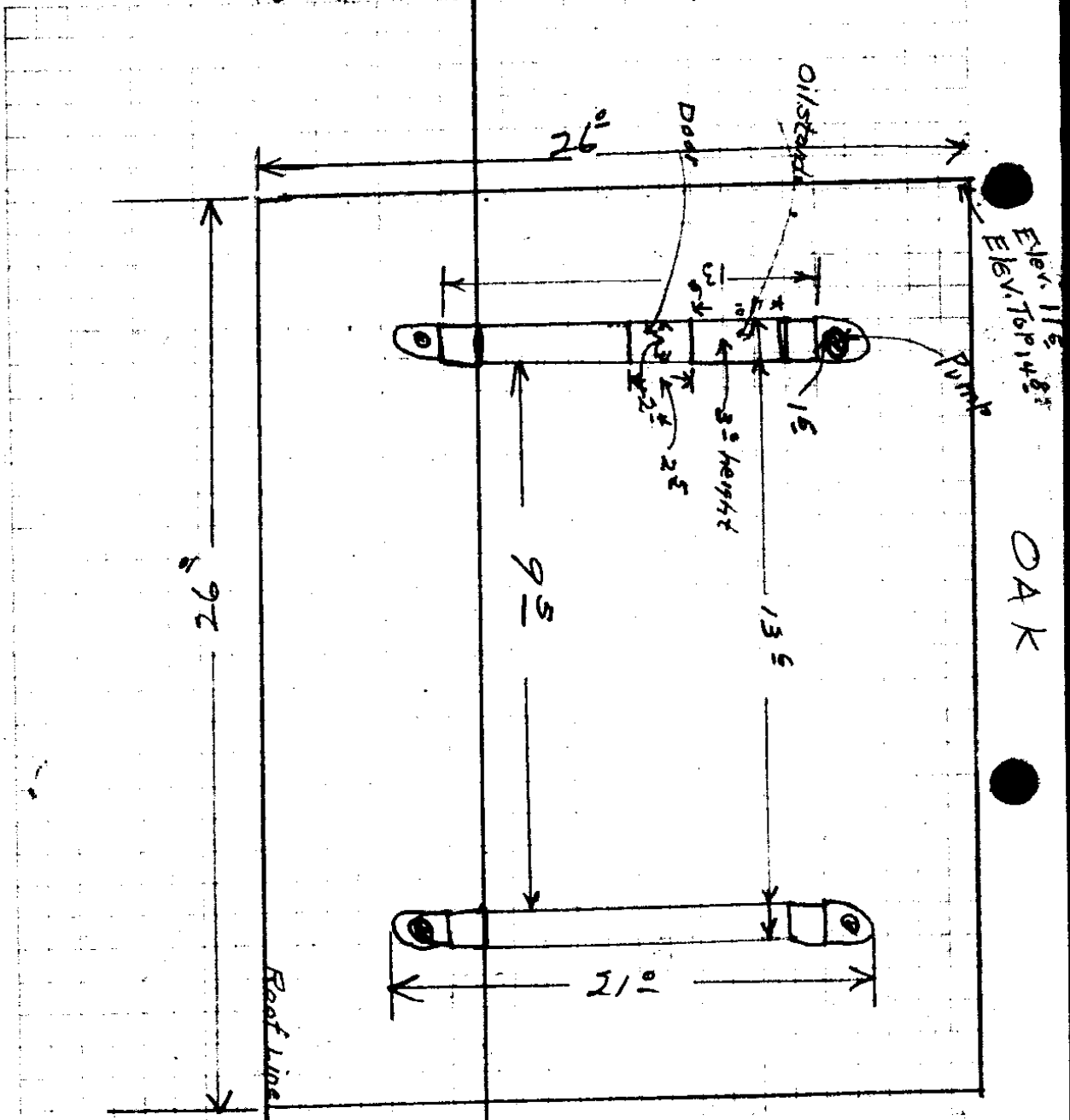
Bldg Stalls

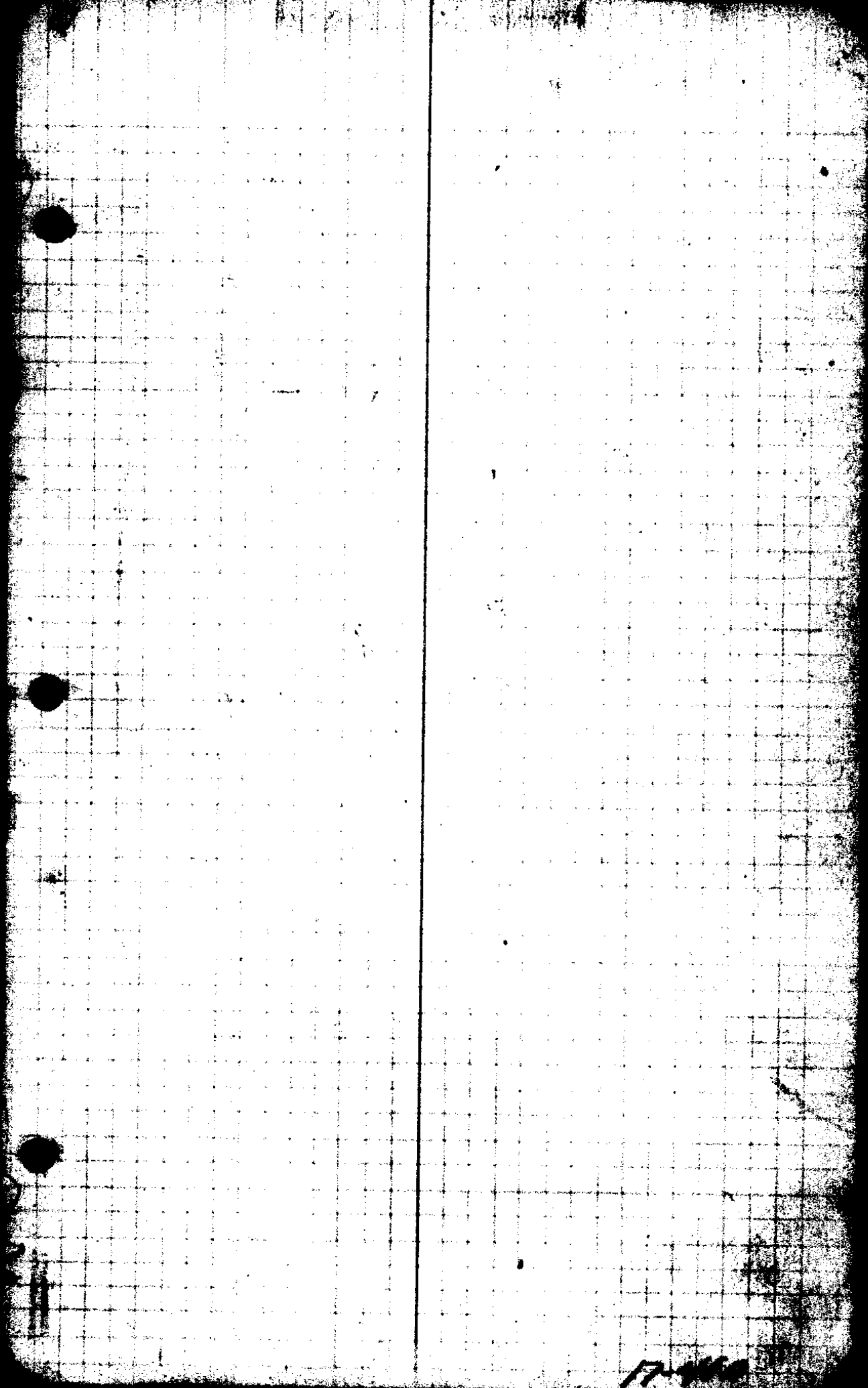
150°

63°

Rose

26° ft square





SE. Cor U
37

Full Meter give A ch. dist

56' +25°30' L56°57' N32°E
↓

189° +12°45' R90°

7.7

R90°

82.6 +7°15'

63.9 +22°

69° +30°

L90°

6.4 -

R90°

45.9 33°50'

64° +36°

465 +33°10'

East

SW 62 31

Bet. 15/16 South

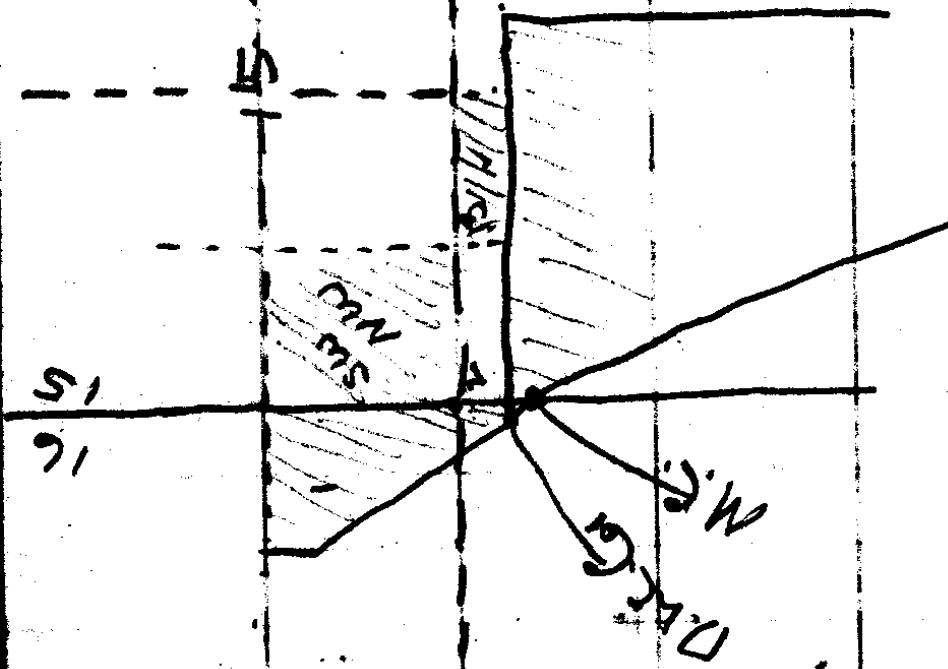
~~40 ch. 1/2~~

.5 - Stream 2 lks - CME
10.0 Ridge E & W
20.0 Enter bottom
40.0 1/4 Post
6" Willow N 18° W 5 lks
5" Spruce N 75° E 5 lks
46.75 Right bank of River
5" Willow N 3° W 30 lks
7" " N 2° E 30 lks

Sect. 9-10-15-16

18" alder	89 E	35 lks
24" "	317 1/2 W	15 "
20" "	N 87 W	48 "
36" Fir	N 32 E	19 "

lot 2 Out.



π

B.M.

476.85

5.2

482.05

1

6.0

476.05

101

5.5

476.55

102

4.9

477.15

103

4.5

477.55

104

3.9

478.15

105

3.3

478.75

106

2.9

479.15

2

8.6

471.45

202

8.1

473.95

3

12.0

470.05

203

9.5

472.55

T.P.

11.60

470.45

2.00

472.45

4

5.9

466.55

204

2.8

469.65

5

9.3

463.15

205

6.0

466.45

T.P.

11.15

461.30

1.8

463.10

6

3.4

459.75

206

0.4

462.20

7

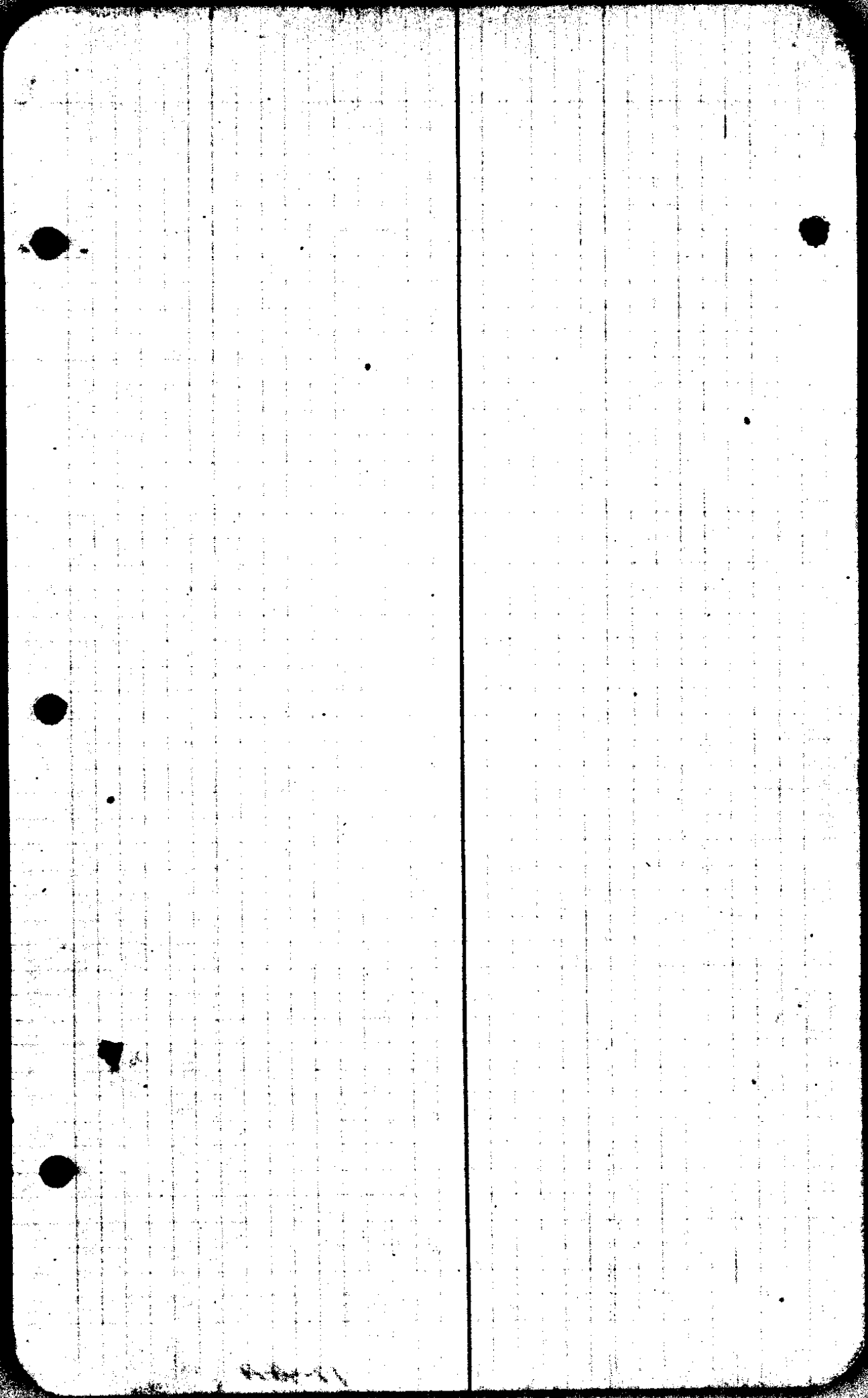
6.9

456.20

207

4.3

458.50



23

17-11-10

sta	+	T	-	R	Elev
		110.60			
57				5.51	
+50				5.63	
58+00				5.76	
+50				5.88	
59				6.01	
+50				6.13	
T.P.	3.01	107.48	6.13		104.47
60+00				3.14	
+50				3.20	
61+00				3.32	
+50				3.51	
62+00				3.67	
+50				3.76	
63+00				3.87	
+50				4.01	
T.P.	3.27	108.64	4.01		103.37
64+00				5.40	
+50				5.52	
65+00				5.65	
+50				5.77	
66				5.90	
+50				6.02	
T.P.	1.33	109.95	6.02		102.62

17-409

Stac	+	A	-	R	
	7.93	109.95			
67+00				7.76	
+50				4.58	
68				7.71	
				7.83	
				4.42	
				4.36	
				1.57	

$$\begin{array}{r}
 26542 \\
 89175 \\
 \hline
 4356 \overline{) 110717} \quad 2,54 \\
 \underline{8712} \\
 23597 \\
 \underline{21780} \\
 18170
 \end{array}$$

H W Fppstein
Edwin Weaver
F. I. Weaver
W.S. Crear.
Clara Fields

Act by corner
between Sec 17-18-T30S R5 W
From old B.T. which contained
a white mark but had indication
of old B.T. other tree gone
but stump in place.

Edwin Weaver claim it's
his as he ^{had} been before
set Ford axle for corner
marked

W. Oak 16" BV569 E 32⁷ feet
W oak 7" diam BV542 W 23⁵ "

Recorded Vol. 1 Page 183
Jan. 26/25. W.S.

