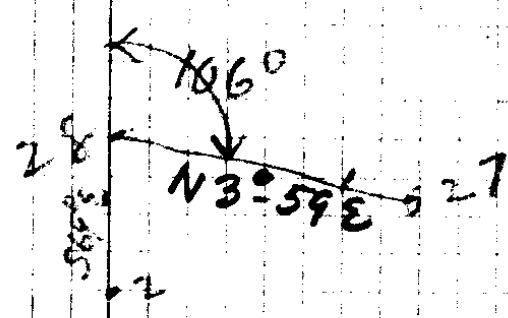


$$\tan A = \frac{10.2}{1320}$$

$$\begin{array}{r}
 1320 \overline{) 10.2000} \quad .0077 \\
 \underline{9240} \phantom{00} \\
 9600 \phantom{00} \\
 \underline{9240} \phantom{00} \\
 3600 \phantom{00} \\
 \underline{3600} \phantom{00} \\
 0000
 \end{array}$$

110  
 142  
 108



See Com

C. S. File No. 16/68

Page 1 - Vets Facility

$$\begin{array}{r} 964 \\ 956 \\ \hline 5784 \\ 4820 \\ 8676 \\ \hline 921584 \end{array}$$

$$\begin{array}{r} 125 \\ 21 \\ \hline 315 \end{array}$$
  

$$\begin{array}{r} 996 \\ 115 \\ \hline 4980 \\ 996 \\ 996 \\ \hline 114540 \end{array}$$

$$\begin{array}{r} 141.2 \\ 961 \\ \hline 1412 \\ 8472 \\ 12708 \\ \hline 1386932 \end{array}$$

$$\begin{array}{r} 1883^{\circ} 41' E \\ 4 \\ \hline N 87^{\circ} 41' E \end{array}$$

$$\begin{array}{r} 3710 \\ 66 \\ \hline 22260 \\ 22260 \\ \hline 24460 \end{array}$$

