

Myrtle Creek
School Grounds
Levels & Topography

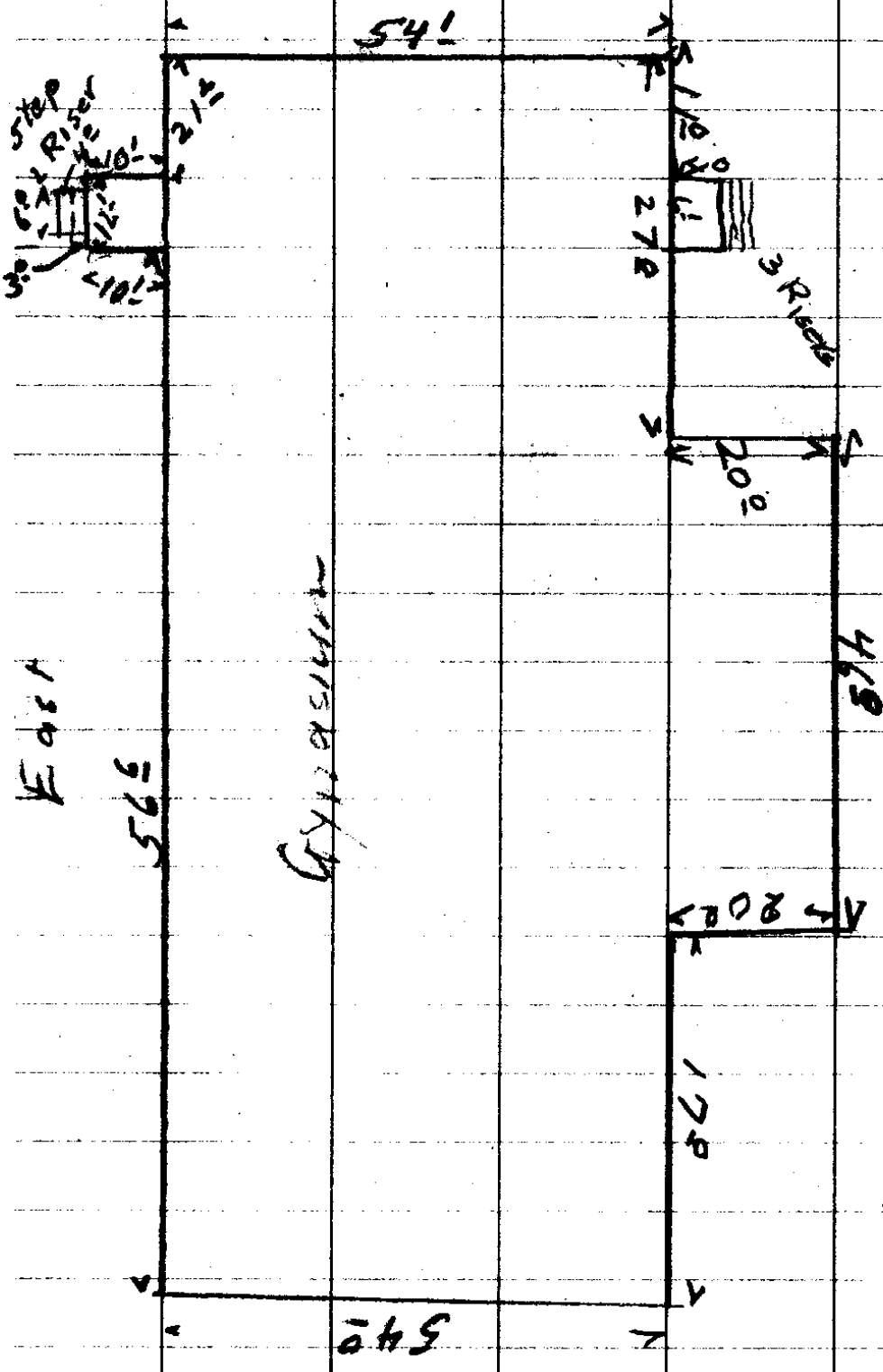
I

15-22

June 1938

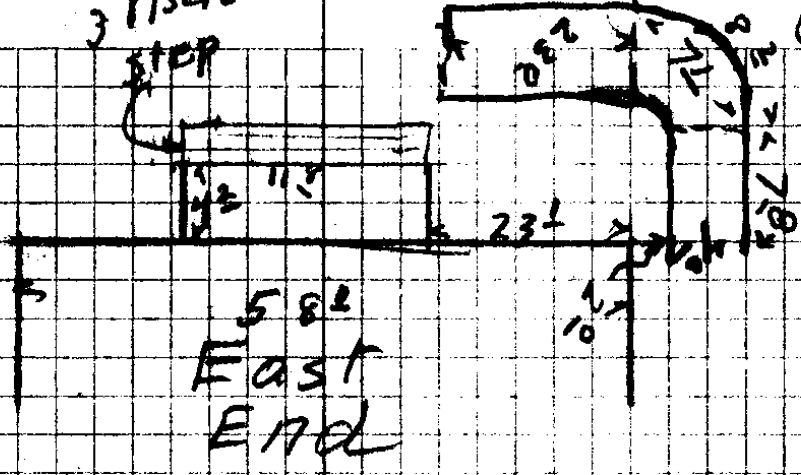