17-489

4022
 1344
 2682

85
 5
 4.25

27.4
 4.25
 23.15

524
 4616
 624
 310
 183
 147

50-25

359
 249
 110-59
 01

N 46-10 W
 110
 11

S 23, 44 W

N 23, 49 E
 89
 35
 66
 11

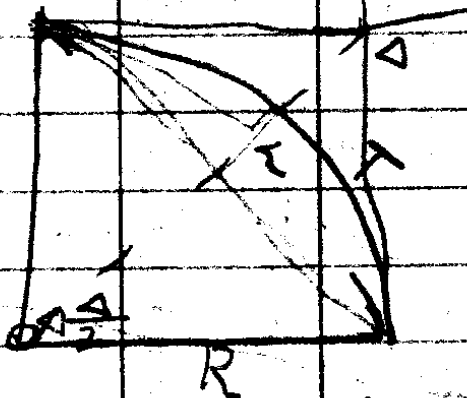
179
 66
 113

179
 68
 111-51

15

103
 90
 130
 120

10
 105



$$\tan \frac{\Delta}{2} = \frac{T}{R}$$

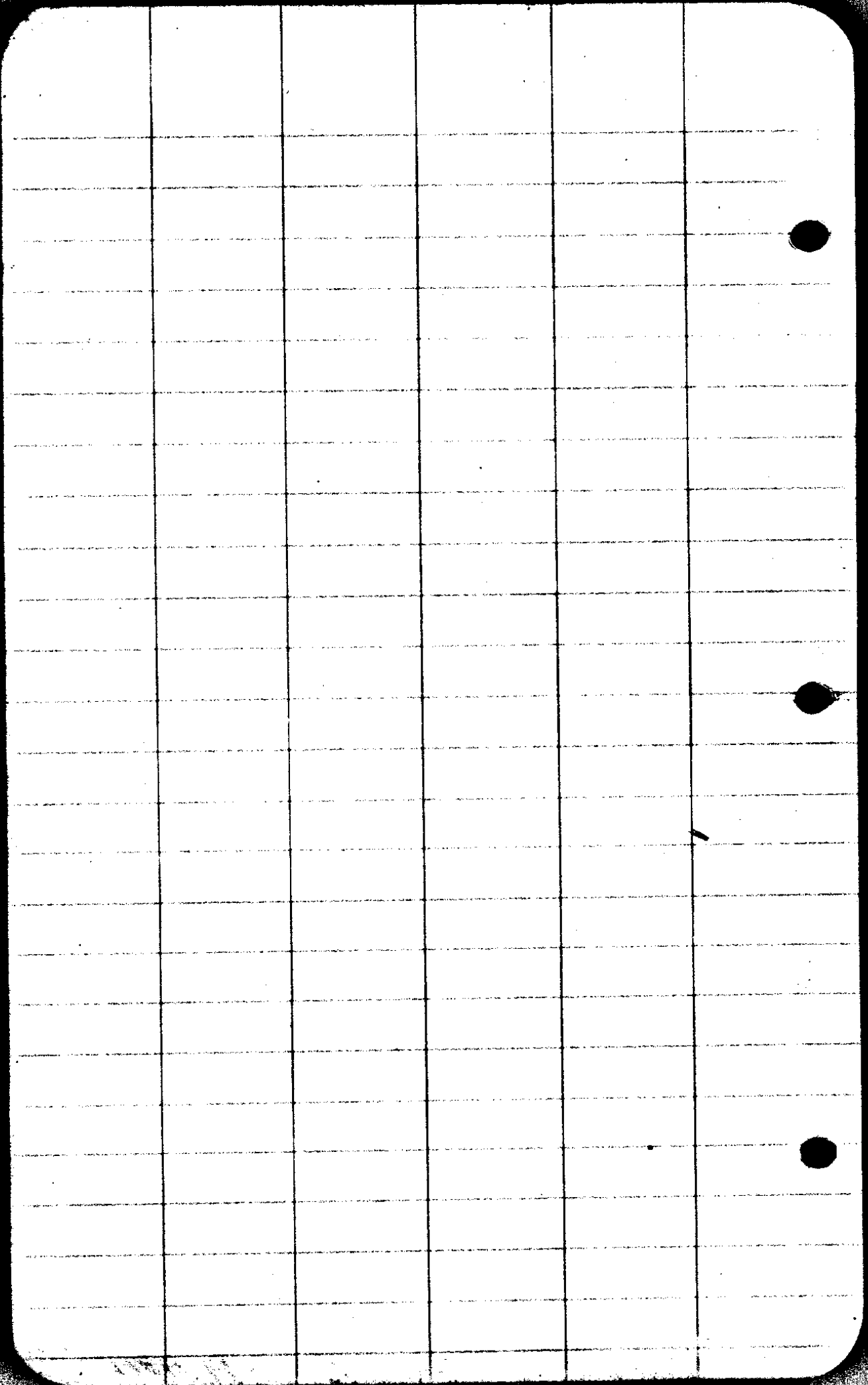
$$R = \frac{5730}{\text{Degree of Curve}}$$

$$L = 100 \frac{\Delta}{\text{Degree of Curve}}$$

1 foot of curve = 100/1.03

North line

95 44.6 Feet
south of point for
 $\frac{1}{2}$ distance



Not by Pine

11th week

+ 10

+

+ 20

+ 10

+ 8

France

+00

2699

Δ1

1084

Δ2

987

Δ3

2675

Δ4

1345

Δ5

2020

Δ6

149

300
288

Δ7

98-48 N81-30W N81-12W

1156

Δ8

N87-32W N87-32W

798

Δ9

N85-20 N85-23W

79

1695

Δ10

N84 W N83-43W

1-40

745

Δ11

N85-30W N86-02W

2019

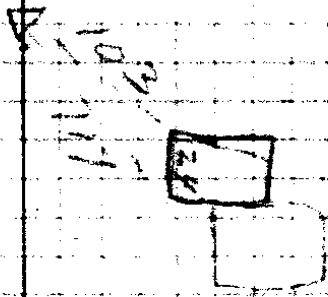
1002

Δ12

Δ13

17/21

Outline of James



A sheet of graph paper with a grid of 10 columns and 20 rows. Three binder holes are punched along the left edge. The paper is otherwise blank.

17-460

0° 53'

~~178 33~~
88 53
310 00

300 00
88 53

Down on St I 595 by hand

Con on Douglas St

N 10° 15' W

100° 00'
16° 45'

T.F.

Face pillar North side

S 11° 55' W

18 35

T.F. with 104° 20' R

STK

N 88° 2' E N 87° 35' E

81° 00'

87° 42' R

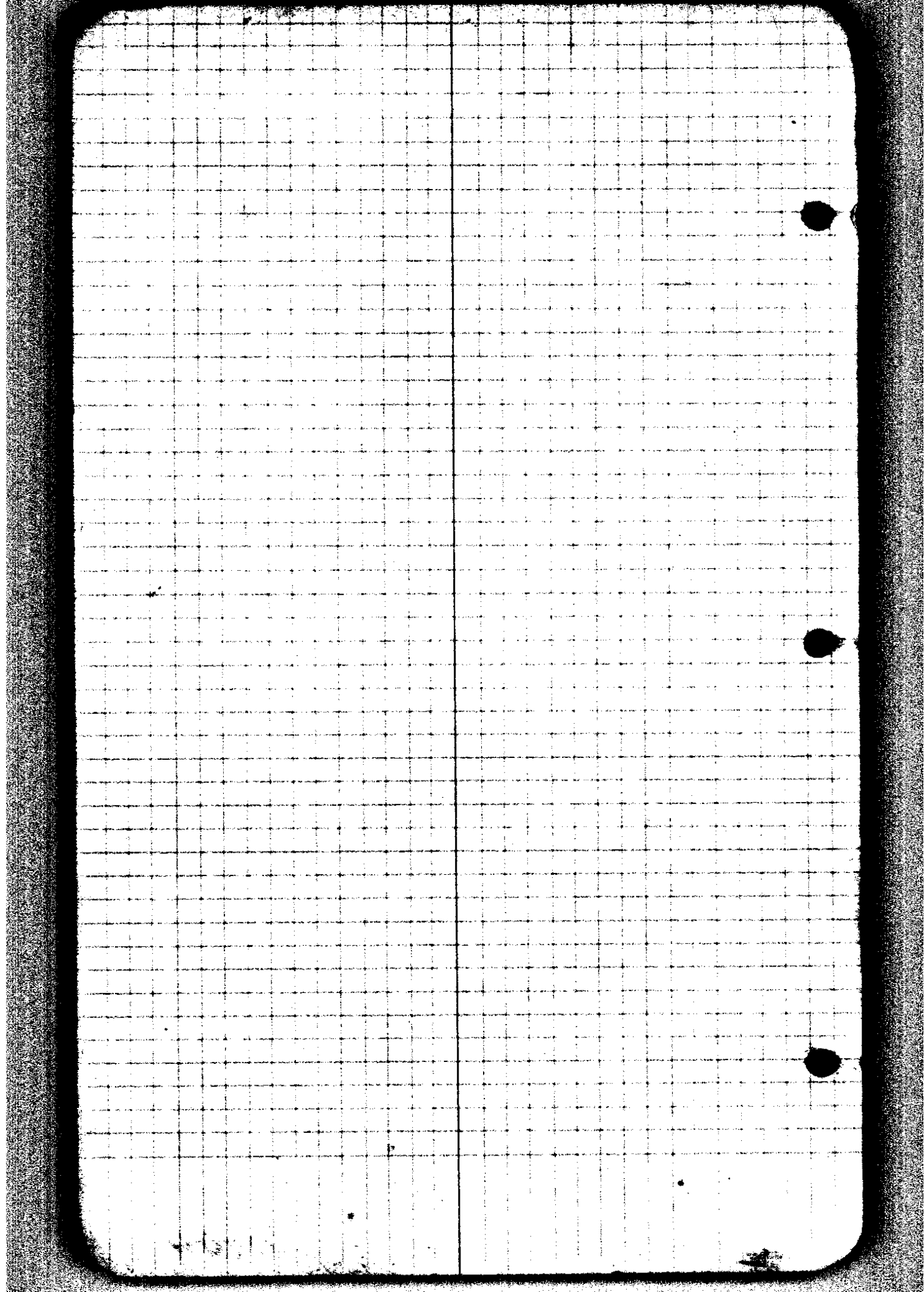
STK

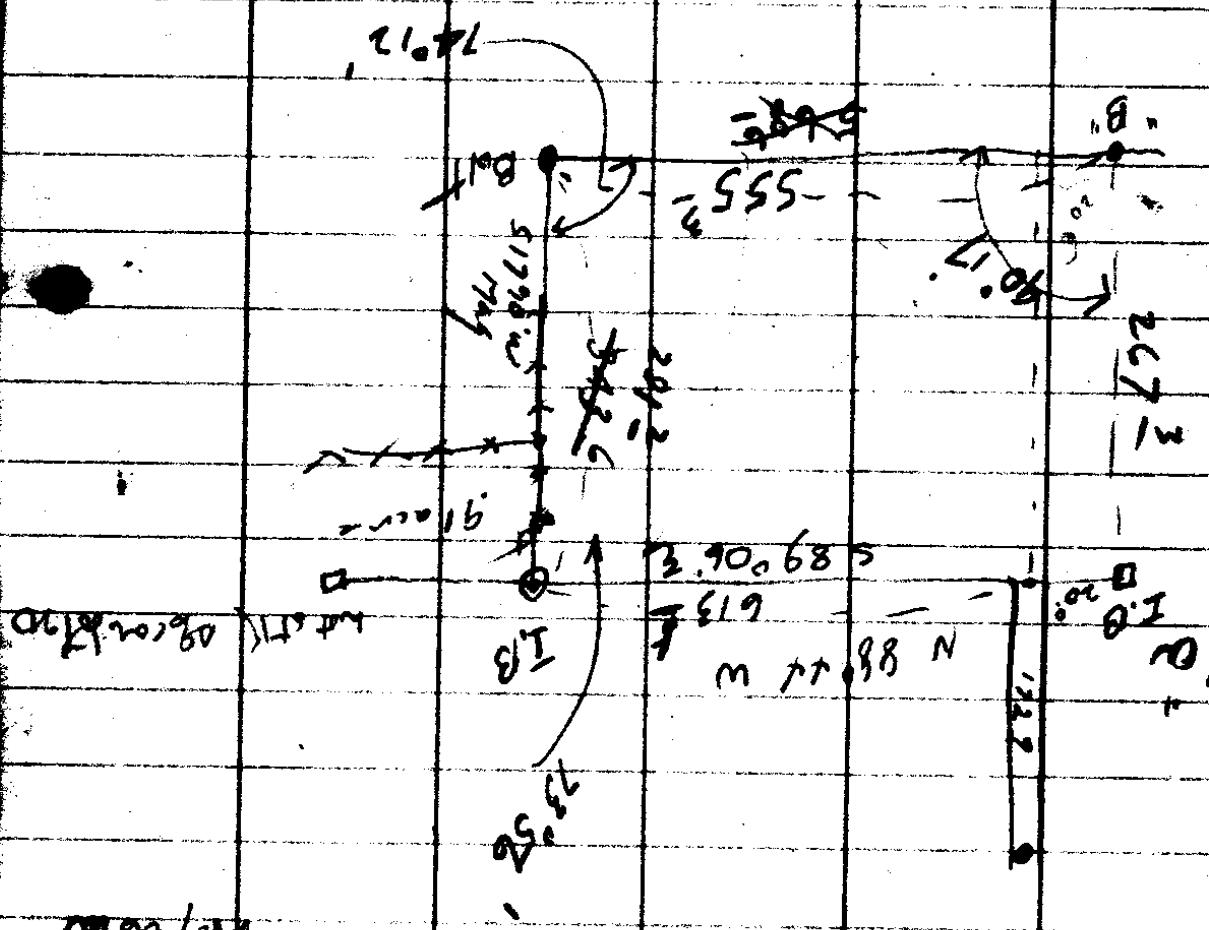
N 00° 7' W

15 39

0°

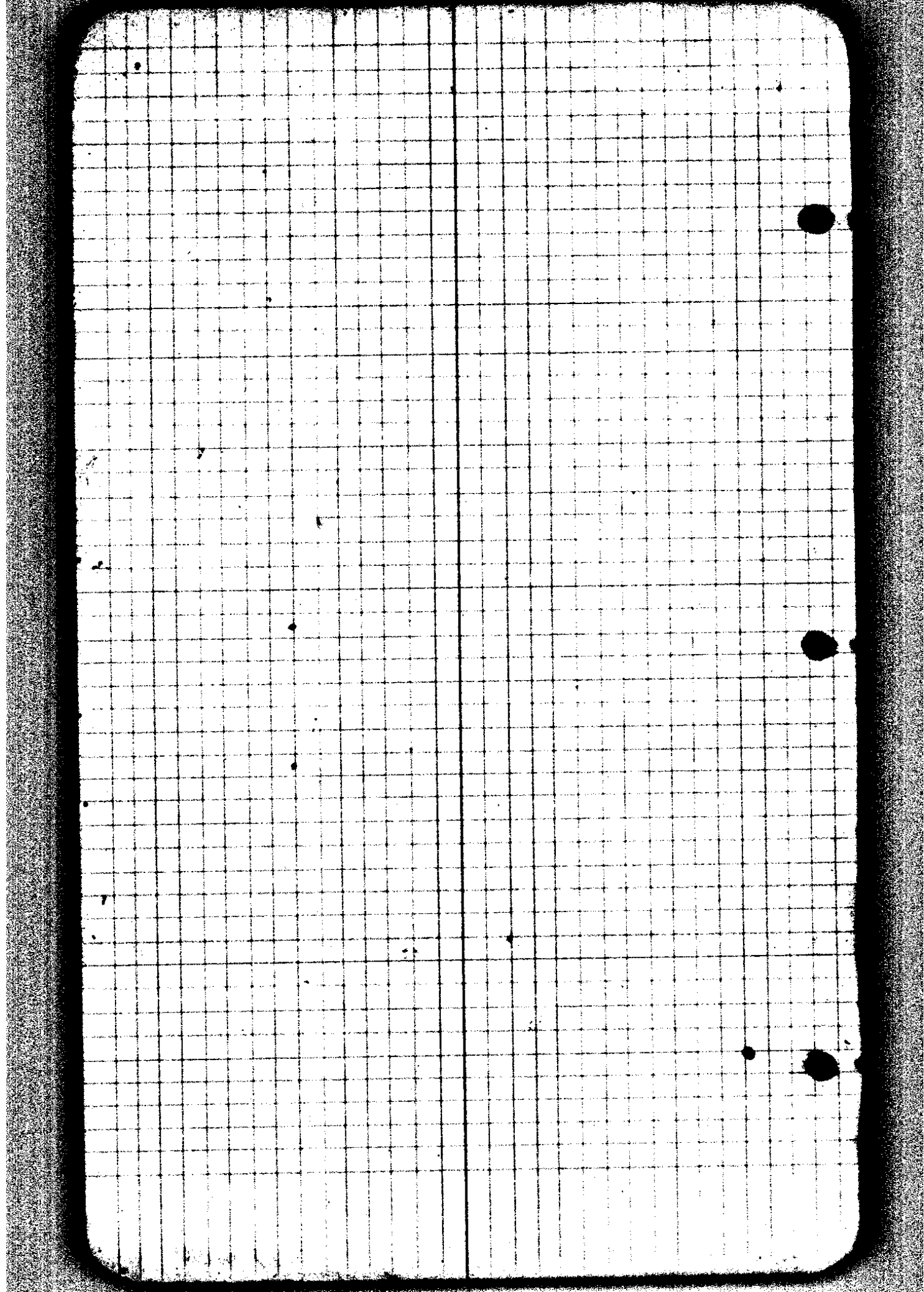
T.P.





ST 8720
 Roscoe Green
 17-11
 3436
 6272
 28
 52
 135
 358

189°06'00"



17-489

Harry Booth

0700	20.4
0760	20.1
1700	19.4
1740	19.1
2700	18.5

5026

195
240

435

17-46A

70° 00"	74.6	8"
69° 25'	85.5	6"
71° 00'	89.5	20" ✓
74° 12"	35.3	15" ✓
73° 15'	27.9	15" ✓
80° 00"	18.4	15" ✓
82° 10"	13.0	20" ✓
94° 00'	24.5	10" ✓
94° 00"	28.0	8" ✓
95° 30"	39.6	10" ✓
82° 45"	67.4	12" ✓
78° 30'	83.0	10" ✓
76° 45'	83.5	20" ✓

17-48A

3+25						
$\frac{3.8}{0}$	$\frac{4.0}{25}$	$\frac{3.8}{50}$	$\frac{3.7}{75}$	$\frac{3.8}{100}$	$\frac{3.5}{125}$	$\frac{3.6}{128.2}$
446.15	445.95	446.15	446.25	446.15	446.45	446.35
48						
3+50						
$\frac{3.5}{0}$	$\frac{4.3}{25}$	$\frac{4.0}{50}$	$\frac{3.9}{75}$	$\frac{4.0}{100}$	$\frac{4.7}{125}$	$\frac{4.4}{129.0}$
(25 ft) 446.45	445.65	445.95	446.05	445.95	445.75	445.55
No. of Boundary						
$\frac{3.5}{0}$	$\frac{4.5}{25}$	$\frac{4.5}{50}$	$\frac{4.6}{75}$	$\frac{4.7}{100}$	$\frac{4.6}{125}$	$\frac{4.8}{129.8}$
446.45	445.45	445.45	445.35	445.25	445.35	445.15

Chapman St. to S.W. Cor. of H.S. prop. 285.2 ft

Angle	Dist.	Size
	42.3	8"
So. Line	37.6	15"
7° 22" R	27.2	10"
26° 41" "	57.4	24"
29° 13" "	90.3	36"
44° 45" "	106.0	30"
42° 00" "	24.9	8"
	60.9	15"
52° 40" "	57.9	6" ✓
59° 00" "	60.0	15" ✓
59° 00" "	91.0	24"
63° 22" "	78.0	8"
66° 35" "	54.7	24"

129

17-10-19

449.95 ✓

1+2.5

$\frac{4.9}{0}$	$\frac{5.0}{25}$	$\frac{4.7}{50}$	$\frac{4.9}{75}$	$\frac{5.2}{100}$	$\frac{5.5}{117.1}$
-----------------	------------------	------------------	------------------	-------------------	---------------------

445.02 444.95 445.25 445.05 444.75 444.45

1+50

$\frac{5.1}{0}$	$\frac{5.0}{25}$	$\frac{4.7}{50}$	$\frac{5.0}{75}$	$\frac{4.7}{100}$	$\frac{4.9}{118.5}$
-----------------	------------------	------------------	------------------	-------------------	---------------------

444.75 444.95 445.25 444.95 445.25 445.05

1+75

$\frac{5.2}{0}$	$\frac{5.2}{25}$	$\frac{5.0}{50}$	$\frac{4.7}{75}$	$\frac{4.8}{100}$	$\frac{5.0}{118.7}$
-----------------	------------------	------------------	------------------	-------------------	---------------------

444.75 444.75 444.95 445.25 445.15 444.95

2+00

$\frac{5.2}{0}$	$\frac{4.9}{25}$	$\frac{4.7}{50}$	$\frac{4.5}{75}$	$\frac{4.5}{100}$	$\frac{4.7}{119.9}$
-----------------	------------------	------------------	------------------	-------------------	---------------------

444.75 445.05 445.25 445.45 445.45 445.25

2+25

$\frac{4.4}{0}$	$\frac{4.4}{25}$	$\frac{4.6}{50}$	$\frac{4.4}{75}$	$\frac{4.6}{100}$	$\frac{4.2}{121.5}$
-----------------	------------------	------------------	------------------	-------------------	---------------------

445.55 445.55 446.35 445.55 445.35 445.75

2+50

$\frac{3.3}{0}$	$\frac{3.8}{25}$	$\frac{4.0}{50}$	$\frac{3.8}{75}$	$\frac{3.9}{100}$	$\frac{4.1}{123.6}$
-----------------	------------------	------------------	------------------	-------------------	---------------------

446.65 446.15 445.95 446.15 446.05 445.85

2+75

$\frac{3.4}{0}$	$\frac{3.2}{25}$	$\frac{3.4}{50}$	$\frac{4.0}{75}$	$\frac{3.4}{100}$	$\frac{3.8}{125}$
-----------------	------------------	------------------	------------------	-------------------	-------------------

446.55 446.75 446.55 445.95 446.55 446.15

3+00

$\frac{3.9}{0}$	$\frac{3.8}{25}$	$\frac{3.5}{50}$	$\frac{4.0}{75}$	$\frac{4.0}{100}$	$\frac{3.8}{125}$	$\frac{3.8}{126.1}$
-----------------	------------------	------------------	------------------	-------------------	-------------------	---------------------

446.05 446.15 446.45 445.95 445.95 446.15 446.15

17-400

Sta	+	π	-	Rod	City Bench Elev.
	3.55	453.09			449.54
			2.84		450.25
	2.25	452.50			
			7.68		444.82
	5.70	450.52			

-0425					
$\frac{7.5}{0}$	$\frac{5.3}{25}$	$\frac{5.0}{50}$	$\frac{3.7}{75}$	$\frac{1.5}{100}$	$\frac{1.0}{110.4}$
443.02	445.02	445.52	446.82	449.02	449.52
0+00	$\frac{5.1}{0}$	$\frac{8.4}{25}$	$\frac{8.2}{50}$	$\frac{7.2}{75}$	$\frac{6.5}{100}$
					117.0
	442.82	442.12	442.32	443.32	444.02
					444.52

0+25					
$\frac{7.2}{0}$	$\frac{7.6}{25}$	$\frac{7.7}{50}$	$\frac{8.0}{75}$	$\frac{7.8}{100}$	$\frac{7.7}{112.8}$
443.32	442.92	443.32	442.52	442.78	442.82

0+50					
$\frac{6.5}{0}$	$\frac{6.4}{25}$	$\frac{6.6}{50}$	$\frac{6.9}{75}$	$\frac{7.5}{100}$	$\frac{7.2}{114.2}$
444.02	444.12	443.92	443.62	443.02	443.12

0+75					
$\frac{6.4}{0}$	$\frac{5.7}{25}$	$\frac{6.1}{50}$	$\frac{6.1}{75}$	$\frac{6.1}{100}$	$\frac{6.2}{115.3}$
444.12	444.82	444.42	444.42	444.42	444.32

1+00					
$\frac{5.9}{0}$	$\frac{5.6}{25}$	$\frac{5.8}{50}$	$\frac{5.9}{75}$	$\frac{5.8}{100}$	$\frac{6.1}{115.3}$
444.62	444.92	444.72	444.62	444.72	444.42

T.P. 5.84 444.68

5.27 449.95

B.M.