$$\begin{array}{r} 114.5 B \\ \hline \end{array}$$

$$\sin A = \frac{a}{c}$$

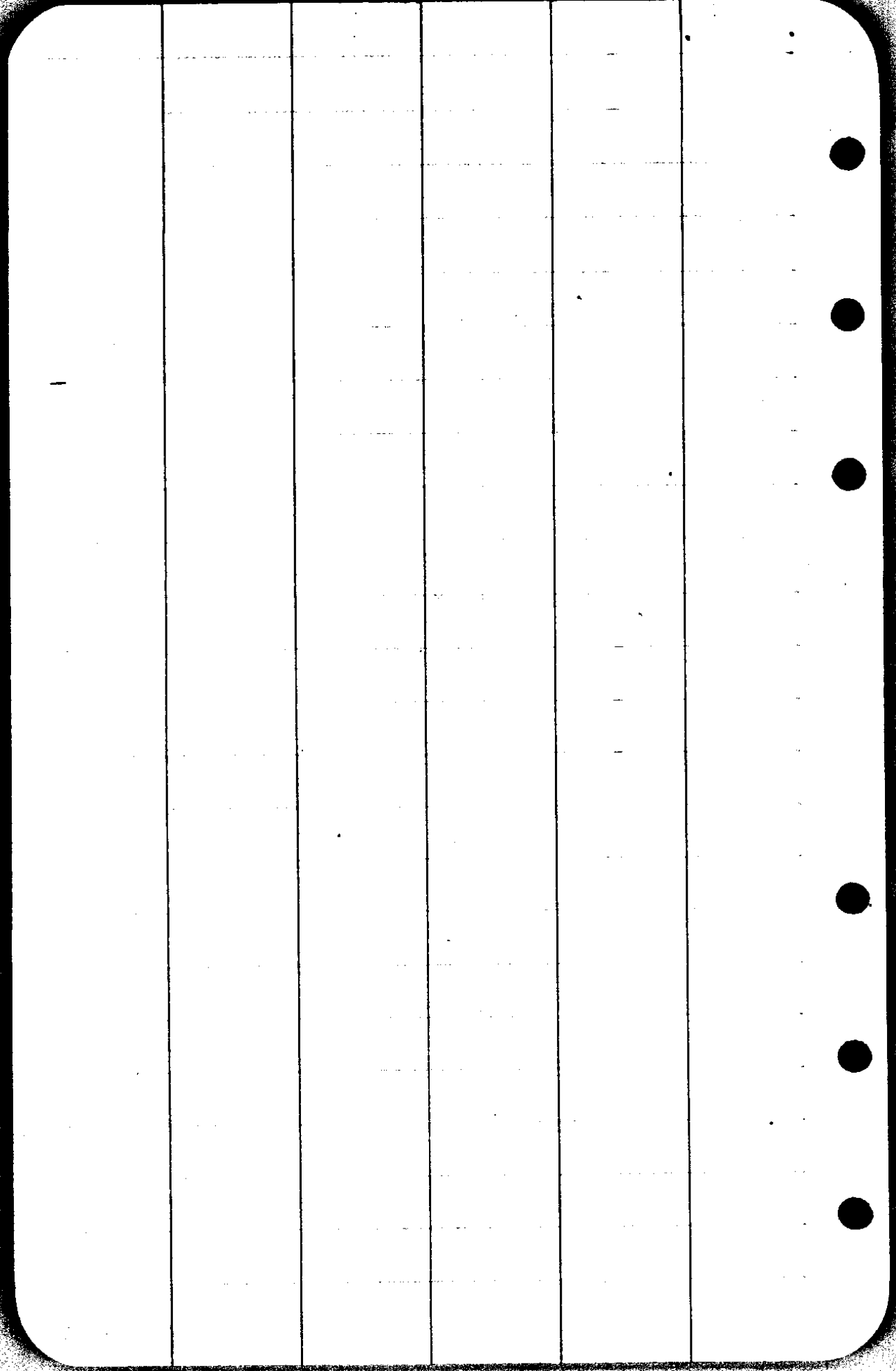
$$a = \sin A \times c$$

$$\begin{array}{r} 522 \\ 222 \\ \hline 2742 \\ 2872 \\ \hline 1507.3 \end{array}$$

$$\begin{array}{r} 1145 \\ 6697 \\ \hline 5015 \\ 10305 \\ 6870 \\ \hline 758065 \end{array}$$

$$\begin{array}{r} 1507.3 \\ 41.5 \\ 41.5 \\ 100. \\ 98.8 \\ \hline 10001 \end{array}$$

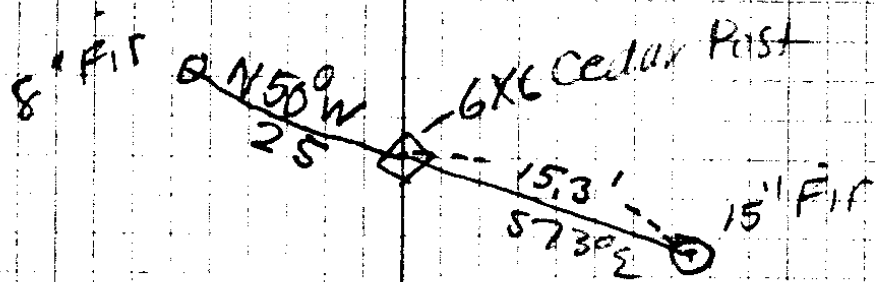
1888.7



Apr 23

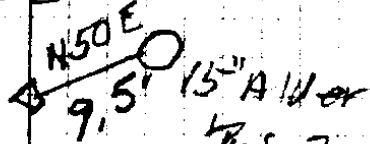
40

1/4 Cor bet 3 & 4  
T25/3



Apr 22

1/16 Cor  
E side  
SE 4 Sec 4



1/16 S 3  
T25 SR 3W  
LS 37

Apr 23

1/4 Cor  
S side Sec 4  
25/3

Square 6" Fir for Cor  
fr which

6" Fir - N 40° E 4'  
5" • S 82° W 7'