Eppstein
N.E. Richardson
Eppstein Jr.
Lane
Sellers
Shirtcliff
Dyer

5

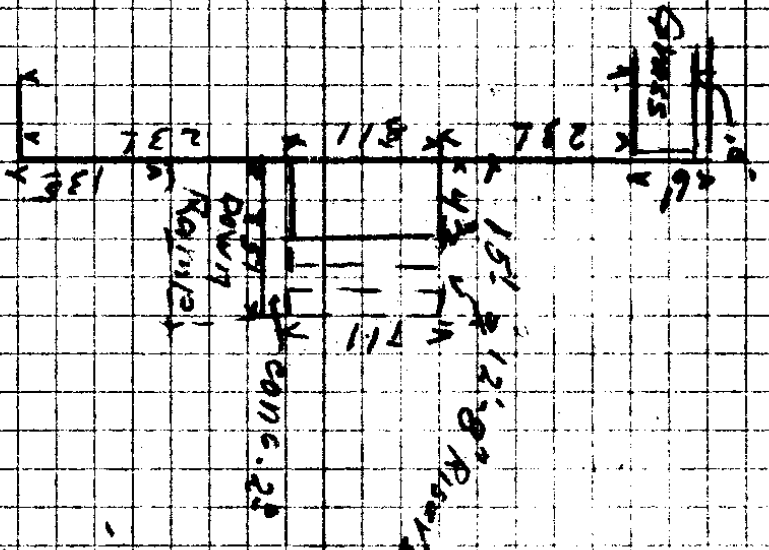


3 RISERS
STEP

(5)



582
East
End



West End.