17-488

509.77

1420

$\frac{2.4}{650}$	$\frac{4.4}{40}$	$\frac{5.4}{30}$	$\frac{6.1}{20}$	$\frac{7.6}{0}$	$\frac{8.6}{20}$	$\frac{8.7}{30}$	$\frac{8.4}{40}$
507.37	505.37	504.37	503.67	502.17	501.17	501.09	501.37

8.60 501.17

3.89

505.06

265 Δ

510.12

1440

$\frac{2.8}{60}$	$\frac{4.6}{40}$	$\frac{6.3}{30}$	$\frac{1.8}{20}$	$\frac{4.5}{0}$	$\frac{6.5}{20}$	$\frac{6.7}{30}$	$\frac{7.1}{40}$
507.32	505.52	503.82	502.26	500.58	498.56	498.36	497.96

$\frac{2.6}{60}$	$\frac{5.0}{40}$	$\frac{6.2}{30}$	$\frac{3.0}{20}$	1460	$\frac{8.1}{20}$	$\frac{9.1}{30}$	$\frac{9.3}{40}$
507.52	505.12	503.92	502.86	499.46	496.66	495.96	495.76

$\frac{4.3}{60}$	$\frac{7.6}{40}$	$\frac{1.6}{30}$	$\frac{3.1}{20}$	1480	$\frac{10.9}{200}$	$\frac{12.2}{30}$	$\frac{12.9}{400}$
508.47	505.17	503.46	501.96	498.16	494.16	492.86	492.16

$\frac{4.5}{60}$	$\frac{7.5}{40}$	$\frac{2.8}{30}$	$\frac{5.3}{20}$	2400	$\frac{13.5}{20}$	$\frac{15.2}{30}$	$\frac{16.5}{40}$
508.27	505.27	502.26	499.76	498.16	491.56	489.86	488.56

11.74

512.79

4.03 501.09

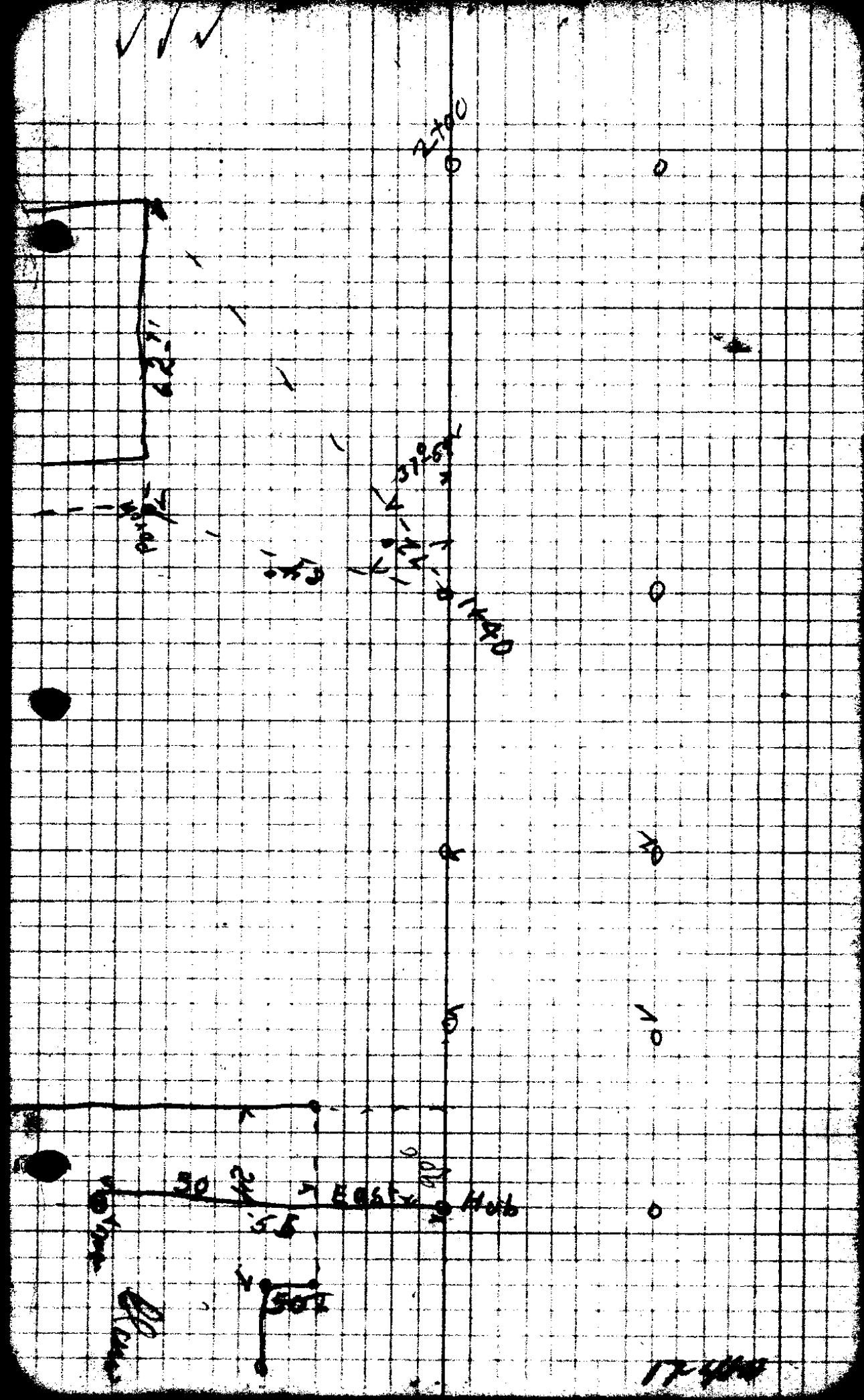
~~1.51~~

509.82

4.46 508.31

7.17

502.65



+ ∇
 1191 5/4.51 502.60

Sta. 0 → 12

12.56 ^{without curb} 11.91 9.87 5.5 2.7 0.9
~~85~~ ~~87~~ ~~93~~ ~~25~~ ~~19~~ ~~C~~ ~~78~~
 501.95 502.60 504.02 504.64 509.01 512.81 513.61

0+00

12.21 10.91 9.9 4.1 1.6
~~750~~ ~~500~~ ~~257~~ ~~C~~ ~~190~~
 502.30 503.60 504.61 510.41 512.91

0+12 ^{June}

12.93 12.56 11.13 9.75 4.4 4.2 2.9 1.2
~~84.6~~ ~~76.5~~ ~~50.~~ ~~25.~~ ~~C~~ ~~20.0~~ ~~30~~ ~~40.~~
 501.58 501.95 503.38 504.76 510.11 512.21 513.51 515.21
 11.89 9.82 7.95 0+22 5.65 5.0 3.3
~~75~~ ~~30.~~ ~~25~~ ~~282~~ ~~30.~~ ~~40.~~
 502.62 504.19 506.54 510.76 511.41 513.11

5.75 516.41 ✓ 3.85 510.66 ✓

2.6 0+40 6.5 5.0 4.0
~~20~~ ~~11.5~~ ~~C~~ ~~21.~~ ~~30.~~ ~~40.~~
 507.17 508.27 509.91 511.41 512.41

+ 1.23 509.77 7.87 508.54 ✓

509.77

5.4 4.4 3.7 0+60 1.8 0.8 0.4
~~70.~~ ~~40.~~ ~~20.~~ ~~28~~ ~~27~~ ~~30.~~ ~~40.~~
 504.37 505.37 506.07 506.97 507.97 508.97 509.37

4.3 4.3 4.5 0+80 3.7 4.0 4.0
~~50.~~ ~~40.~~ ~~20.~~ ~~45~~ ~~200~~ ~~30~~ ~~40~~
 505.17 505.47 505.77 505.27 506.07 505.77 505.77

curb
 3.0 3.5 4.5 5.4 1+00 6.3 6.0 5.6
~~68.7~~ ~~59~~ ~~40.~~ ~~20.0~~ ~~67~~ ~~20.~~ ~~30~~ ~~40~~
 506.77 506.27 505.77 504.97 504.17 503.47 502.57 501.77

17-480

Cor.

165.6

Δ 9

8 244 257.7

Δ 8

10 245 270.2

Δ 7

330 300 219.2 299.7 518.5

Δ 6

94
94°

31-11-12-14

Cor Δ 5

256.4

Δ 4

435

Δ 3

50 276 280.6

Δ 2

3 231 270.5

Δ 1

300 8-11 167.5 296.5 464.0

N 7th

114

140172
North

South

West

East

North
135 31 N

West

East

1899
31.96
397.9
16
74
498

10476
10780
18837.2
100893
7379
18893

1.05
6.3
249

73.2
31.9

88411

NO. 5
MAY 1917

NO. 5
MAY 1917

21335

N 26 52 W
D 1052

471

Δ 1

3830

Δ 2

2552

Δ 3

99

Δ 4

3930

Δ 5

145

Δ 6

471

Δ 7

2552

Δ 8

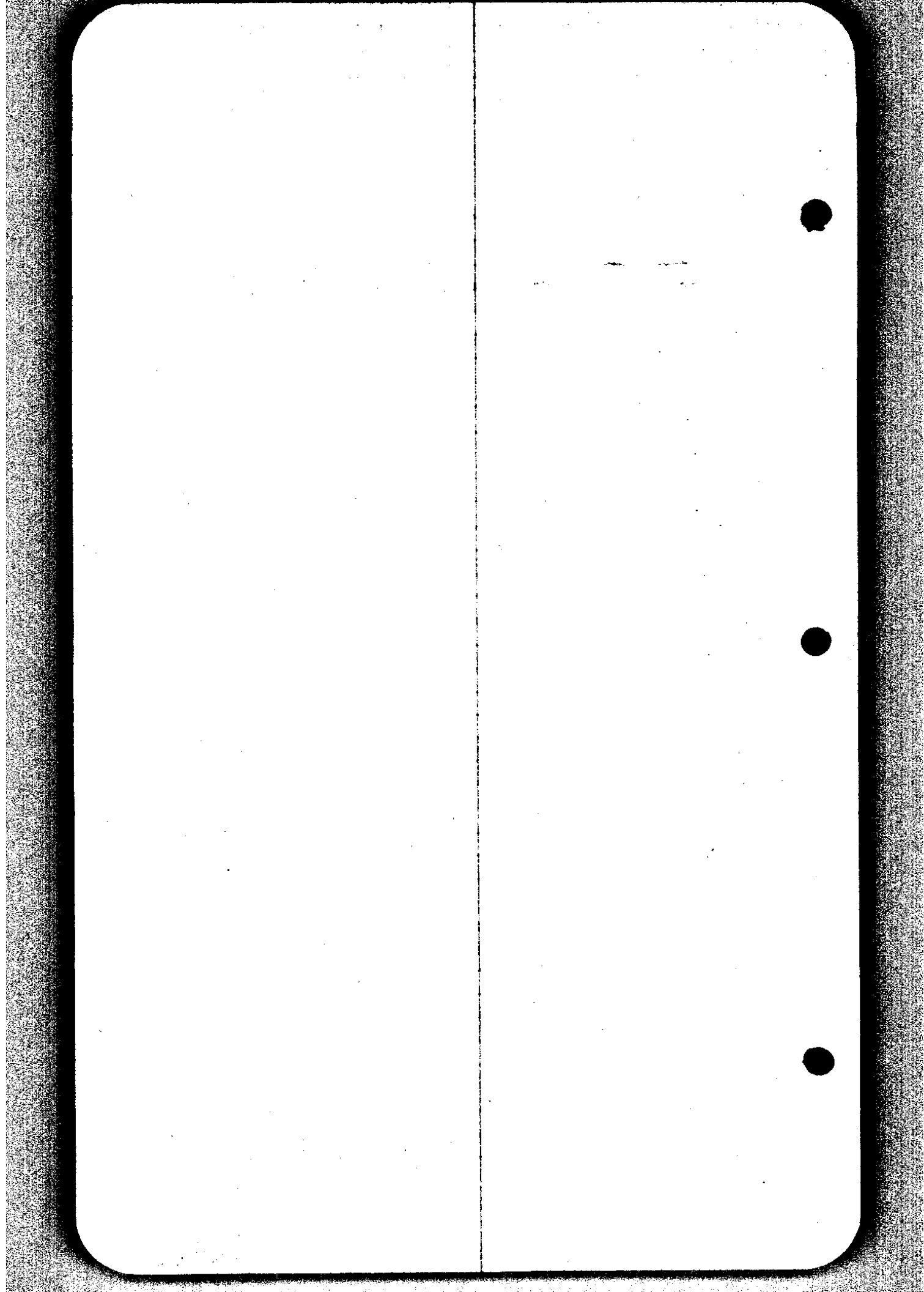
471

21012

1.05
6.3
249

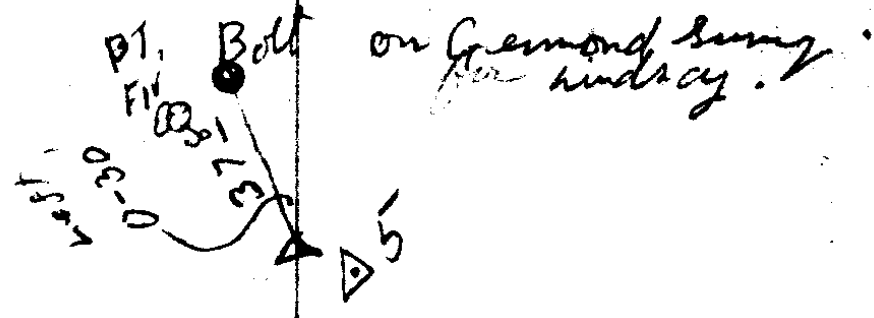
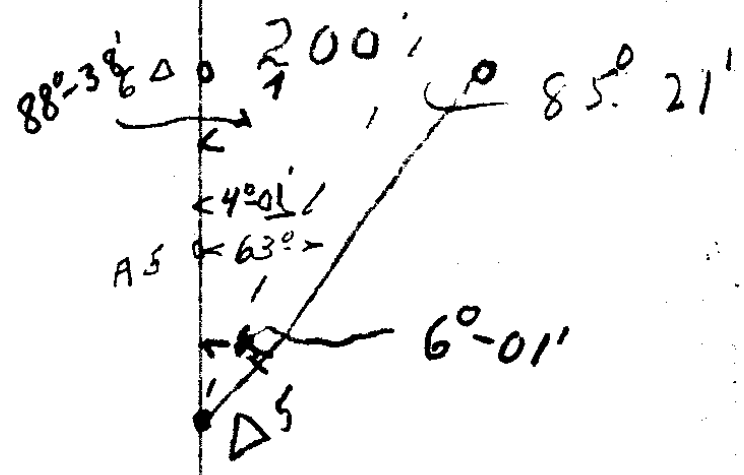
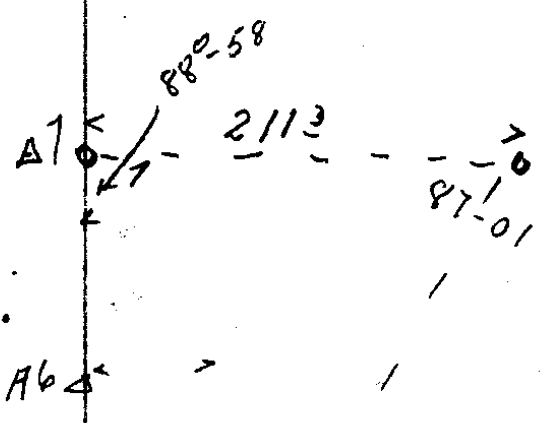
73.2
31.9

42



$$\begin{array}{r} 4 \\ 88-58 \\ 179 \\ \hline 92-59 \\ \hline 87-01 \end{array}$$