Apr 23

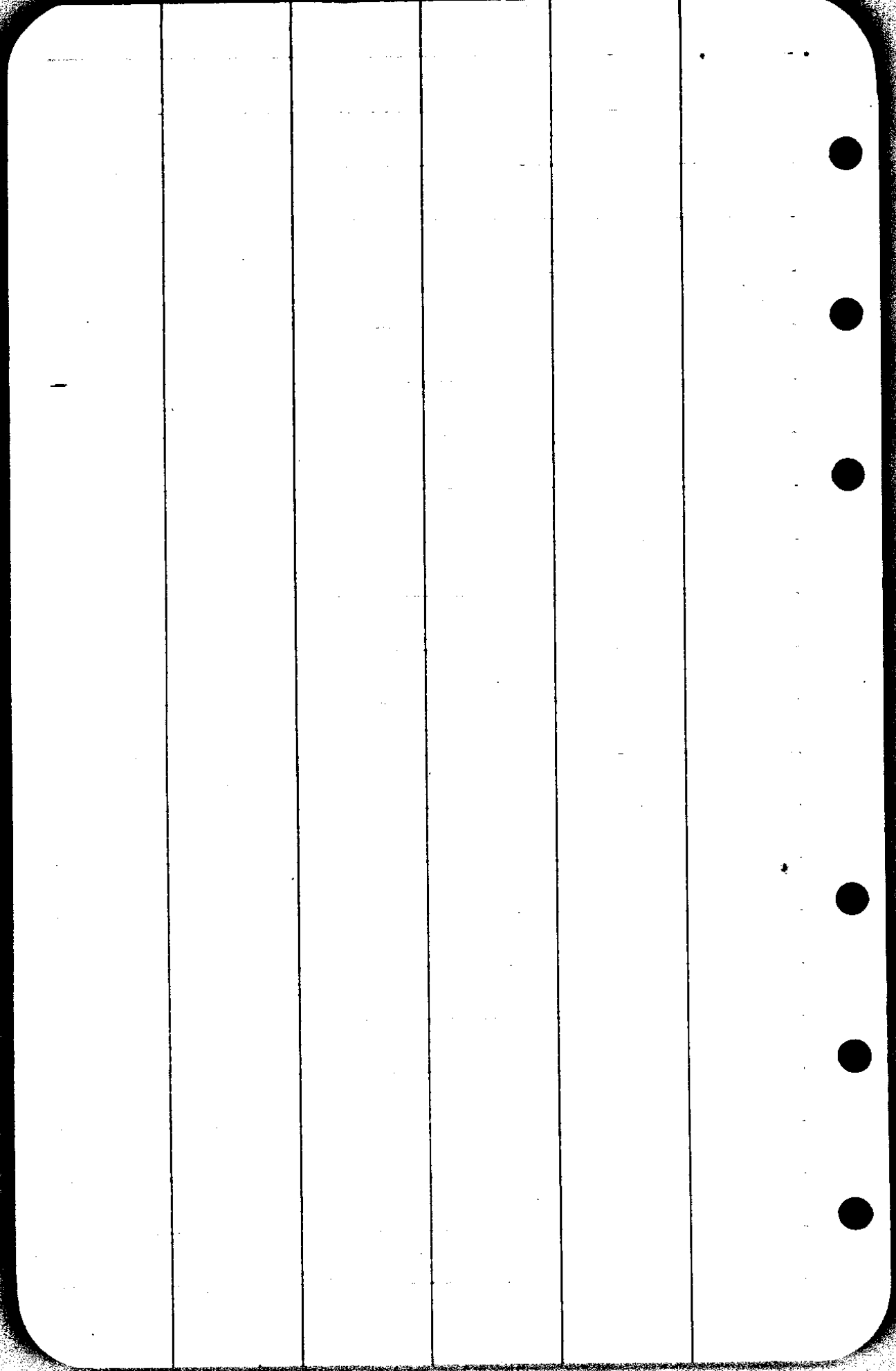
1/16 Cor = 4x4 Chink Post

on S side SE 4

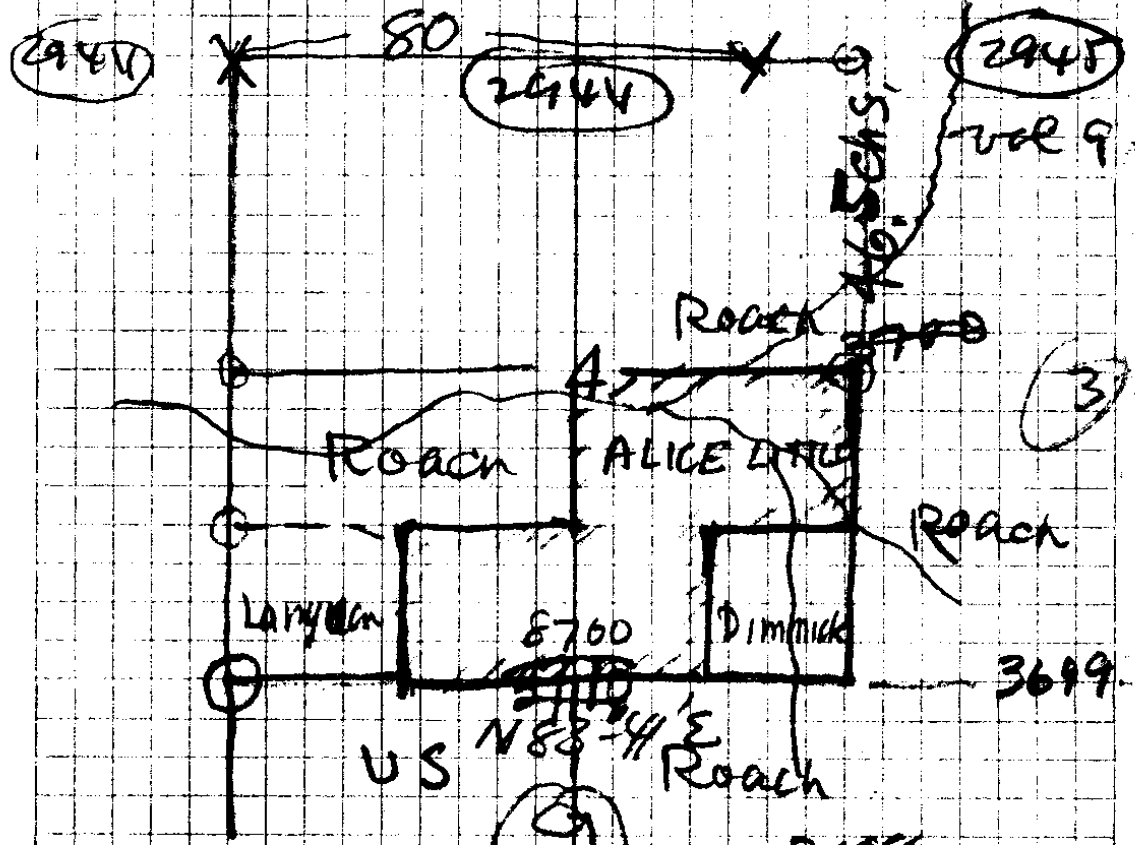
6" Fir white N 12° W 5'

1/16 Cor 3x3 Fir Post  
S side SW 4 Sec 4

6" Fir N 47° E 6.5' C. S. File No. 16/68



25/3



E bet 4 + 9 Random

3620 = 48" Fir

40

4735 30" Hem

W 40.31 = 1/2 new parr.

20" Fir  $\approx 16^\circ W$  43" Junco

10" "  $\approx 33^\circ E$  17" = 112"

n bet 9 + 10

70.15 = 24" Hem

80 = CW 349, 10.

5" Ced  $\approx 55^\circ E$  4" = 2.6

6" " S 31 E - 8 = 7.2

4" " S 69 W 8 = 7.2

6' "  $\approx 41^\circ W$  11 = 7.2

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n bet 3+4 Random  
~~S bet~~ 42, 33 = 40" Fir