C. S. File No. 15/72

31.4
24.7
13.7

75.6

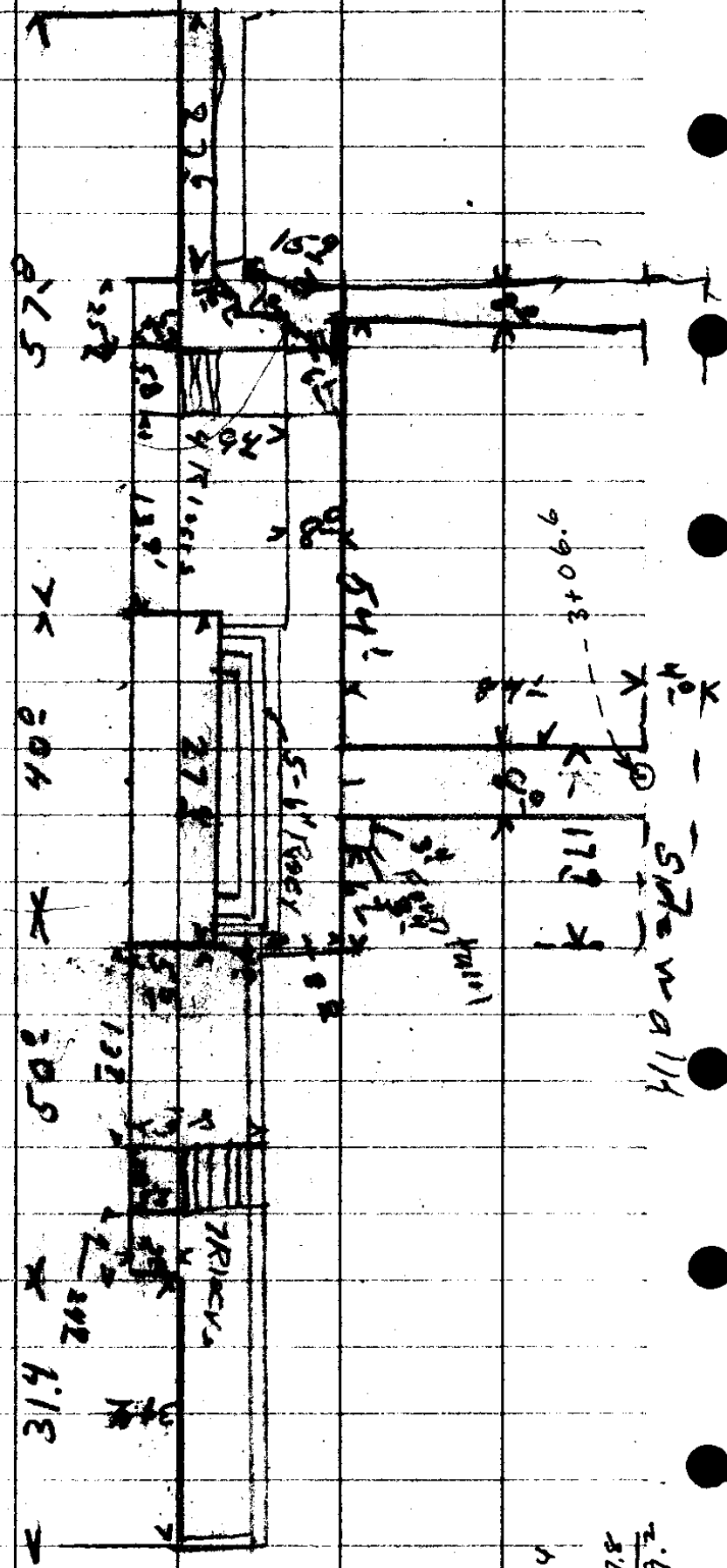
90
37.9
31.4

79.2

135.9
25.7

161.6

FRONT.