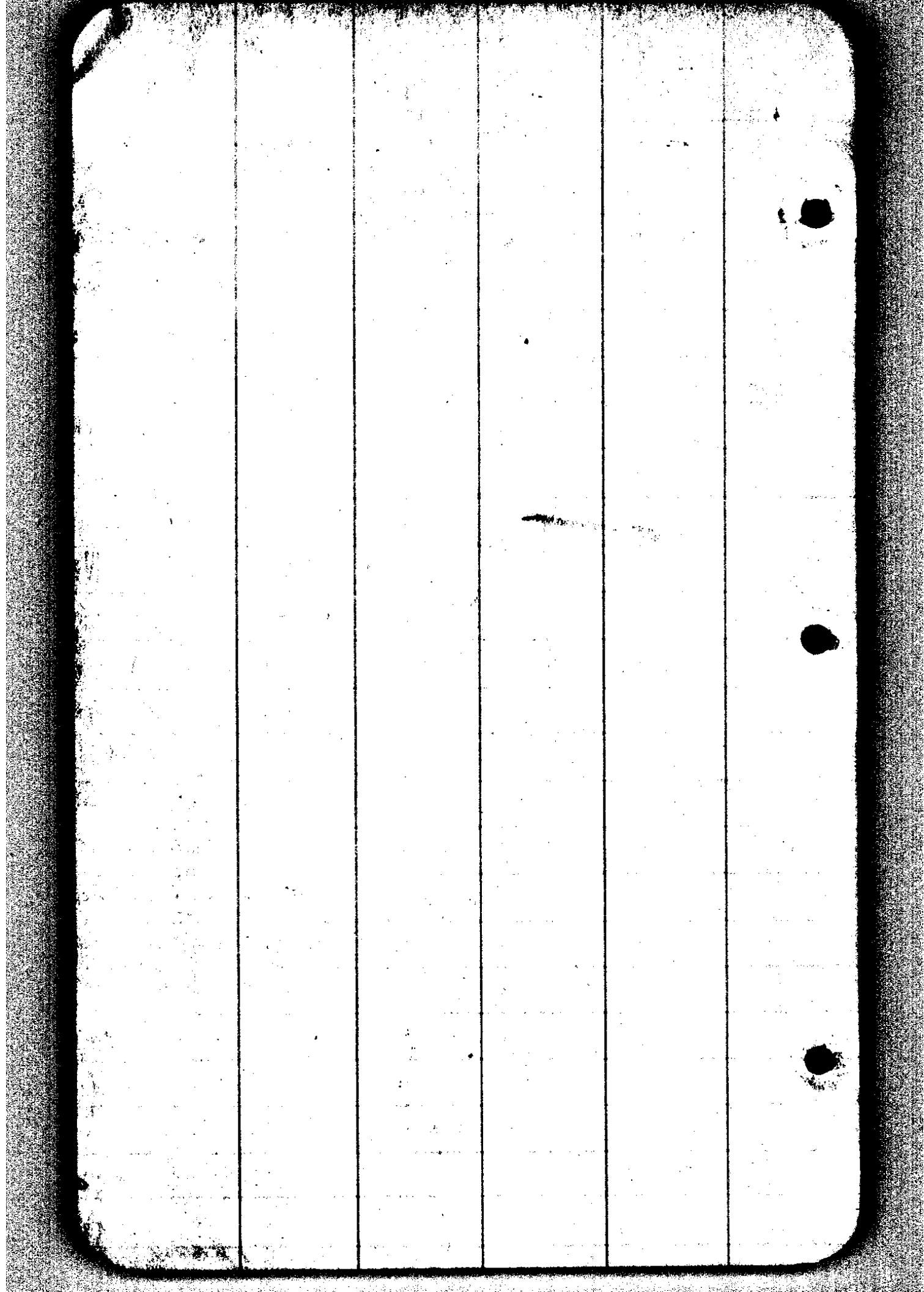
On West line
Cor S.W.



multiply .0579

Split Fence line North turned 90 to
Left

17400



9
15.12

12.9.32

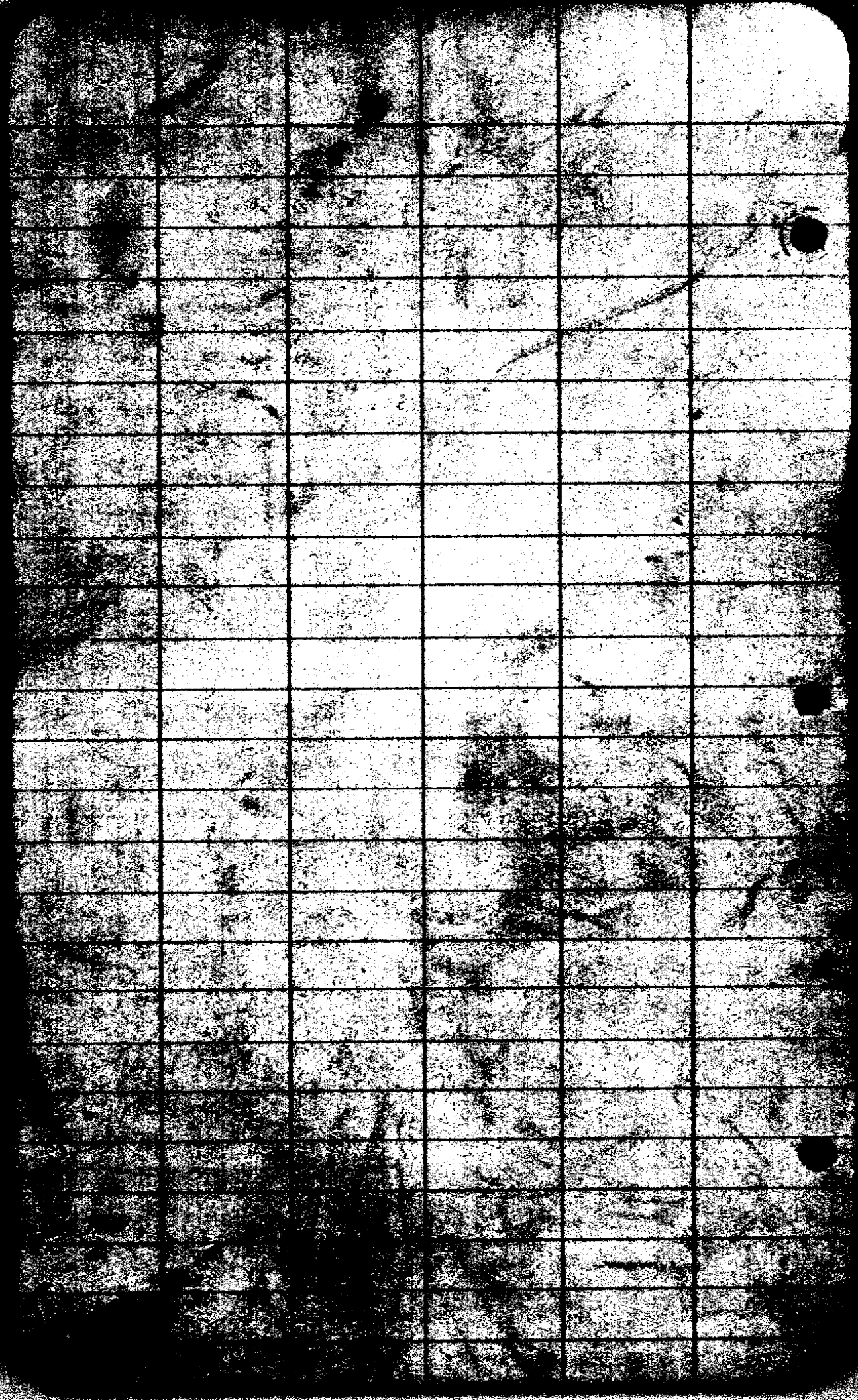
9

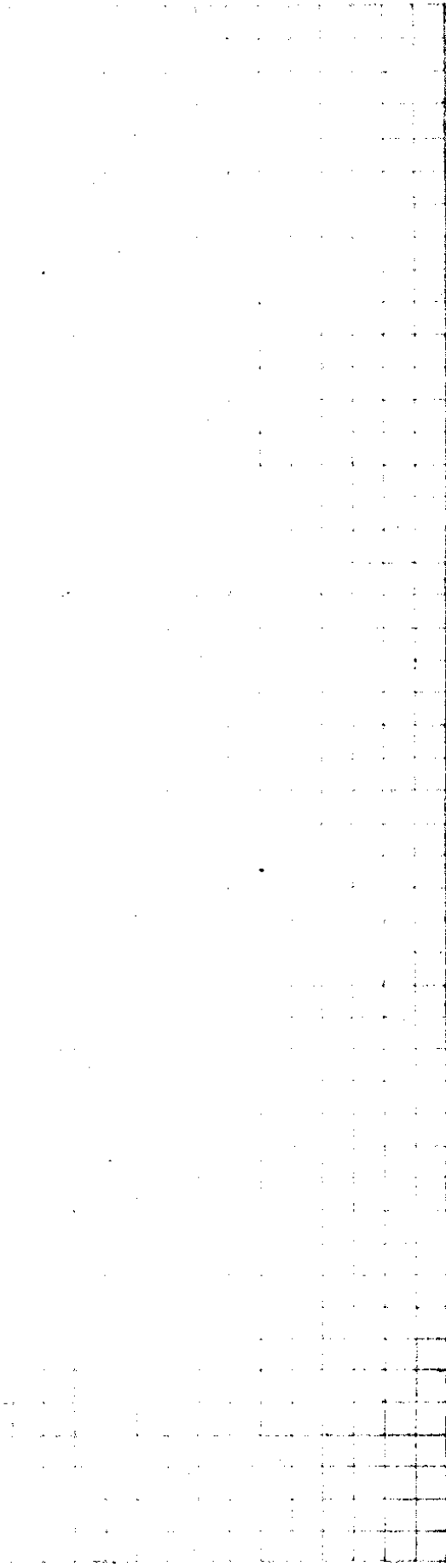
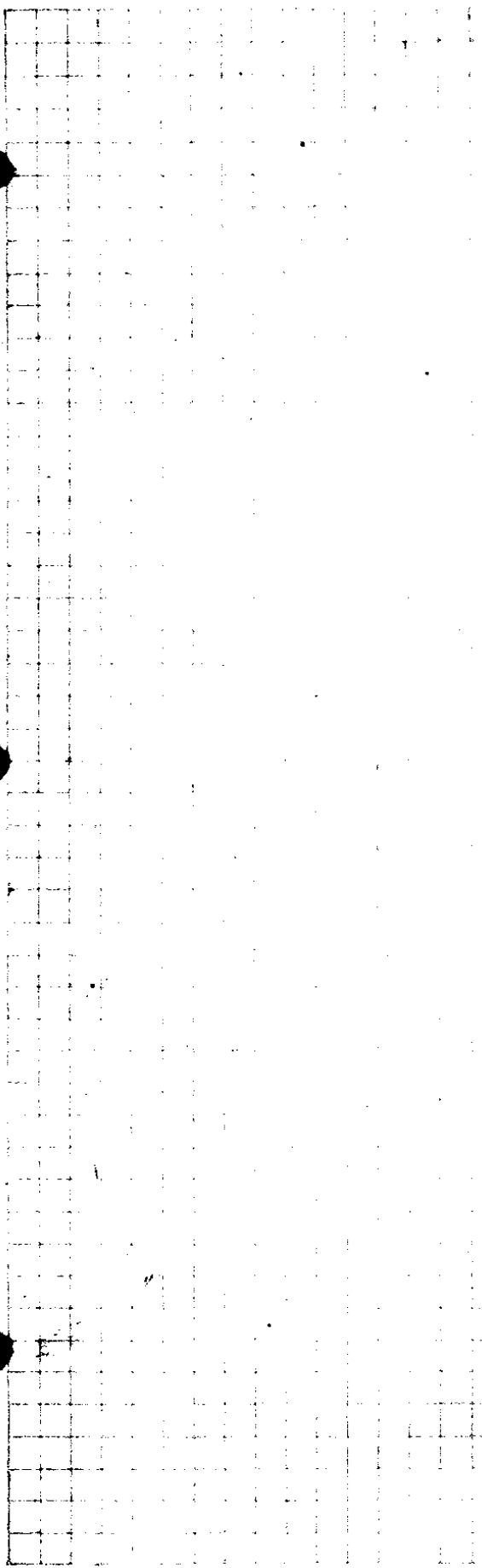
12.9.31

6.4.32

18.0

12.9.32





17-45A

$\frac{.15}{1.3}$

9.7

10.2

$\frac{1.27}{.63}$

\$.