S 10-24' W bet 3+4

3.8, 52 = Yew

6" Fir N 21° E 13 L

8" " N 73° W 72 L

En true Lincolns

Blug 32

32, 50 = Creek

40 = Yew

80 = sec cor 4, 5, 32, 33

16" ced N 60° E 13 L

24" " S 60° E 9 L

12" " S 80° W 17

16" Fir N 75° W 19 L

S Line 33-

5 Chs = good spruce

~~2m S Bay 34~~

~~70 = Spring~~

~~80 = cor, 2, 3~~

66  
44  
32  
26  
3036

56  
26  
336  
216

$$\begin{array}{r}
 144.6 \\
 \underline{989} \\
 13014 \\
 11568 \\
 \underline{13014} \\
 143.0094
 \end{array}$$

$$\begin{array}{r}
 1339 \\
 \underline{992} \\
 2678 \\
 12051 \\
 \underline{12051} \\
 1528.288
 \end{array}$$

$$\begin{array}{r}
 924 \\
 \underline{54} \\
 3696 \\
 4620 \\
 \underline{49896}
 \end{array}$$

$$\begin{array}{r}
 948 \\
 \underline{158} \\
 7584 \\
 4740 \\
 948 \\
 \underline{149784}
 \end{array}$$

The Grand

Em line line (S line 33)

74, 75 = creeks + 450  
3 lines

80 = ca 34, 33, 34

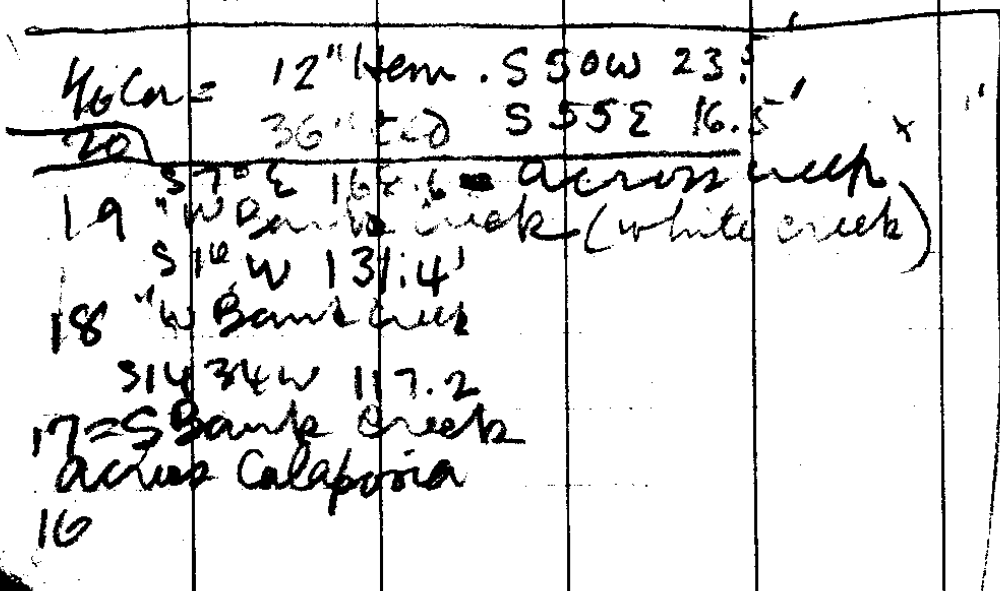
- 30" Fir N 52 E 10
- 8" " S 50 E 45
- 36" " S 5 W 56
- 24" " N 40 W 56

W 4 ca 4 = 1.5 N of # 11 + 111.5 W

S 1/6 ca (W side 4) 10' N of 18 + 102' W

S 4 ca Sec 5 = 36" Fir N 45 W 22'  
18" " S 26 E 12'

Corner is abt 509' n of trail xing



118.3  
140.8  
144  
106  
-----  
509'

7/8 Pine 2 1/2 long 40 (8)  
 96

88.3  
 959  
 7947  
 4415  
 7947  
 84.6797  
 984 3  
 207  
 6888  
 1968  
 203688  
 26116  
 947  
 18312  
 23544  
 23544  
 2608152  
 4984  
 1854  
 4990  
 7984  
 494  
 174635  
 839 2  
 114 (3)  
 3356  
 839  
 839  
 95.646  
 1895 4  
 538 3  
 7160 (1)  
 2685  
 4475  
 48.1510

N 130 41 W  
 2-33  
 11-76  
 4-40  
 6-36  
 19-29  
 20-05  
 32-15  
 52-20  
 32-30R  
 N 19 50 W  
 16-39 R  
 9-11  
 130 70  
 10  
 90-11  
 3-59