31.4
50
40
57.8

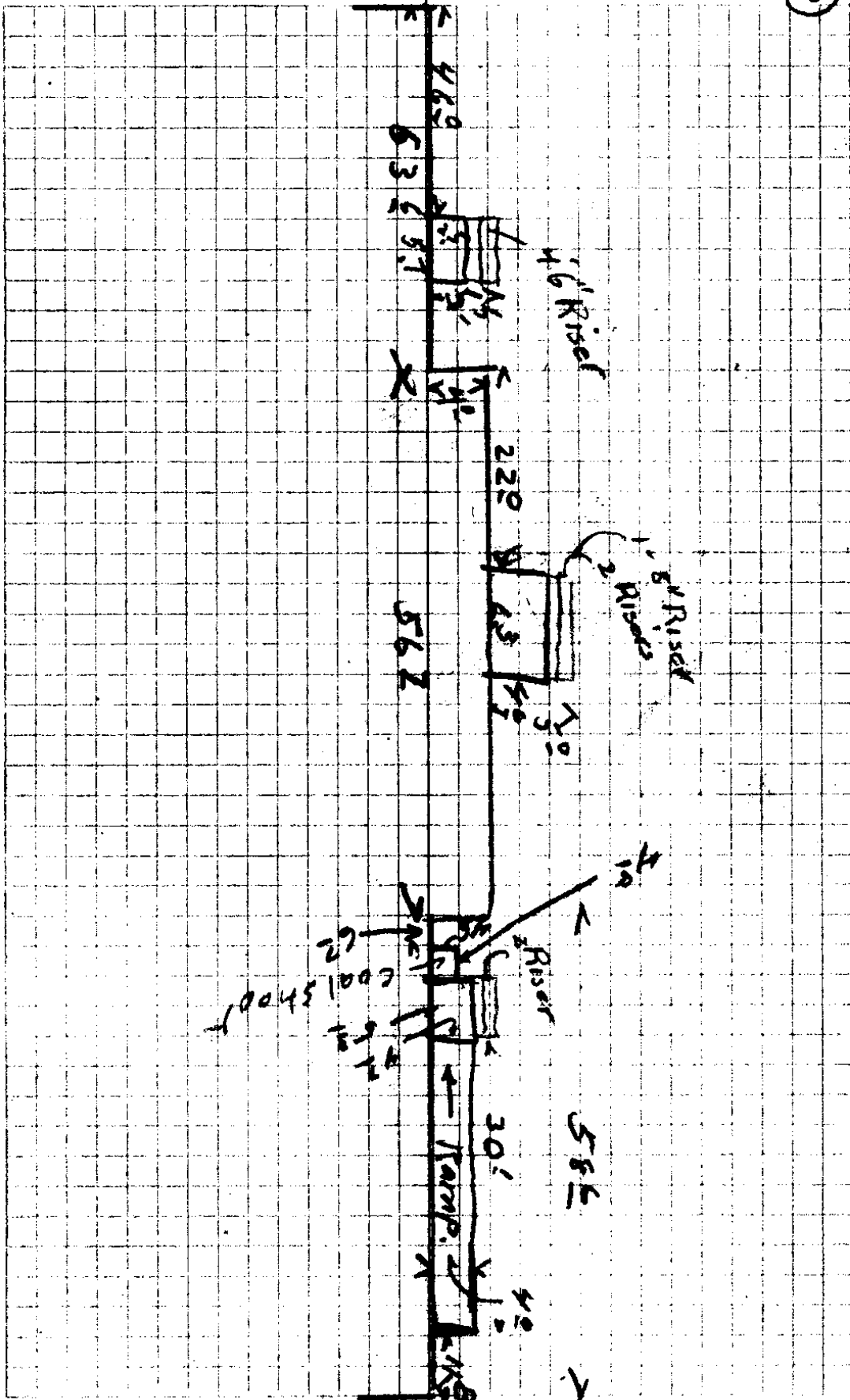
179.2

570 WALL

3+06.6

5

6



11.8
 30.1
 6.3
 4.8
 6.7
 54.7

C. S. File No. 15/22

7 Street to North

0.52 North Line
+ 1.0 + 2.6 06.6

D0+00

+ 2.5

+ 3.0

704.2
C

D0+50

+ 1.0
2.5

+ 3.0
5.0

07.0
C

D1+00

713.4
+ 2.8
3.3

714.4
+ 3.8
5.0

710.6
C

D1+50

715.6
+ 2.0
2.8

717.6
+ 4.0
5.0

13.6
E

D2+00

718.9
+ 2.3
2.5

721.5
+ 4.9
5.0

16.6
C

D2+50

722.6
+ 2.7
2.5

725.5
+ 5.6
5.0

19.9
C

D3+00

724.5
+ 2.3
2.5

727.8
+ 5.6
5.0

22.2
C

D3+50

724.6
+ 2.6
2.5

728.0
+ 6.0
5.0

22.0
C

D3+72

724.7
+ 2.2
2.5

726.8
+ 6.3
5.0

22.0
C

D4+00

725.6
+ 2.8
2.5

729.6
+ 6.8
5.0

22.8
C

D4+50

728.1
+ 4.4
2.5

728.1

24.1
C

D5+00

726.1
+ 4.8
2.5

726.1

721.3
C

5

cont.