100.00

89.8

4.09

104.09

7

5.86

98.23

88.53

2

5.14

98.95

89.16

89.16

9.79

Grade

0400

100.00

89.9

3.55

103.55

-

3.78

10.2

99.77

89.57

4.25

10.00

99.30

89.3

E

4.84

98.71

88.92

5.61

9.4

97.94

88.54

-

5.57

9.7

97.98

88.28

W 87 - 15

73 15

16 30

N 89 - 15

26 - 30

62 - 45

$$\frac{43^{\Sigma}}{28}$$

$$\frac{49^{\circ}}{16}$$

$$\frac{50^{\circ}}{12}$$

$$\frac{2+00}{51^{\circ}} \\ 0$$

$$\frac{57^{\circ}}{12}$$

$$\frac{69^{\circ}}{316}$$

$$\frac{44^{\circ}}{32}$$

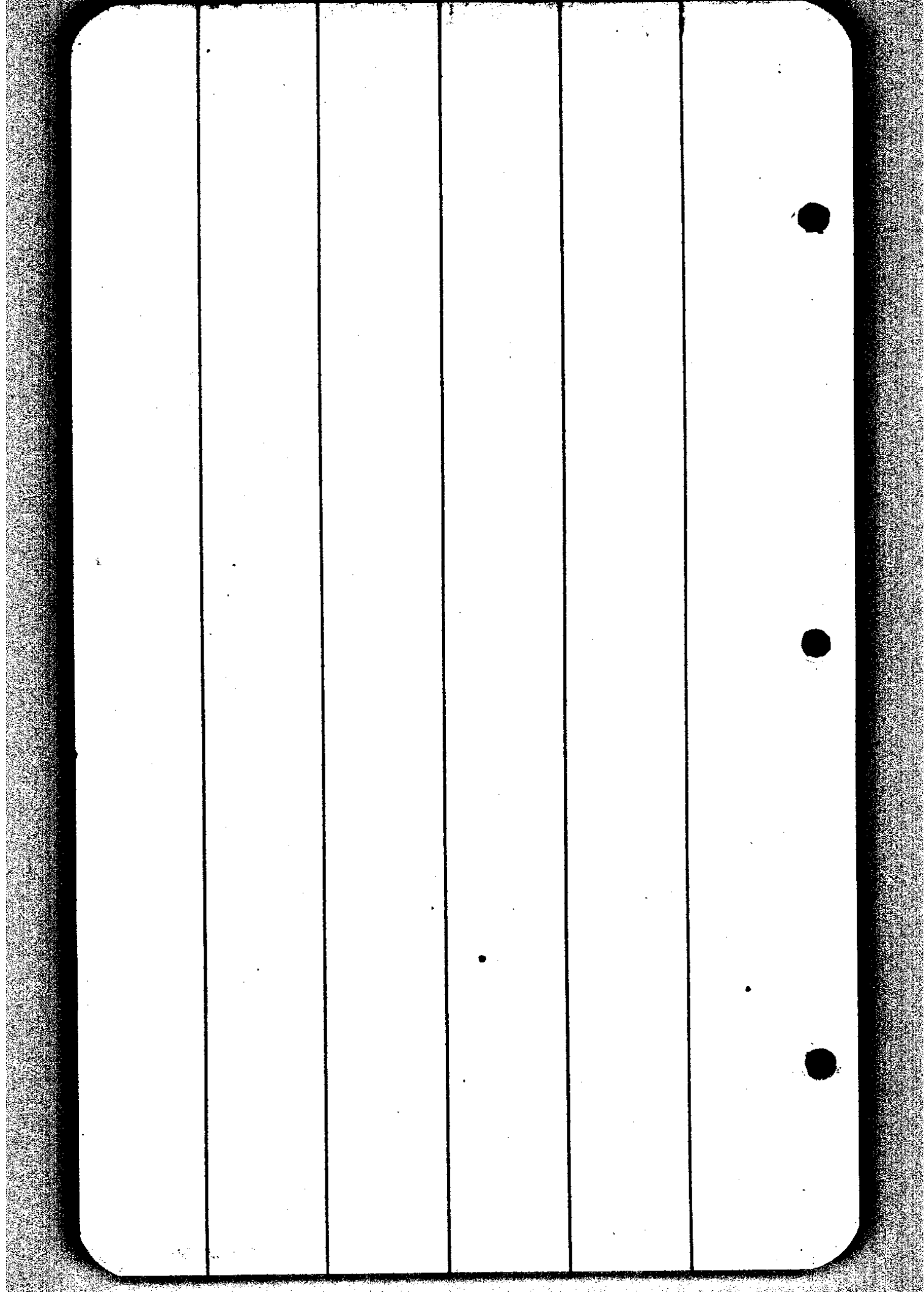
$$\frac{47^{\circ}}{16}$$

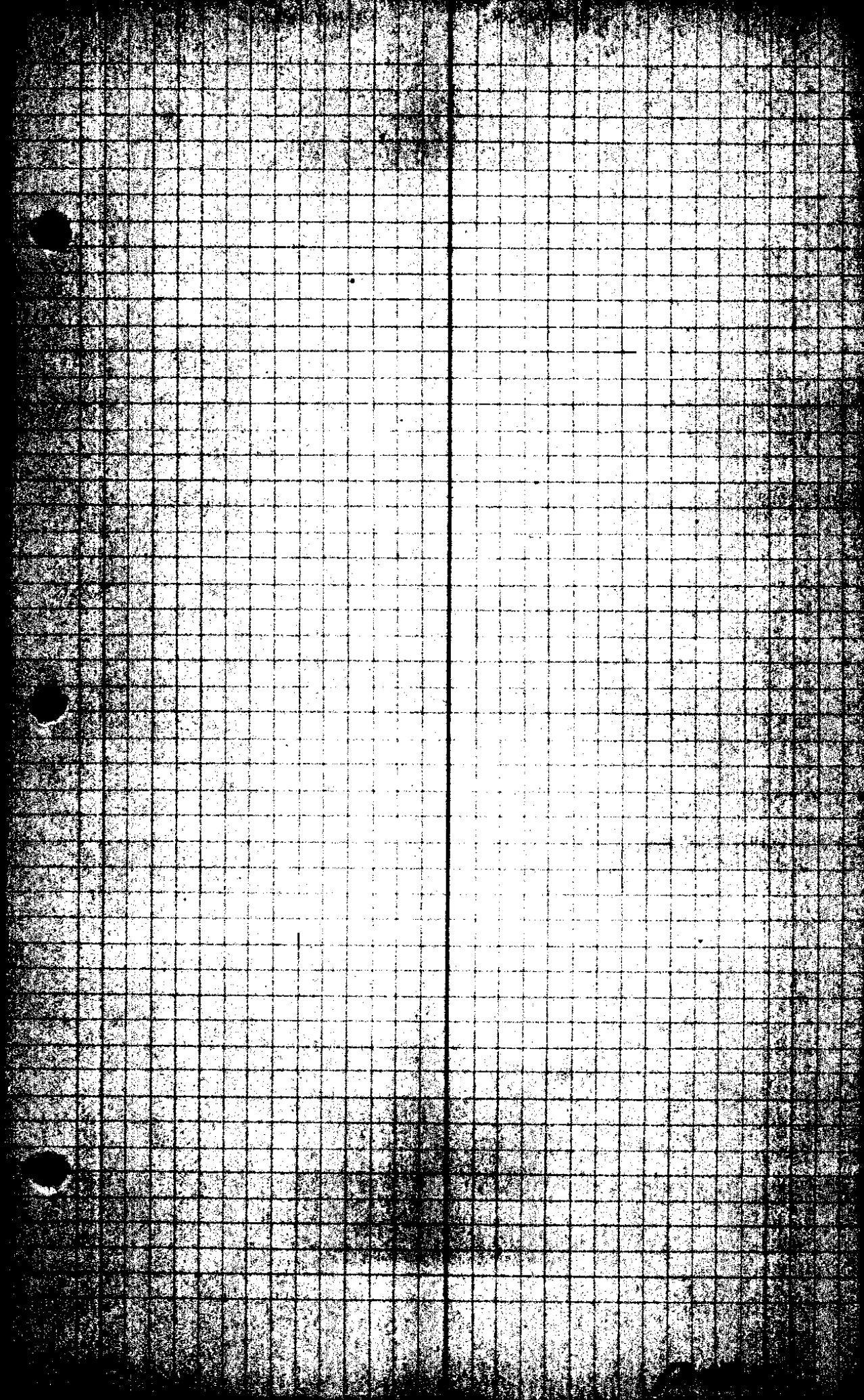
$$\frac{48^{\circ}}{12}$$

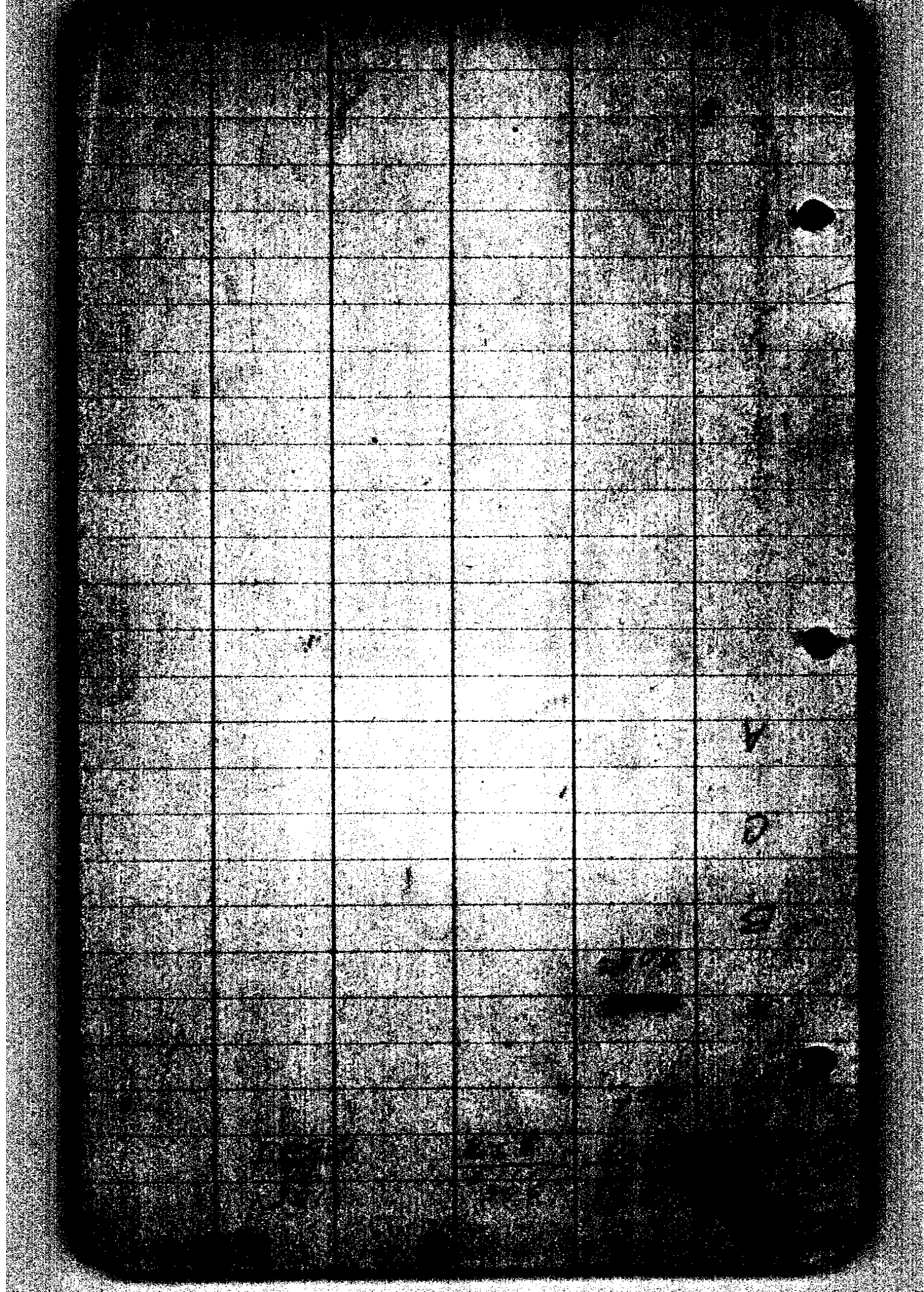
$$2+26^{\circ} \\ \frac{52^{\circ}}{0}$$

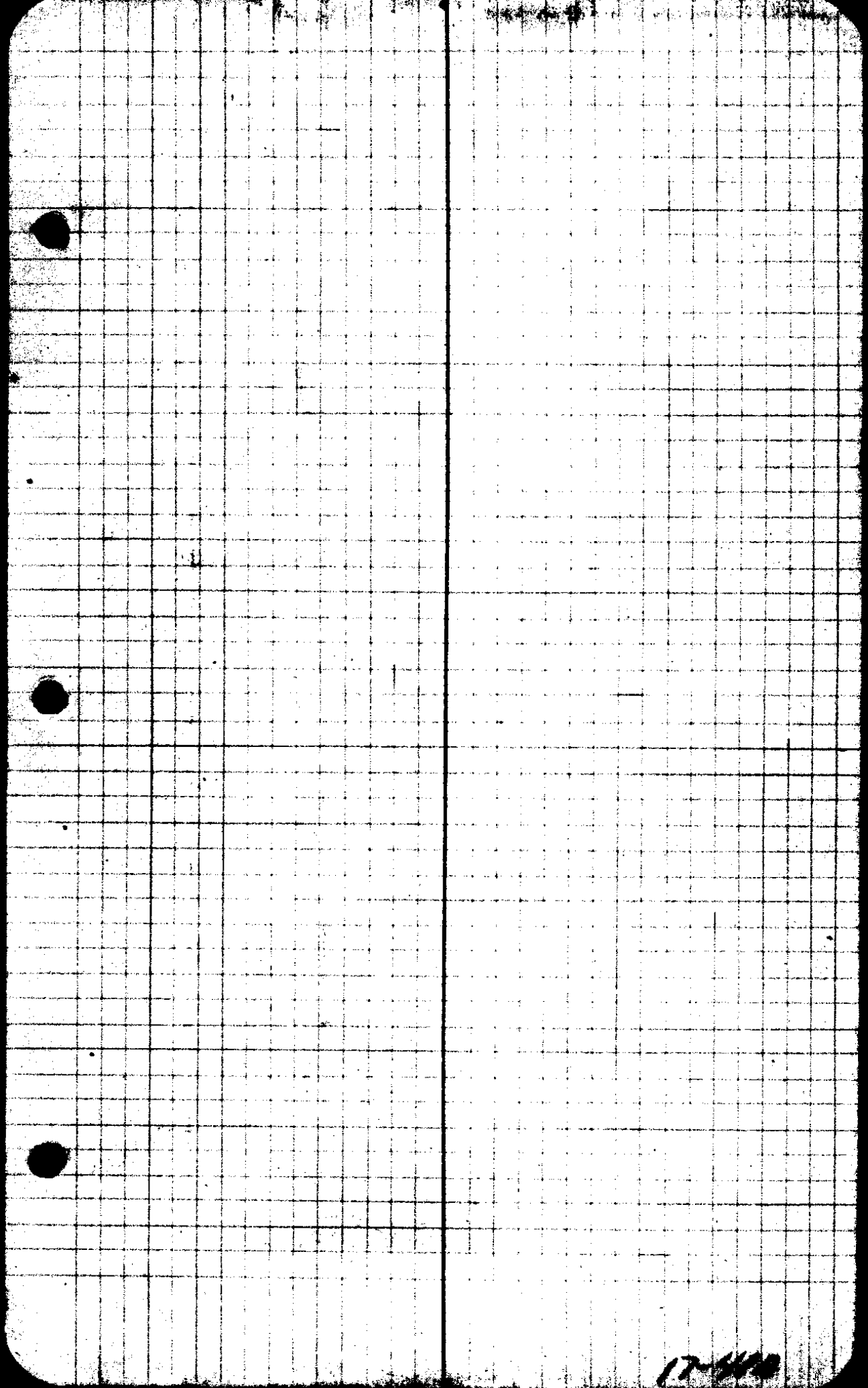
$$\frac{56^{\circ}}{12}$$

$$\frac{61^{\circ}}{24}$$









17-40

$$\frac{71^2}{16}$$

$$\frac{72^2}{12}$$

0+00

$$\frac{72^2}{8}$$

$$\frac{72^2}{4}$$

$$\frac{75^2}{12}$$

$$\frac{83^2}{17.5}$$

$$\frac{84^2}{19}$$

$$\frac{71^2}{16}$$

$$\frac{71^2}{12}$$

0+25

$$\frac{72^2}{8}$$

$$\frac{76^2}{5}$$

$$\frac{79^2}{12}$$

$$\frac{84^2}{24}$$

$$\frac{70^2}{12}$$

$$\frac{70^2}{12}$$

0+50

$$\frac{76^2}{8}$$

$$\frac{75^2}{5}$$

$$\frac{77^2}{12}$$

$$\frac{82^2}{25.5}$$

$$\frac{68^2}{16}$$

$$\frac{68^2}{12}$$

0+75

$$\frac{69^2}{8}$$

$$\frac{72^2}{4.5}$$

$$\frac{75^2}{12}$$

$$\frac{81^2}{30.5}$$

$$\frac{65^2}{16}$$

$$\frac{66^2}{12}$$

1+00

$$\frac{67^2}{8}$$

$$\frac{70^2}{6.2}$$

$$\frac{72^2}{12}$$

$$\frac{76^2}{26}$$

$$\frac{62^2}{16}$$

$$\frac{63^2}{12}$$

1+25

$$\frac{64^2}{8}$$

$$\frac{68^2}{12}$$

$$\frac{76^2}{36}$$

$$\frac{58^2}{16}$$

$$\frac{59^2}{12}$$

1+50

$$\frac{61^2}{8}$$

$$\frac{63^2}{12}$$

$$\frac{71^2}{33.0}$$

$$\frac{52^2}{6}$$

$$\frac{57^2}{12}$$

1+75

$$\frac{57^2}{8}$$

$$\frac{59^2}{12}$$

$$\frac{66^2}{31.0}$$

17-408

No. DIST D.L. R M.C

1042 3°-20

50° 40' 51° 04' E

3010

0° 44'

51° 30' W 52-16 W

3

2997 0°-13'

51° 30' W 51° 32' W

2

3001 3°-12'

51° 30' W 51° 32' W

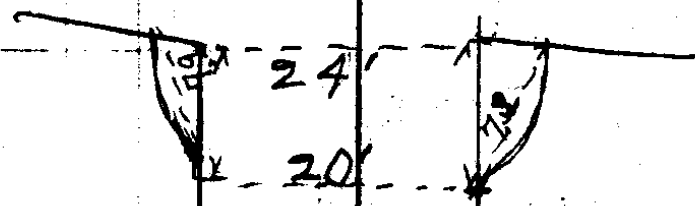
1

91

11-35

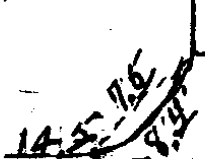
57° W 56° 52' W

Comercial Ave.



128.2

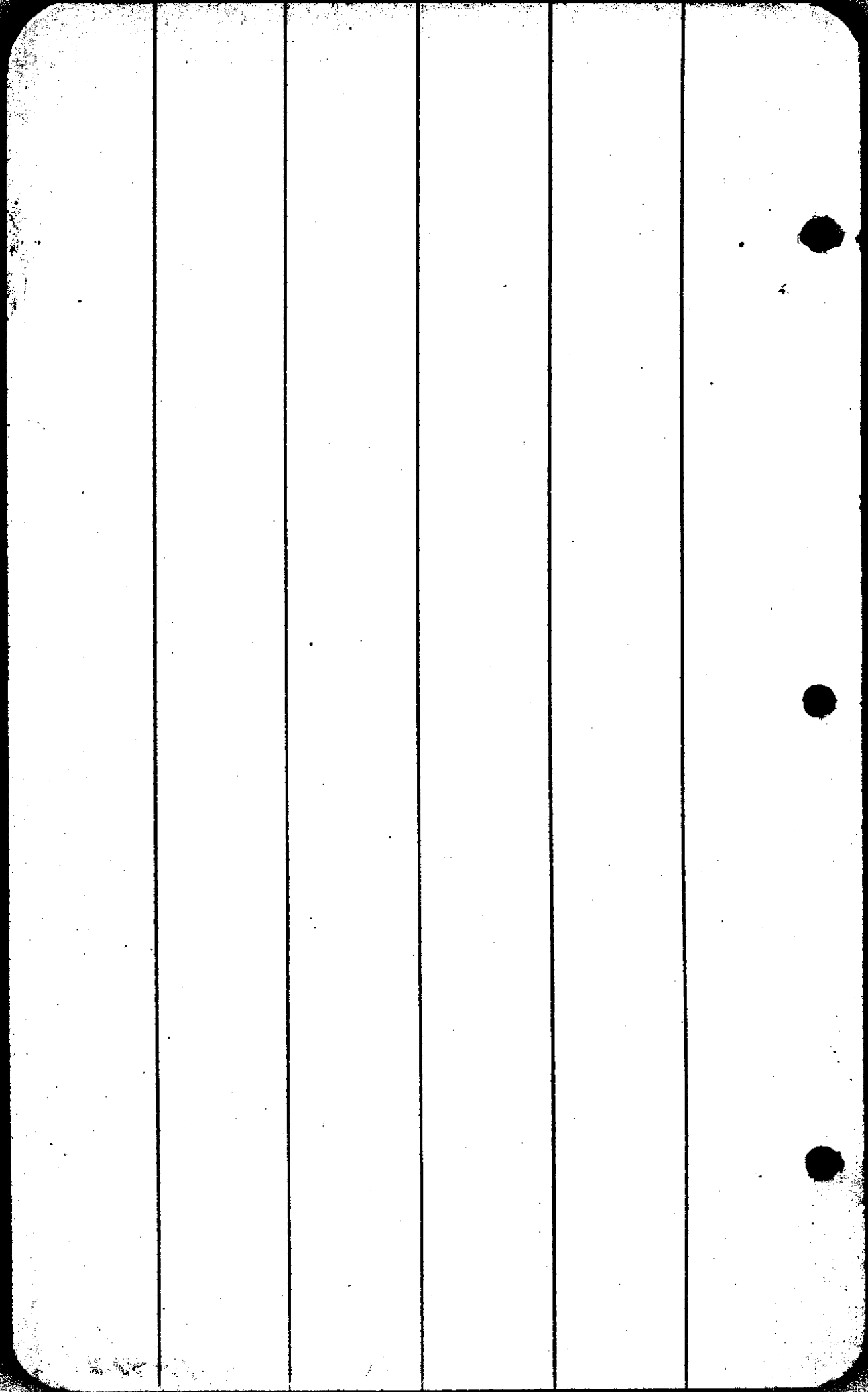
128.1

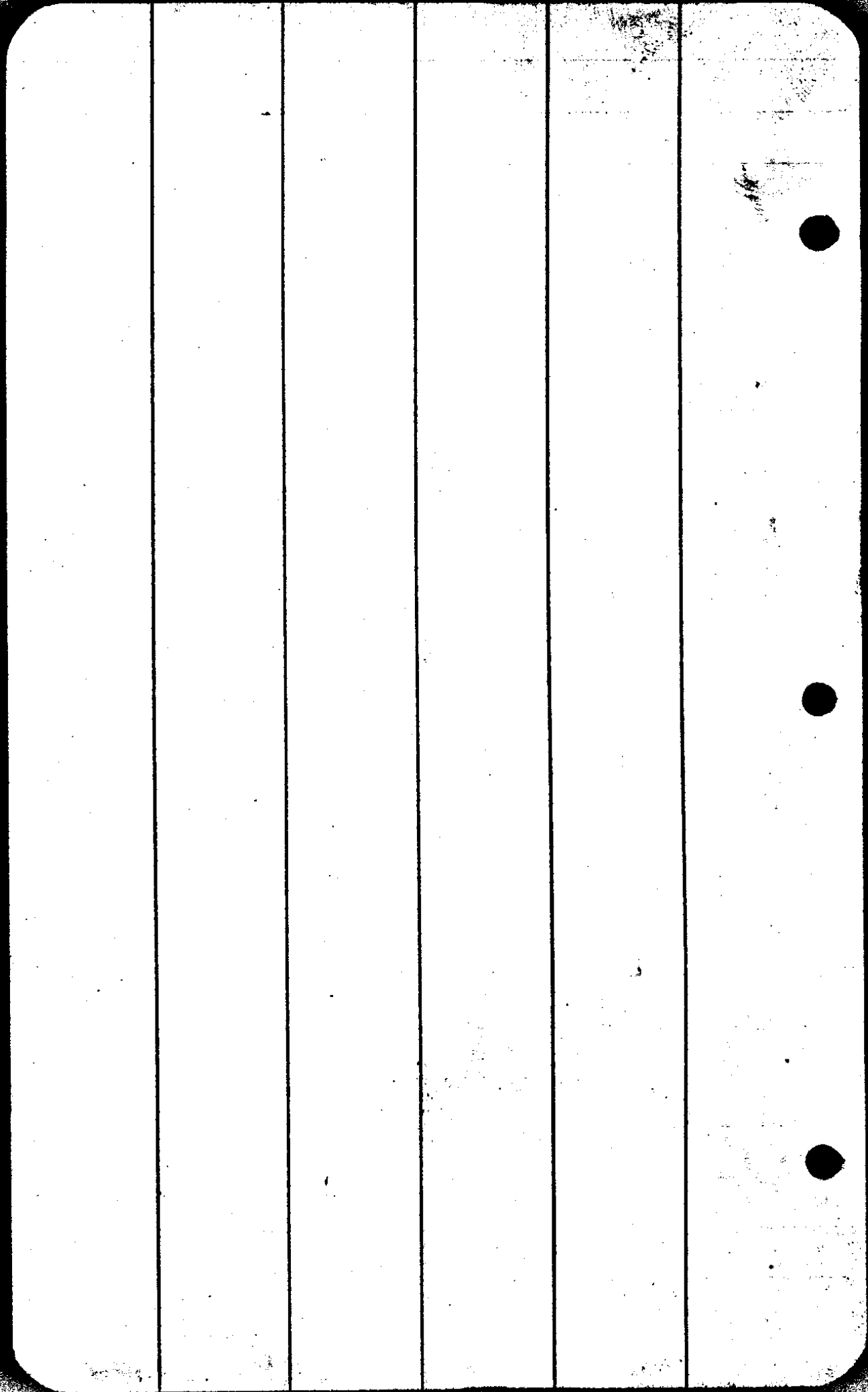


20'

Alley

17-460





Parrish

AM in Par to out

Left C+F

449.75 C 0.18 ✓
 449.93 C 0.63 ✓
 450.16 C 1.15 ✓
 450.39 C 1.14 ✓
 450.61 C 0.98 ✓
 450.84 C 0.84 ✓
 451.07 C 0.49 ✓
 451.30 C 0.78 ✓
 451.53 C 0.93 ✓
 451.75 C 1.10 ✓
 451.98 C 0.60 ✓
 452.21 C 0.75 ✓
 452.44 C 0.48 ✓
 452.67 C 0.27 ✓
 452.89 C 0.45 ✓