1444.6 136  
 154.7 96  
 64.9  
 53.6 232  
 79.3 40  
 290.7 272  
 22 96.8  
 2086.9 368.6  
 199.7  
 2286.6 55  
 58  
 110  
 55  
 145  
 125  
 290  
 246  
 364.6  
 64 ✓  
 62  
 5285.92 = 27940, 93881 126 ✓  
 1522 = 623104.00 62  
 2796384281 188  
 62  
 250  
 62  
 312  
 62  
 314 ✓  
 62 ✓  
 436 ✓  
 100  
 536  
 100  
 636

16-65 S. Flis N 6/68

(9)

Job 24

(29) 2

S 69° E  
Δ 4-24 R

81.1 = 72.7  
26-15'  
897

S 70° E

S 74° E, 88.6 = 75.1  
32°  
848

S 74-24 E

(30) 1

Δ 7-45 L

S 66 1/2° E

1080 = 899  
34-2°  
824

S 66-39' E

(31)

Section

N 66 1/4

125.4 3  
 976 5  
 7524  
 8778  
 11286  
 1223004  
 645  
 972  
 2290  
 4515  
 5805  
 626940

951  
 121  
 951  
 2513  
 951  
 124581  
 798  
 5918  
 6384  
 7182  
 3990  
 477204  
 9098  
 57  
 6688  
 4720  
 53868  
 10787  
 944  
 4312  
 4312  
 9702  
 1017632  
 98.7  
 143.8  
 132.8  
 49.9  
 149.8  
 124.6  
 55.  
 47.7  
 53.8  
 101.7  
 54.  
 60.  
 96.1  
 1107.9  
 1223  
 1289.4  
 62.7  
 1352.1

108  
 72  
 26

150  
 26  
 150  
 150  
 7500  
 170  
 22500  
 676  
 23176 (1522)  
 131  
 2512  
 676  
 604  
 7200  
 6044  
 1156  
 1522  
 1522  
 3044  
 044  
 7610  
 1522  
 231644  
 1156  
 2317640

1352.1 302  
 925  
 14446 3022  
 7200  
 6044  
 1156

C. S. File No. 16/68

28 (N 40 E 132.2)  $\frac{31}{2} = 131.9$   
 27  $\Delta 13^{\circ}-10' R$   $995 = 48.1$   
 N 9<sup>o</sup> W 53.8  $(26\frac{1}{2})$  N 9<sup>o</sup>-11' W  
 26  $\Delta 10^{\circ}-39' R$   $951 = 83.9$   
 N 20<sup>o</sup> W 114.0  $(33)$  N 19<sup>o</sup> 50' W  
 25  $\Delta 32^{\circ}-30' R$   $265.3$   
 N 52<sup>o</sup> W 287.0  $(19^{\circ}-4)$  N 52<sup>o</sup>-20' W  
 24  $\Delta 32^{\circ}-15' R$   $184.6$   
 N 19<sup>o</sup> 2' W 185.0  $(3^{\circ}-00)$  N 20<sup>o</sup> 05' W  
 23  $\Delta 13^{\circ}-29' L$   $997 = 260.8$   
 N 6<sup>o</sup> W 261.6  $(4030)$  N 6<sup>o</sup>-36' W  
 Marked at 21  
 22 = 2280.6 N  $\Delta 4^{\circ}-40' R$   $203.1$   
 N 11<sup>o</sup> W 207.0  $(10^{\circ}-20)$  N 11<sup>o</sup>-16' W  
 21 =  $\Delta 2^{\circ}-33' R$   $299.4$   
 N 13<sup>o</sup> W 300' 3<sup>o</sup> vert  $299.4$  N 13<sup>o</sup> 49' W  
 20  $\Delta 34^{\circ}-14' L$   $88.3$   $16\frac{1}{2} = 84.7$   
 N 20<sup>o</sup> 2' E  $88.3$   $16\frac{1}{2}$  N 20<sup>o</sup>-25' E  
 19 = Top Rim Rock  $\Delta 20^{\circ}-25' R = 1716.9$   
 53.6 F  
 18 = 1663.3  
 79.1  $36^{\circ}$  64.0  
 17 1599.3  
 Under Roof N 164.6  $20^{\circ}$  154.7'  
 16 = 1444.6  $940$