D5+50	+4 ⁰ 25	721 ²		717 ² C
D6+00	+8 ⁸ 35	722 ³		717 ⁵ C
D6+45	+5 ² 35	721 ⁰		718 ⁸ C

North east corner

XXXXXX
A Line

A0+00	684 ⁴ +9 ⁹ 180	683 ⁴ +8 ⁸ 150	679 ² +5 ² 100	687 ² +3 ⁶ 50	674 ⁵ C
A0+50	688 ¹ +10 ⁶ 180	686 ² +8 ⁵ 150	683 ² +5 ⁵ 100	680 ³ +2 ⁸ 50	77 ⁵ C
A1+00	690 ⁶ +9 ⁴ 180	689 ⁸ +7 ⁷ 150	685 ⁴ +4 ² 100	683 ⁴ +2 ² 50	81 ² C
A1+50	693 ⁶ +9 ⁰ 180	692 ¹ +7 ⁵ 150	689 ³ +5 ² 100	686 ² +2 ³ 50	84 ⁶ C
A2+00	692 ² +10 ² 180	693 ⁴ +7 ⁴ 150	690 ² +6 ³ 100	688 ² +1 ² 50	86 ⁷ C
A2+50	694 ⁵ +10 ² 180	694 ⁵ +6 ³ 150	691 ² +5 ² 100	689 ¹ +0 ⁵ 50	88 ⁹ C
A3+00	698 ⁵ +7 ⁵ 930	697 ³ +6 ³ 75	694 ³ +3 ⁸ 50	693 ⁰ +2 ⁰ 25	91 ⁰ C
A3+06 ² sidewalk	698 ² +7 ⁵ 930	697 ⁸ +6 ⁴ 75	694 ³ +4 ¹ 50	693 ⁵ +2 ¹ 25	91 ² C

673 ⁸ - 0.7 63	671 ⁶ - 2.9 150	672 ⁴ - 2.4 28	671 ⁵ - 3.0 30
677 ⁹ - 0.5 70	674 ³ - 3.2 702	674 ⁷ - 3.0 24	677 ⁶ - 3.6 50
680 ² - 0.3 73	677 ⁶ - 3.6 706	678 ² - 3.2 250	680 ⁹ - 3.7 500
684 ⁴ - 0.2 62	681 ² - 3.4 102	681 ² - 3.4 6	683 ² - 3.4 50
686 ¹ - 0.6 65	684 ¹ - 2.6 97	684 ¹ - 2.5 25	686 ³ - 2.6 50
688 ⁴ - 0.6 73	686 ⁵ - 2.4 104	687 ⁴ - 1.8 23	686 ⁶ - 2.4 50
690 ⁸ - 0.2 60	688 ⁷ - 2.3 108	688 ⁷ - 2.3 24	686 ⁶ - 2.4 50
690 ² - 0.3 62	688 ² - 2.3 10	688 ¹ - 2.5 25	686 ⁶ - 4.6 50

	S.W. ENH	LC	T	695.3	
A3+50	700.5 +12.1 <u>712.6</u>	699.1 +8.2 <u>707.3</u>	697.6 +6.8 <u>704.4</u>	695.3 +4.5 <u>700.8</u>	690.8 C
A4+00	696.4 +7.7 <u>704.1</u>	699.8 +11.4 <u>711.2</u>	698.2 +10.3 <u>708.5</u>	694.2 +6.5 <u>700.7</u>	883 C
A4+50	693.8 +5.6 <u>700.4</u>	696.1 +7.2 <u>703.3</u>	694.9 +5.9 <u>700.8</u>	691.9 +2.9 <u>700.2</u>	890 C
A5+00	85+00 691.5 +5.2 <u>696.7</u>	693.2 +5.0 <u>698.2</u>	691.7 +3.5 <u>695.2</u>	689.6 +1.4 <u>691.0</u>	883 C
A6+00	85+50 694.0 +8.2 <u>702.2</u>	690.5 +4.2 <u>694.7</u>	689.4 +2.9 <u>692.3</u>	687.8 +1.2 <u>689.0</u>	865 C
A6+50	699.1 +8.3 <u>707.4</u>	692.3 +6.2 <u>698.5</u>	689.2 +4.2 <u>693.4</u>	687.2 +1.5 <u>688.7</u>	849 C
B0+00	693.3 +9.2 <u>702.5</u>	691.5 +7.5 <u>699.0</u>	688.1 +4.8 <u>692.9</u>	686.3 +2.9 <u>689.2</u>	857 C
B0+50	696.5 +8.2 <u>704.7</u>	695.3 +7.6 <u>702.9</u>	692.6 +4.9 <u>697.5</u>	690.2 +2.5 <u>692.7</u>	888 C
B1+00	699.1 +8.2 <u>707.3</u>	697.7 +7.2 <u>704.9</u>	694.6 +4.2 <u>700.8</u>	692.5 +2.0 <u>694.5</u>	905 C

B line

684.5 688.1 Right 685.6 (9)