Right 449.12

Red Right cable Right 7.47 C+F
 West 7.42 449.17 449.12 C 0.05
 6.26 450.33 449.34 C 0.99
 5.92 450.67 449.62 C 1.05
 5.56 451.03 449.89 C 1.14
 5.47 451.12 450.17 C 0.95
 5.22 451.37 450.44 C 0.93
 5.29 451.30 450.72 C 0.58
 5.37 451.22 450.99 C 0.23
 5.19 451.40 451.27 C 0.13
 4.87 451.72 451.54 C 0.18
 4.74 451.85 451.80 C 0.05
 4.48 452.11 452.07 C 0.04
 4.38 452.21 452.35 F 0.14
 4.27 452.32 452.62 F 0.30
 4.30 452.29 452.89 F 0.60
 4.46 452.13

17-48A

Sta	+	Parrott π	-	Rod	Elev
	2.62	466.02			463.40
T.P.	1.68	457.18	1052		455.50
7 P ^{on} _{end} _{rod}	6.85	456.59	7.44	Left East	449.74
0+30				6.67	449.92
0+50				6.03	450.56
0+75				5.28	451.31
1+00				5.06	451.53
1+25				5.00	451.59
1+50				4.91	451.68
1+75				5.03	451.56
2+00				4.51	452.08
2+25				4.13	452.46
2+50				3.74	452.85
2+75				4.01	452.58
3+00				3.63	452.96
3+25				3.67	452.92
3+50				3.65	452.94
3+75				3.25	453.34
4+00				3.11	453.48

Grade C & F

28.93 C 0.38-

24.85 C 0.21-

22.60 C 0.33-

520.35 C 0.92-

516.93 F 0.01-

516.21 C 0.03-

514.92 F 0.17-

513.64 F 0.22-

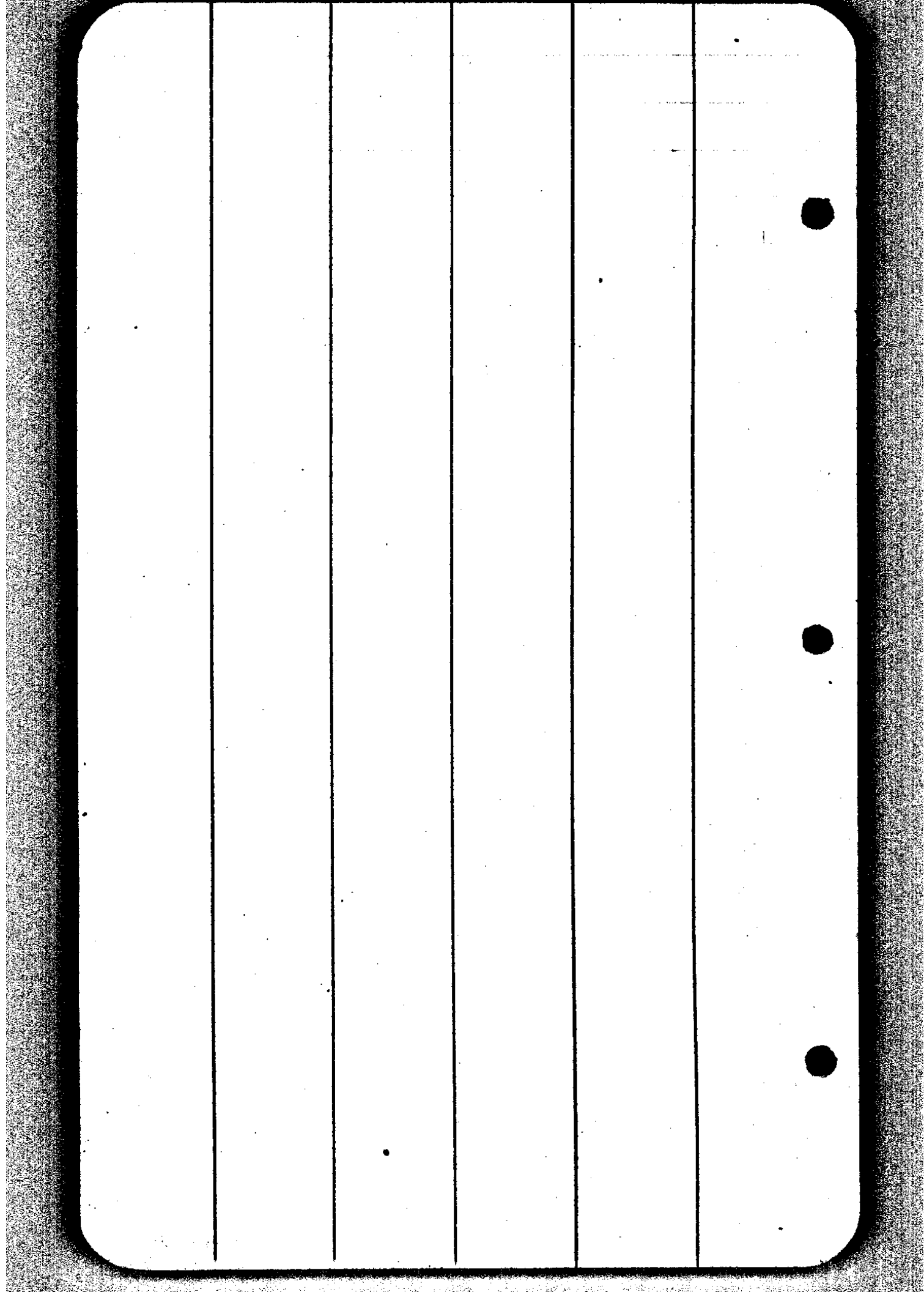
512.14 F 0.03-

510.80 F 0.22-

509.77 C 0.29-

508.49 C 0.56

507.20 C 0.68



Grade C & F

62.95 F1.38

60.69 F1.36

58.43 F0.87

56.20 F0.02 Orig C 0.18

C 0.20 " " F 1.10

55.30 C 0.20

53.70 C 0.67

51.97 C 0.91

50.24 C 1.09

48.72 C 1.42

47.11 C 1.03

44.46 C 1.08

42.08 C 1.07

39.71 C 2.15

34.65 F 0.71

32.41 F 0.43

30.17 C 0.31

Sta	#	T	-	R	EV
		53822			
4+12				8.91N	529.31
7+66	0.42	526.07	12.57		525.65
3+66				1.01N	525.06
3+41				3.14N	529.93
3+16				4.80N	526.27
2+39	old stake			9.15N	516.92
2+25				9.83N	516.24
2+00				11.32N	514.75
1+75				12.65N	513.42
TP	2.28	515.70	12.65		513.42
1+46				3.59N	512.11
1+20				5.12N	510.58
1+00				5.64N	510.06
0+75				6.65N	509.05
0+50				7.82N	507.88
Club End				9.92	505.78
0+50 south old stake				8.99	506.71

17-450

Roberts

Sta	+	+	-	Rel. Elev
	99	581.18		580.19
TP	1.76	580.04	12.90	588.28
9+00				8-47 S 561.57
8+75				10.71 S 559.33
8+50				12.48 S 557.56
TP	2.23	559.79	12.48	557.56
8+23				3.61 S 556.18
7+73				5.72 S 554.07
7+73				4.29 N 553.50
7+50				5.42 N 554.37
7+25				6.91 N 557.88
7+00				8.46 N 551.33
6+78				9.65 N 550.14
6+52				11.65 N 548.14
TP	0.25	548.39	11.65	548.14
6+25				2.85 N 545.54
6+00				4.60 N 543.79
5+75				6.53 N 541.86
TP	0.175+0.75		11.28	537.11
	1.11	538.22		
4+75				4.28 N 533.94
4+50				6.25 W 531.97
4+25				7.76 N 530.46

91.5 92.8 C = 93

~~C. 1.19~~

91.0 91.0 C 1.34

~~1.34~~

90.5 90.5 C 2.69

~~C 2.69~~

90.0 90.0 C 4.19

~~4.19~~

552

~~4.19~~

630

4.69

440

5.33

2.10

4.52

376

9.05

22.08

4.30

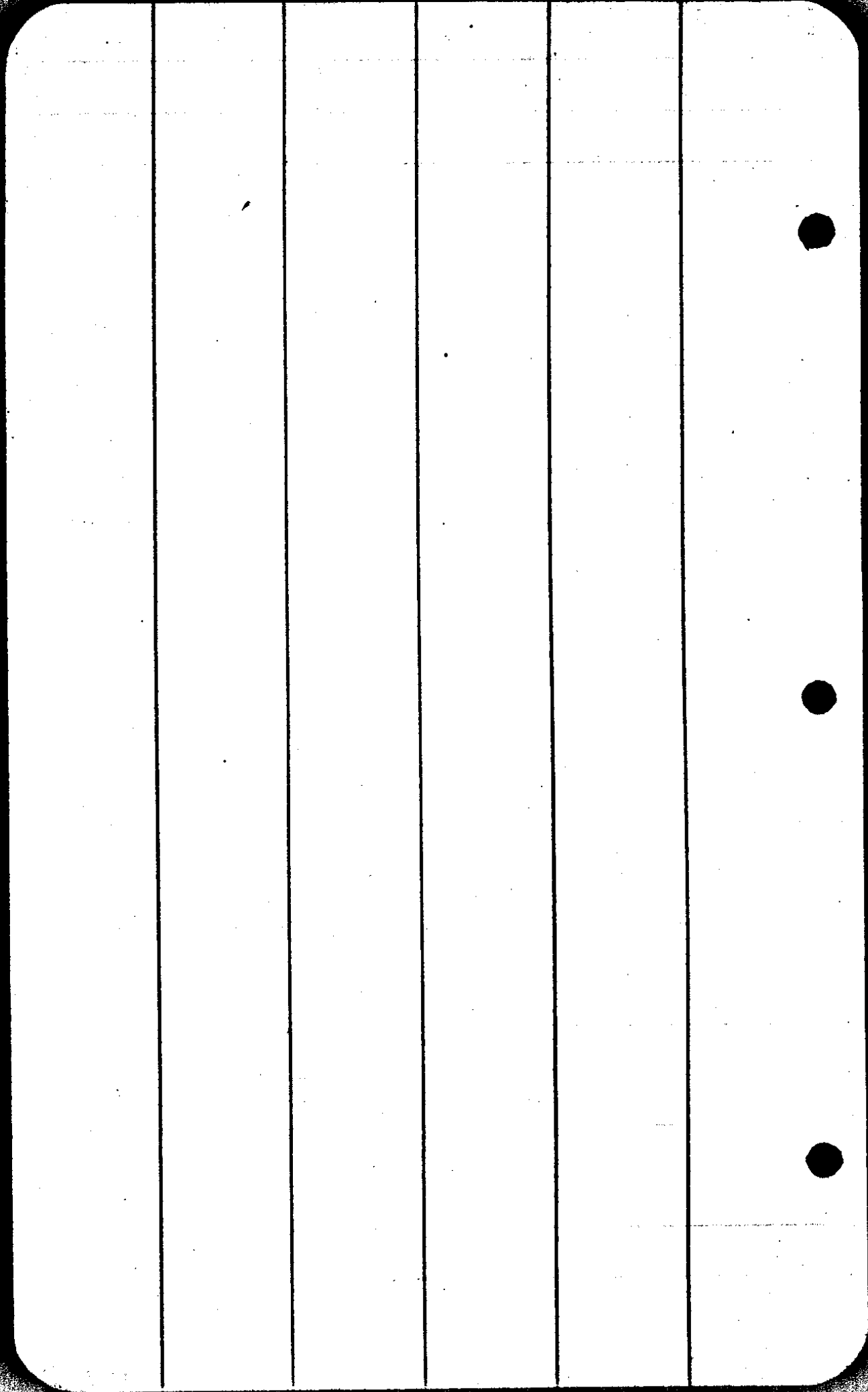
27.89

22.08

5.81

94.19

100.90



98.5

C 1.60

98.0

C 1.46

97.6

C 1.94

97.2

C 2.80

96.8

C 2.64

96.4

C 4.17

96.0

C 4.83

C 1.83

95.6

C 5.63

C 2.63

95.2

C 6.63

C 3.63

~~94.8~~

~~C 7.24~~

~~C 4.24~~

~~94.4~~

~~C 6.85~~

~~C 3.85~~

~~94.0~~

~~C 7.80~~

~~C 4.80~~

93.6

C 8.83

C 5.83

93.2

C 8.39

C 5.39

92.8

C 9.17

C 6.17

92.4

C 9.28

C 6.28

95.4

93.0

C 3.22

C 1.22

C 2.22

92.5

C 6.09

C 6.99

C 4.99

91.9

C 7.56

C 3.36

C 6.36

91.5

C 3.23

C 3.93

C 2.23

DITCH

AUG. 18 - 1925

18+00

3.76

98.49

94.73

19+00

6.15

92.34

20+00

5.30

93.19

20+92

4.30

94.19

17-489

St.	+	H.I	-	-	Elev
0+00					100.00
	5.52	105.52			
1+00				6.06	99.46
2+00				5.98	99.54
3+00				5.52	100.00
4+00			D ₁	6.08	99.44
5+00			D	4.95	100.51
6+00			4.69		100.83
	6.30	107.13			
7+00				5.90	101.23
8+00				5.30	101.83
8+26	xL 94°50			5.09	102.04
9+00				5.88	101.25
10+00	xL 6°37'			5.33	101.80
	4.90	106.20			
11+00				3.77	102.43
12+00				4.61	101.59
13+00				4.23	101.97
14+00				4.52	101.68
	2.10	103.78			
15+00				7.56	96.22
16+00				5.19	98.59
17+00				4.22	99.56
18+00				9.05	94.73

LANSING DRAINAGE

17-480

8+26

L 94° 50'

10+00

L 6° 31'

1. 1. 1. 1.

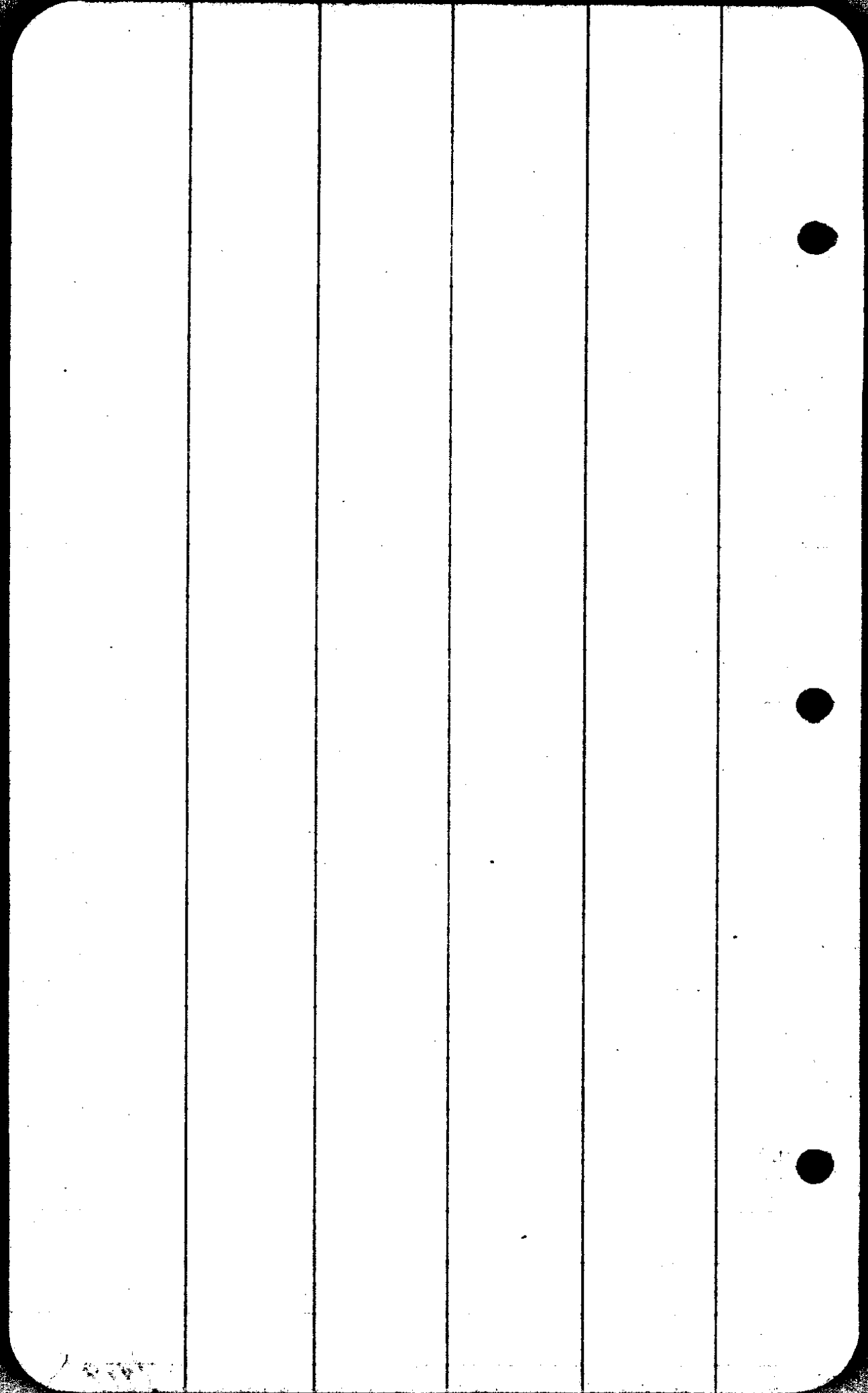
1. 1. 1. 1.