⑦	16 = 1444.6	95.6	$14\frac{1}{2}^{\circ}$	92.5
	15- Creek = 1352.1		$96\frac{1}{4}^{\circ}$ North of SE cor	
		64.5	$13\frac{1}{2}^{\circ}$	62.7
	14		972	
		125.4	$12\frac{1}{2}^{\circ}$	122.3
	13 = 1167.1			
		96.1	F	
	12 wed AM			
		66.0	F	
	11 Marked "10"			
		54.0	Flat	
	10			
		107.8	$19\frac{1}{4}^{\circ}$	101.7
	9- 0.5' E of Line		from here	
		57 $^{\circ}$	$19\frac{1}{4}^{\circ}$	53.8
			944	
	8			
		59.8	$37^{\circ}$	47.7
			798	
	7 = R Bank River			
		55.0	F	55.0
	6 = L Bank Catapodia River			
		131.0	180.00'	124.6
			.951	
	5 =			

814  
970  
 56980  
7326  
 78.9580

165.8  
570  
 116060  
14922  
 1608260

134.5  
992  
 2190  
 9855

720240

155.8  
354

4022  
 264  
14022

154.0862

5585  
1296380

114  
107

1308  
970

8130  
6875  
 12195

7060  
8340

1558  
 4640.5  
 165.5  
 114.3  
 108.5  
 88.4  
 78.9  
 160.8  
 108.6  
 154

585.5

5585.5  
1296

5715.1  
 204

5700  
 5700

5742  
5585  
 157.  
 1296  
 284

North & S Line

⑥ 5	from here	1.5' w. offset :	
	158.0	32° .948	149.8
4	54.0	22½° .924	49.9
3.	133.9	7' 00" .992	132.8
2	144.6	8½° .989	143.0
1			
N	100.4	9° .987	98.7'

Sec Cor.  
Running N to # 62

NOTE 17.0'  
sec →

# 62	N & S blazed line	= 6101' 238
61		
	E	80.7
60	E	123.3
59	E	29.7
58	E	128.9

57 → Buy Apr 16 - '40 - moved 1.0'S  
5915.1



(5)

SWT

~~58~~ 574.5 = ~~END~~ SWT Apr 13

~~264~~

57 = 5715.1

135.5 17° 129.6

56 = 5585.5

956

ACROSS CR

155.8 8-30' 154

55

109.5 7-20' 108.6  
9-2

54

165.8 140 160.8  
970

53

81.4 140 78.9  
970

52

48.4

51

ACROSS CR

108.5

50

114.3

49

15

165.5

48 = 4646.5

238 @ 48

SWT APR 13 1948

103.6  
445  
- 180

9824  
9324

10308

978  
893

2934  
8802  
7824

873354

995  
977

6965  
6965  
8955

972118

1716  
243  
- 148

15444  
15444  
1703288

997  
168  
8973  
- 1612  
- 865

168493

1888.7  
67.7  
93  
31.5  
73

77.  
103.1  
7112  
87.3  
97.2  
1668  
53

2756.5

45742  
2871  
2756  
115

485

④ 47

E 106.4 F

46

E 161.1 F

45

E 2.0 F

44

N67°E 39.5 F

43

S85°E 39.5 F

Δ 15° R

E 613 F

42

Δ 4° R

N74°E 51.1 F 509

41

Δ 8° L

N85°E 51.1 F 509

40

Δ 4° R

70.5 F

39

180.7 5°30' 925 179.8

38

119.4 8°00' 925 118.2

37

115.7' F

36

N72°E 57.4' 56.5

47 46 45 44 43 42 41 40 39 38 37 36



(3)

54 210 300 4  
Lunch  
53  
Lunch  
52  
Lunch  
51  
Lunch  
50  
Lunch  
49  
Lunch  
48  
Lunch  
47  
Lunch  
46  
Lunch  
45  
Lunch  
44  
Lunch