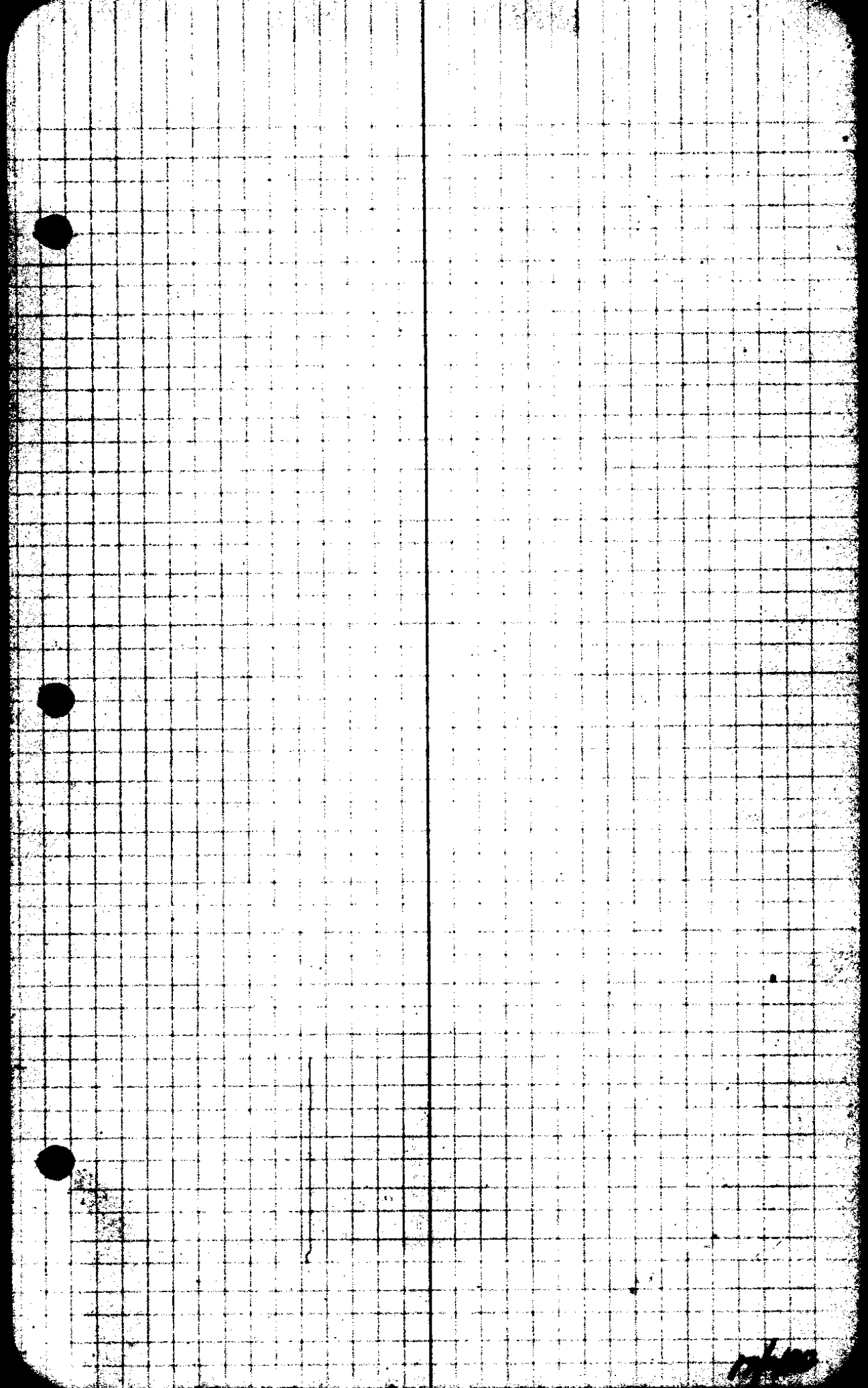
WD 20' 54 8' E 13'

Cov. tract 1 + 2. South

set on $\Delta 2$ sighted on $\Delta 3$

12/100





Δ C 6

50'

5° R

Δ C 5

4-15 211°

Δ C 4

500 196°

Δ C 3

13° 108°

Δ C 2

3°-30' 152°

Δ C 1

136°

Δ C 0'

165° R 90°-31'

N 2°-30' E

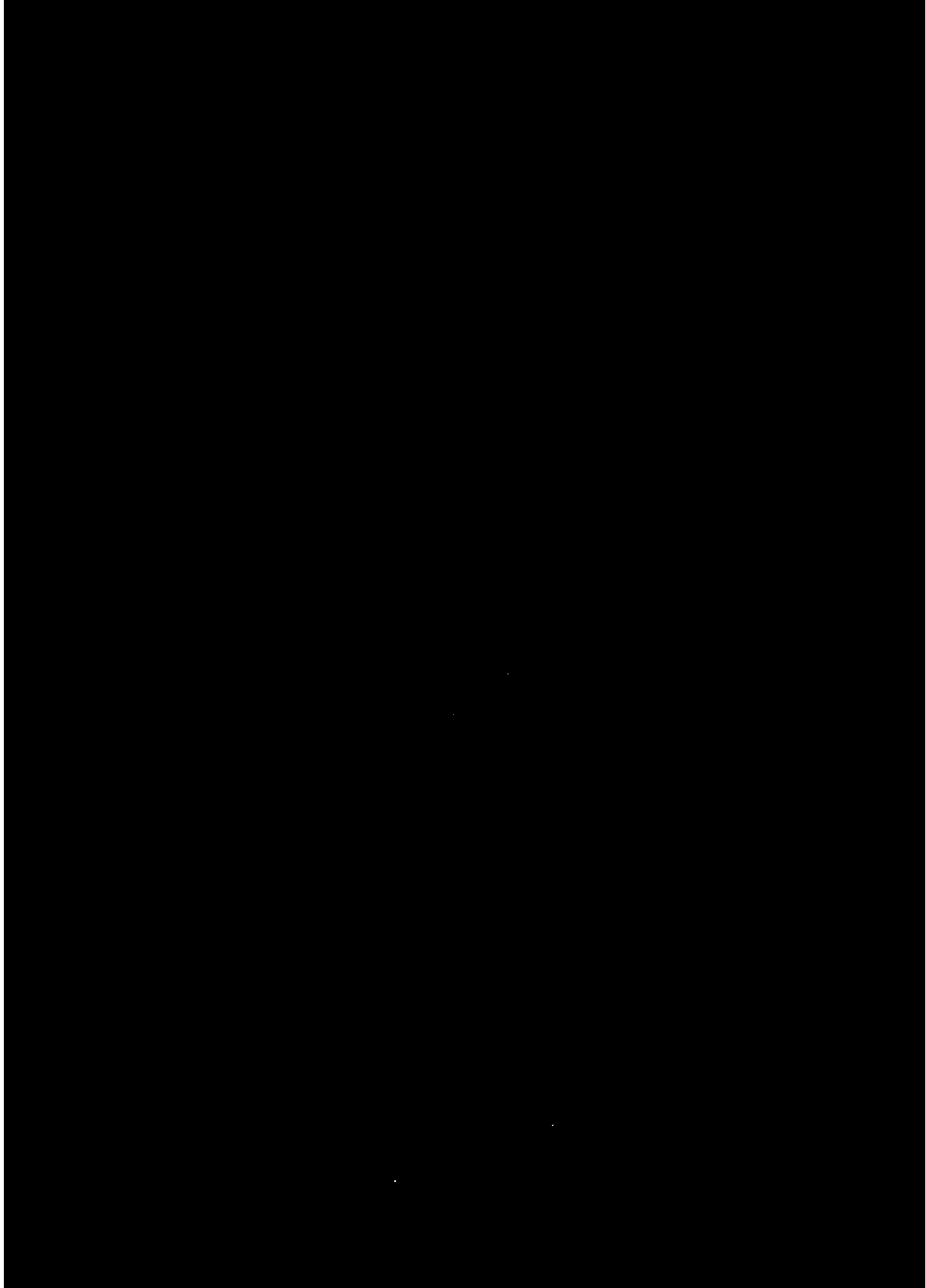
Δ C 2

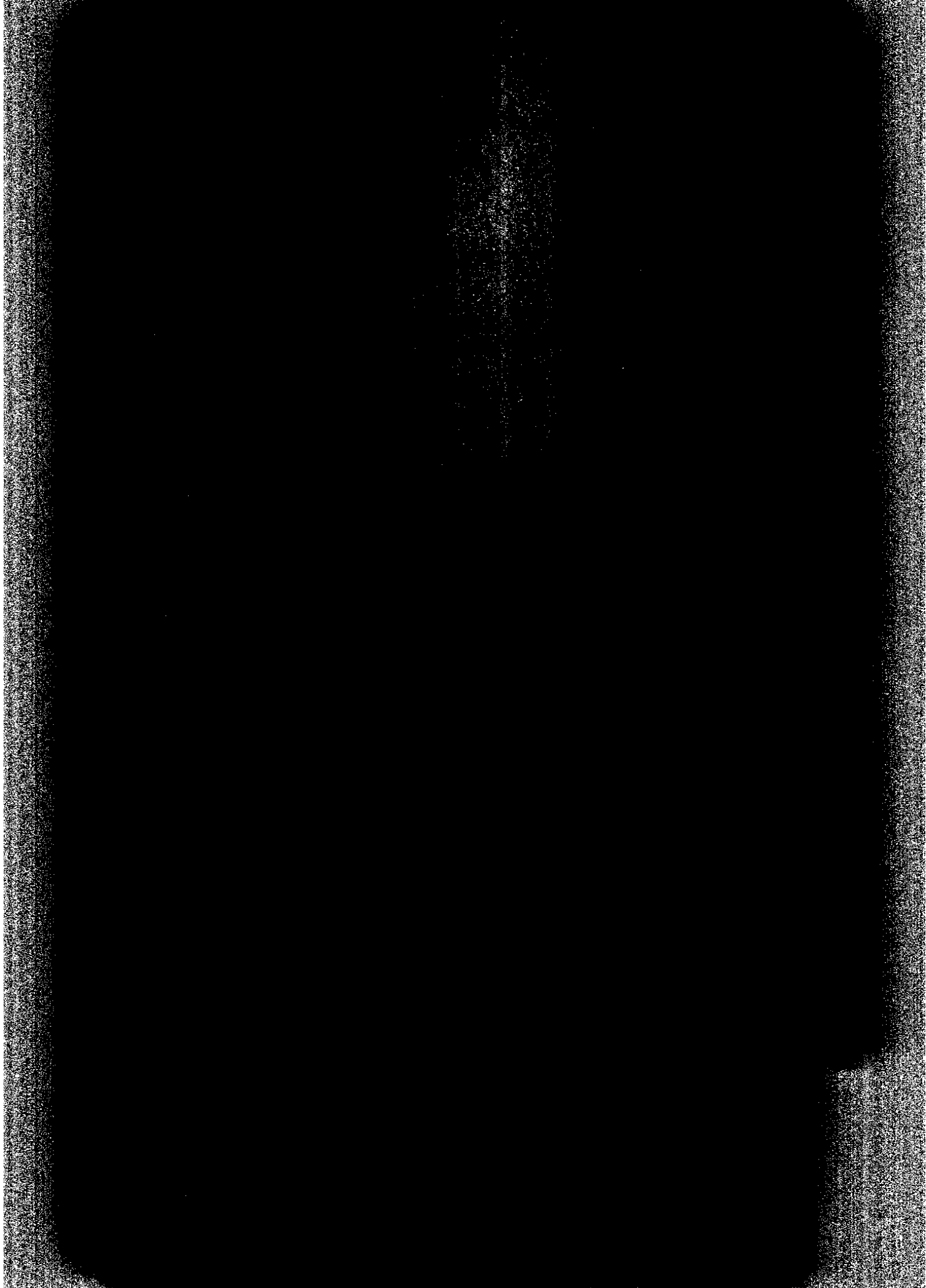
Needle No. ND-588

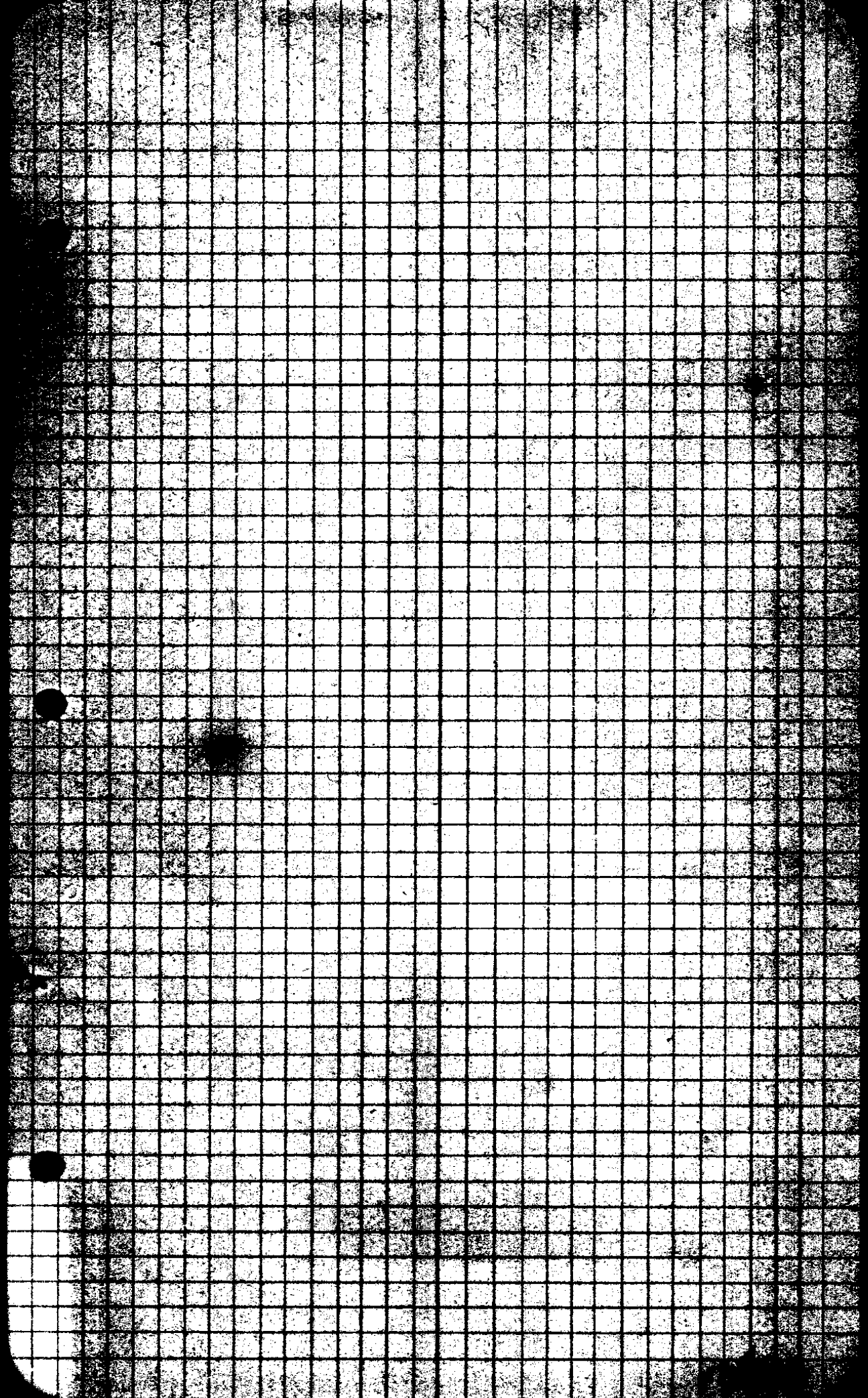
992

N 89°-33' W

Δ 2







int h
orb h
43

11/COV

3.00

83-01

S10-30E

S81-42E

Δ 8

6.55

Δ 7

13.55

7.20

7.20

6°-45'

N86-17E

Δ 5

N86-15E

4.00

Δ 4

4.47

10°-30'

N79-30E

N79-30E

Δ 3

4.00

Δ 2

3.0

Δ 1

3.0

int h
orb h
81/43

7.75

East

E 81-38E

Δ 3 sec
orb h

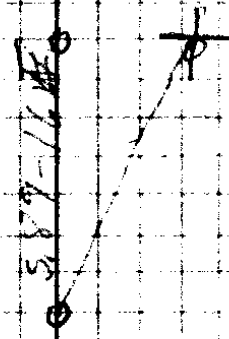
12.50

88

2/2

1154 North

30.25 ch.



9-15 and
 How 35-36
 Y-25-17
 Lat 43-17

1154 North
 30.25 ch.



11/10

stake

8.78

N5W

stake

73°

5.34

N78W

stake

28°

5.34

N50W

corner

X

cut

1.437

Δ6

7.00

Δ5

2.00

Barrel

Δ4

corner

1.397

Δ3

12.91

Δ1

47.00

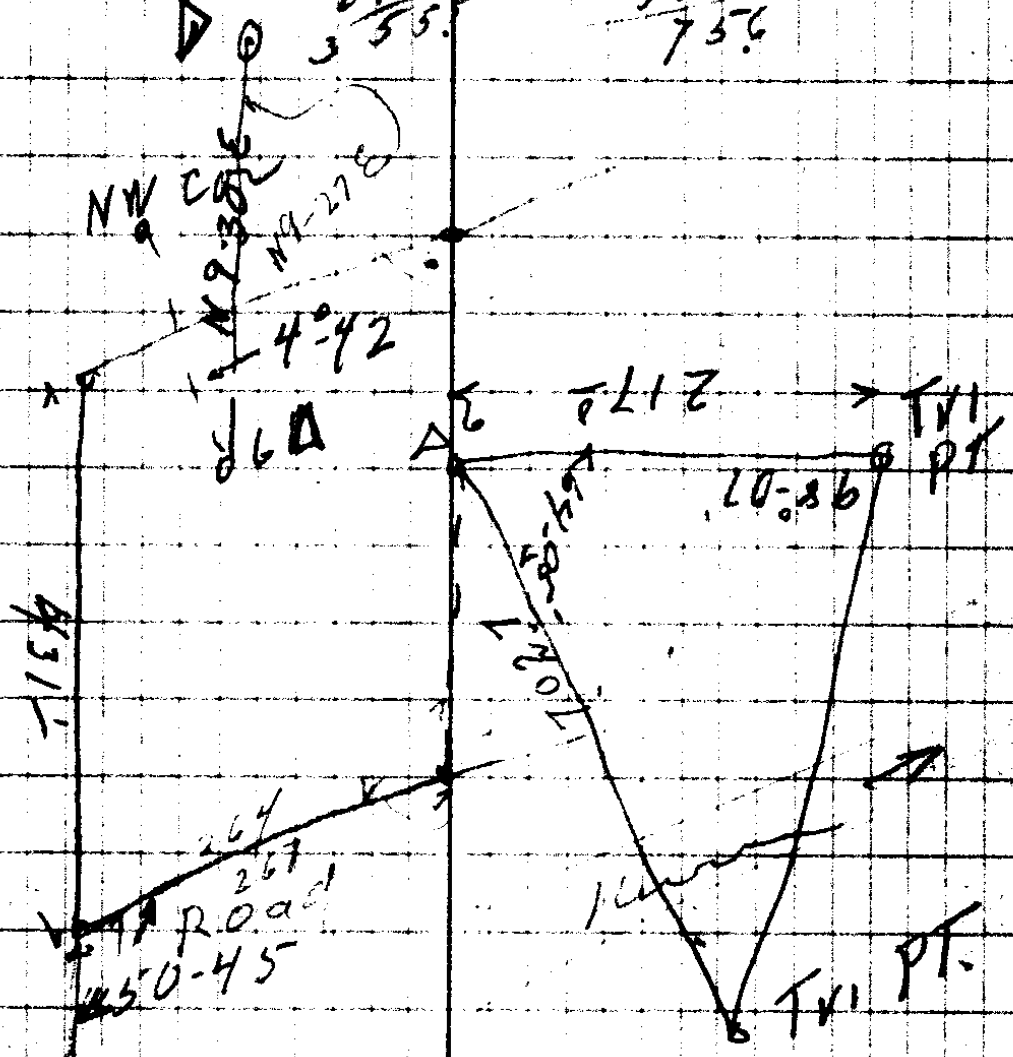
East

589-16E

SW corner

$$\begin{array}{r} 142 \\ 213 \\ \hline 355 \end{array}$$

$$\begin{array}{r} 431 \\ 355 \\ \hline 786 \end{array}$$



June 25-1922
 8-40 A.M.
 Ver 42°-23'
 Hor 87°-58'

Obbaine S.W. Cor.

O & C. Power Co. Line

Sta.	Stadia Dist	Left Angles	Right Angles	M.C.	CC
Δ 8	306				
Δ 7	292 ⁰ 146				
Δ 6	520 ⁰				
Δ 5	126 ⁰				
Δ 4	136 ⁰				
Δ 3	209 ⁰				
Δ 3	149 ⁰				
	71 ⁰				
Δ 2	278 ⁰				
	120 ⁰				
1 Δ		P.O.T.		N 55° 45' W	
4 T.O.	92 ⁰	10°-02'		N 55-45 W	

0400 =
File 222

23.6 10

22.6

last bot 1356

452

452

510.76

100

) 610.76 (20.7

4

44) 210

176

487) 3476

3409

17/100

4 6.75
66

330
845
2755
130

40 50
05

11.503, B 6
83867
3459

927
64

445.5
13

75 3803

370.8

25/320
2305

419335
335468

5562

12
300

38493

59328

83708
485

220.7
123
97.7

630-141
470

41 8540 66
689664 198
3334832 0
3407983 820.4

80902
64

478
123
355.0
220.7
575.7
381
956.7

445.5
2.040
2408485412

323608

486
369
765

51.777 28

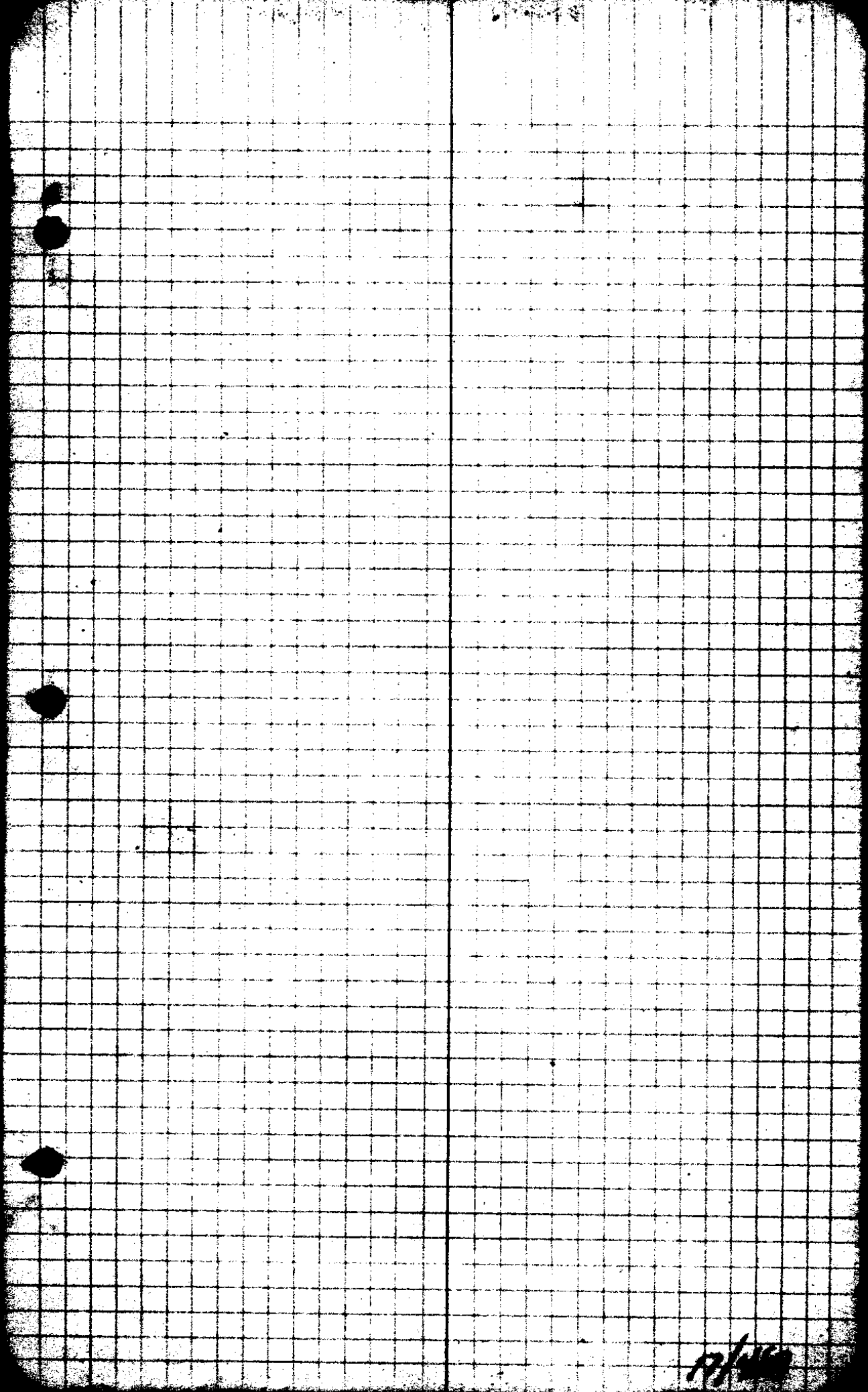
516
39.2
590
N 87-34W
129
177-34
S N 2-26W

242.8
80.8

66
8

322.
80
502

528



17/100

Lilly

NE Cor.

3554

NE Cor.

459° 117-51

588 E

S West

308°

Δ 1.

292.2 110-01

523-49W

NW Cor

303°

N 46-10W -

NE Cor

Apr. 17-1925
Epstein
Bowker

New post 4" x 4" x 4' set
from one B.T. standing
on 12" Alder S 58° E 25' W
Post marked C.5.-C.37
Witness Mr. Ford.

593

59.2

38.5

51.8

34.0'

17/1925

1/4 Cor. Oct 15/22

22. - Enter bottom

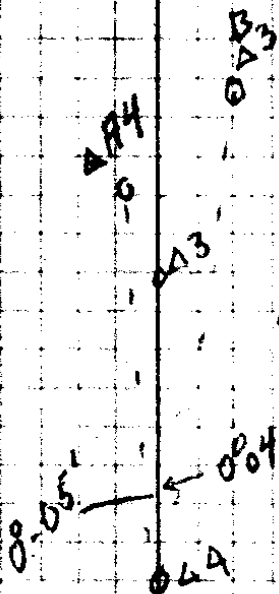
40. 5" Fir N86E 180 lbs

6" - S26E 153 lbs

59. Ch bank - mound

West Oct 16/21

sight on $\Delta 3$



19258' Food
 $\Delta 5$ 6.5' Old

on lot 2+3

from 2 on lot 2 on
1 back from $\Delta 2$
38.5

an old stake

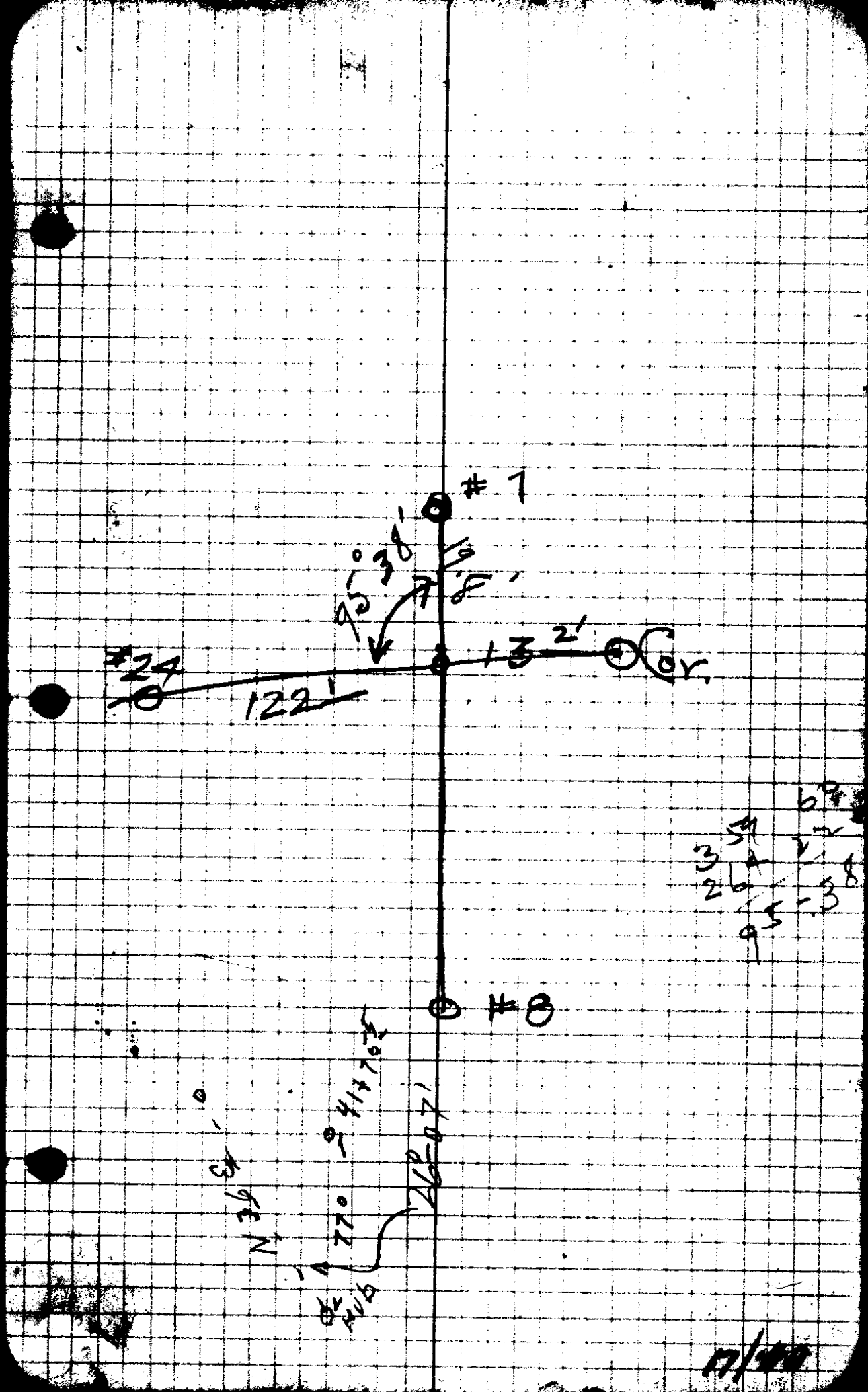
on Pipe set by Muller 3.55.5 feet from ^{lot} ₂

on line improve stake correct

on lot 1+2

11/100

Cl. Cor.	Dist	Angle	Slope	Cal Bear.	N Bear.
0					N86°E
	105.3			N86°E	
1	56.5	0°12'L		N85°48'E	N85°30'E
2	28.3 1.4	1°46'R	100' 28'	N87°34'E	East
3	82.6 25.4	1°58'L	34°20' 100'	N85°36'E	N87°15'E
4	¹⁰⁰ 281.9	78°58'L		N6°38'E	N7°E
5	173.3	8°30'R		N15°8'E	N15°30'E
6	87.6	77°29'R		S87°23'E	S87°30'E
7	65.6	30°38'L		N61°59'E	N61°30'E
8 P.D.					



6
 2
 2
 95-38
 7
 8
 6

11/10

not 17
1003 E

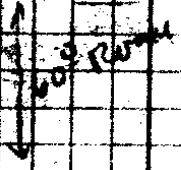
27

50

100

29

can for B&R 2



100

100

20
64
20
61
20
69.5
2.5

49.5
20
69.5

3/11/40 G.A.P.

Cont. to loc 56-31-32

B. 15° N 81° W 50'

B. 36° N 8° W 61.5'

B. 8° N 66° E 10'

W.O. 18° 15' N 53° W 12.5'

Recorded 7/2 E

cont

50 1/4 32

cont. study
old C. Tim Evidence

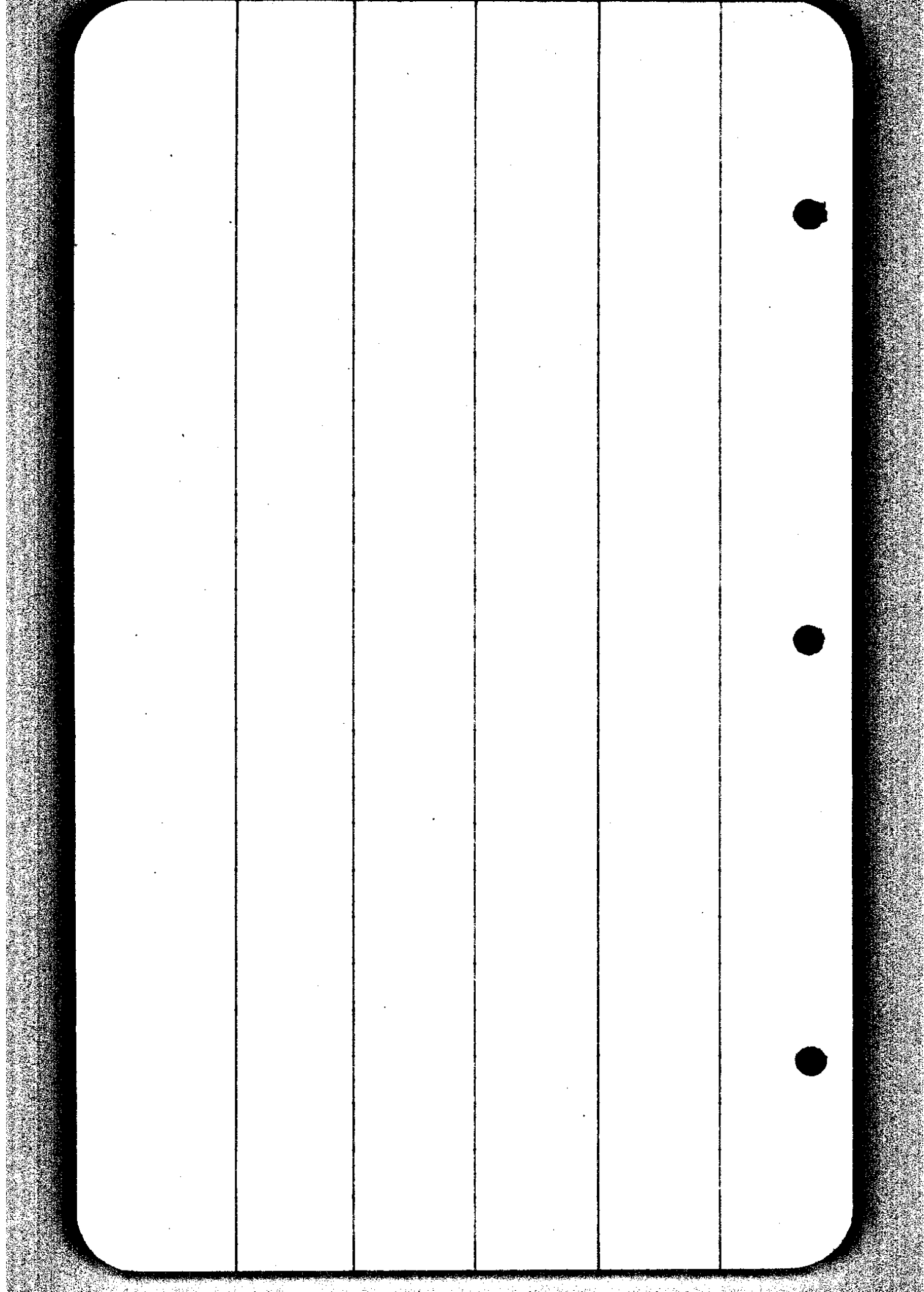
Marked 15' Alder
cont. 6. S 28° W. 369.

Recorded
- 18 E

R.P.

17/40

Turn Int L 90-18 from line west



17/480

at 25559 from NW Cor to my with
line

Δ 15 1326

Δ 9

2113

South 194.8 feet

Δ 8

1903

South 182.6 "

34490

Δ 7

South 171.6 "

3012.37

Δ 6

South 110.1

2963.97

1901.7

Δ 5

1106 192

1046

1°25' R S85W N89-12W

Δ 4

820

Δ 3

138 130

1345

Δ 2

1172 170

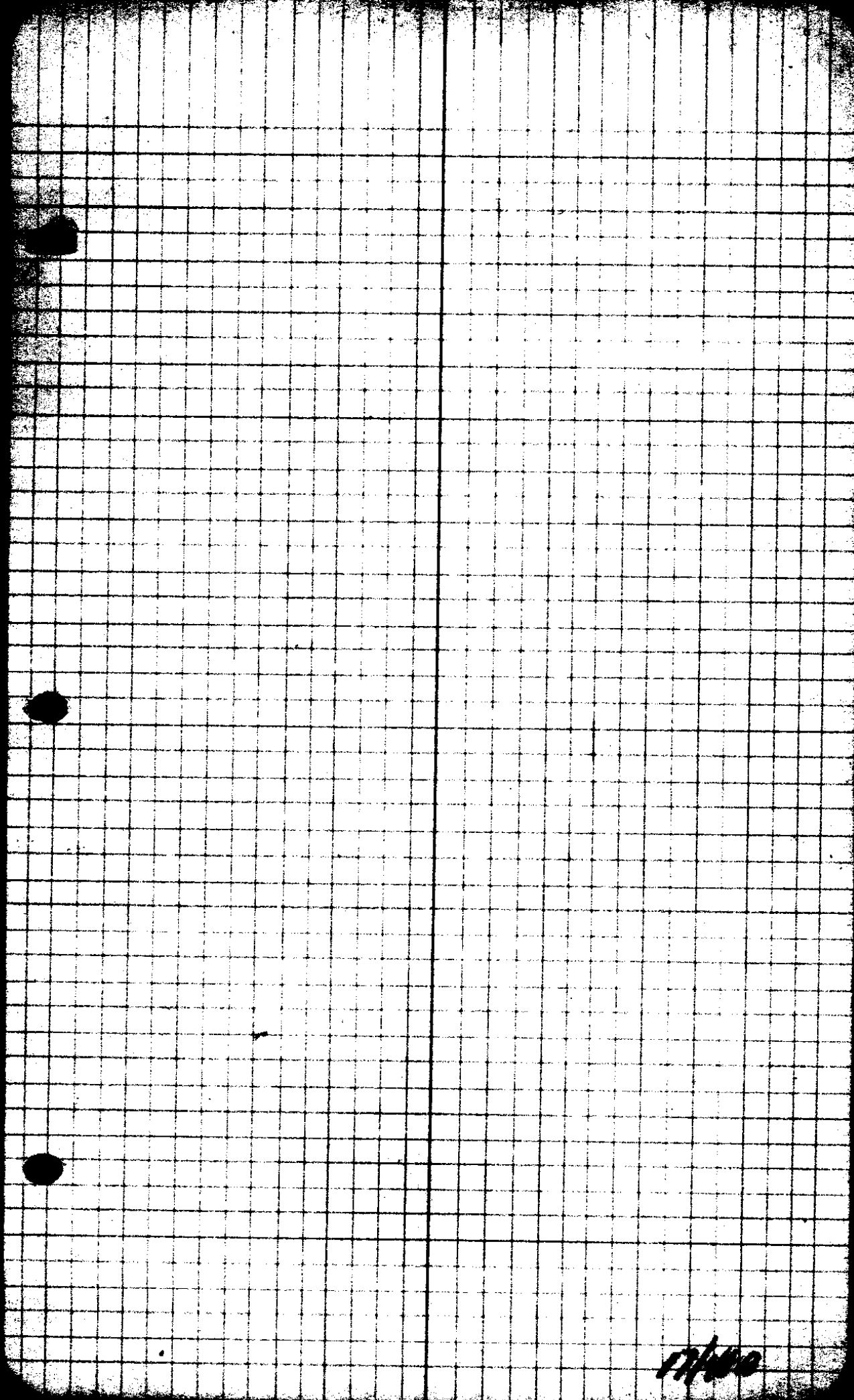
1116

1 Δ

40

S82-30W S89-43W

SE Cor
53



17/100

80

493.26

472.46

0.35

92.91