35	$\Delta 20^\circ L$			
	N	57.4	F	56.5
34	$\Delta 10^\circ R$			
		169	$5^\circ 00'$	.997 168.4
33	E Side Trail (to N)			7' job trail
		41.7	F	
32	W Side Trail			
		210.7	F	
31				
	E	171.6		$6^\circ 45' = 170.4$
30		2756.5		.993
		166.8	F	75' E { E side road
29				
		97.7	$5^\circ 50'$	.995 97.2
28				
		89.3	$12^\circ 00'$	87.3
27				
		71.2	F	
26	(25 South)			
		103.6	$5^\circ 30'$	103.1
25				
		77.0	Flat	
24	(offset 28' S)			
	E	73.0	F	

Tuesday Apr.

1940 Bayer Darby (1)

54.1	1
97.2	
46.	1
92.3	5
184.0	4
111.	3
149.5	7
50.6	2
50.7	3
80.	5
<hr/>	
915.4	1
140.9	5
104.8	4
92.1	3
113.4	
<hr/>	
1366.6	
135.7	
<hr/>	
1502.3	

87	859	4
66	63	
<hr/>		
522	2577	
522	5159	
<hr/>		
45742.	54717	
<hr/>		
1435.5	108.2	2
	895	2
	<hr/>	
	8656	5
1435	9738	
982	8656	
<hr/>		
2870	971634	
11480		
12915	97.7	5
<hr/>		
1409170	945	
	<hr/>	
	4885	
971	3908	
105	8793	
<hr/>		
7768	923265	
971		
<hr/>		
104868	193.5	
	951	
	<hr/>	
	193.5	
	9675	
<hr/>		
	17415	
	1840185	
	<hr/>	
	1937	
	54	
	<hr/>	
	3748	
	4655	
	<hr/>	
	50598	

2000 ft (approx)

② 23

31.5 F

31.5

22

93.0 F

93.0

21

81.0  $33^{\circ}15'$   
836

67.7

20 = 1888.7 V

109.5  $16^{\circ}15'$   
960 = 105.1

19

2' South

106.6  $22^{\circ}$   
927 = 98.8

18

123.6  $26^{\circ}$   
909 = 100.0

17 Top hill just W. of Creek (abt 125')

44.0  $21^{\circ}10'$   
932 = 41.0

16 ← Line 1.0' N from here  
Hub Left Loose here tack in ground at

41.5 F

15 = 1502.3 ✓

141.2  $16^{\circ}$   
961 = 135.7

14 2' N from here - 42" Fir on 1000

115.0  $5^{\circ}$   
970 = 113.4

13

$\Delta 4^{\circ} R$

95.6  $15\frac{1}{2}^{\circ}$   
964 = 92.1

12 Blazed (old) tree 6 N

32	33	34	35	36
5	4	3	2	1

n bet 3 + 4

21, 3 = Brook c SW 2 Lins

26, 5 = ridge

40 -- cor

42, 33, (40" Fir)

50, 25 = Brook

54, 20 = Brook

60, 31 = Fir 40"

205
60
17.30
12.30
13.530

28, 52 = (Cor is 205 Lins & E)

(3, 4, 33, 34)

Removal

30" Fir n S 2 E 10 51

8" " S 50 E 46-30.3

36" " S 5 W 56 40"

3' E of this  
4" Fir

~~24"~~ " n 40 W 56 ~~34~~

4" Fir S 31 E 13 35

EAST (erly) S Line Sec 4, (Rand) (m)

12	108.0	13° 45'	1048	
11		.971		
	1435	110°	140.9	
		.982		
10	915.4	Offset in from 10 Eastly		
	80.0	R	80.0	
9				
	50.7	F	50.7	
8				
	54.0	26 1/2°	937	50.6
7	41R			
	149.5	F	149.5	
6				
	111.0	F	111.0	
5				
	193.5	18°	957	184°
4				
	97.7	19°	945	92.3
3				
	46.0	F	46.0	
2				
	108.2	26°	898	97.2
1				
	63.0	30° 45'	859	54.1
	Sec cal			

CS FILE FOLDER

CONTAINS

MORE

INFORMATION