$\frac{-2.3}{2.6}$	$\frac{-2.7}{2.5}$	$\frac{-5.2}{5.0}$				
6869	6874	6850				
$\frac{-2.1}{4.5}$	$\frac{-1.2}{2.5}$	$\frac{-3.4}{5.0}$				
6862	6863	6854				
$\frac{-2.1}{4.5}$	$\frac{-1.7}{2.5}$	$\frac{-3.6}{5.0}$				
6862	6869	6874	6868		6852	
$\frac{2.2}{3.2}$	$\frac{1.3}{1.6}$	$\frac{-0.8}{2.5}$	$\frac{-1.4}{4.3}$	$\frac{-3.2}{5.0}$		
6854	6851	6862	6873	6863	6841	683.9
$\frac{-1.9}{3.0}$	$\frac{-1.4}{1.5}$	$\frac{1.0}{2.0}$	$\frac{1.0}{2.0}$	$\frac{1.0}{2.0}$	$\frac{-2.4}{4.3}$	$\frac{-2.6}{5.0}$
683.8	6869	6874	6874	6862	6874	
$\frac{-1.1}{1.7}$	$\frac{1.2}{2.0}$	$\frac{1.2}{2.5}$	$\frac{1.2}{2.5}$	$\frac{1.2}{2.5}$	$\frac{1.2}{2.5}$	$\frac{1.2}{2.5}$
6842	6845	687.2	687.5	687.0	683.7	6837
$\frac{-1.5}{9.0}$	$\frac{-1.2}{1.6}$	$\frac{1.5}{2.1}$	$\frac{1.9}{2.5}$	$\frac{1.3}{3.9}$	$\frac{-2.2}{4.5}$	$\frac{-2.0}{5.0}$
6864	6866	6884	6882	6889	6849	6864
$\frac{-2.0}{5.2}$	$\frac{-1.8}{1.4}$	$\frac{0.0}{2.0}$	$\frac{0.0}{2.5}$	$\frac{-0.4}{4.1}$	$\frac{-2.4}{4.6}$	$\frac{-2.2}{5.0}$

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	701.9	701.0	701.5	695.0	
B1+50	$\begin{array}{r} 701.9 \\ + 8.5 \\ \hline 170 \end{array}$	$\begin{array}{r} 701.0 \\ + 7.9 \\ \hline 150 \end{array}$	$\begin{array}{r} 701.5 \\ + 5.2 \\ \hline 100 \end{array}$	$\begin{array}{r} 695.0 \\ + 51.7 \\ \hline 50 \end{array}$	$\frac{693.1}{C}$
B2+100	$\begin{array}{r} 705.3 \\ + 9.1 \\ \hline 170 \end{array}$	$\begin{array}{r} 703.9 \\ + 7.2 \\ \hline 150 \end{array}$	$\begin{array}{r} 701.5 \\ + 5.2 \\ \hline 100 \end{array}$	$\begin{array}{r} 699.1 \\ + 3.4 \\ \hline 50 \end{array}$	$\frac{96.2}{C}$
B2+50	$\begin{array}{r} 704.1 \\ + 5.3 \\ \hline 170 \end{array}$	$\begin{array}{r} 704.1 \\ + 5.3 \\ \hline 150 \end{array}$	$\begin{array}{r} 704.6 \\ + 5.8 \\ \hline 100 \end{array}$	$\begin{array}{r} 702.8 \\ + 4.0 \\ \hline 50 \end{array}$	$\frac{98.8}{C}$
B3+00	$\begin{array}{r} 706.1 \\ + 5.8 \\ \hline 170 \end{array}$	$\begin{array}{r} 705.7 \\ + 5.4 \\ \hline 150 \end{array}$	$\begin{array}{r} 704.3 \\ + 4.0 \\ \hline 100 \end{array}$	$\begin{array}{r} 702.2 \\ + 1.2 \\ \hline 50 \end{array}$	$\frac{700.3}{C}$
B3+50	$\begin{array}{r} 705.5 \\ + 5.1 \\ \hline 170 \end{array}$	$\begin{array}{r} 705.1 \\ + 4.2 \\ \hline 150 \end{array}$	$\begin{array}{r} 702.2 \\ + 1.5 \\ \hline 100 \end{array}$	$\begin{array}{r} 700.5 \\ + 0.1 \\ \hline 12.5 \end{array}$	$\frac{700.4}{C}$
B					
B4+50	$\begin{array}{r} 701.5 \\ + 4.2 \\ \hline 170 \end{array}$	$\begin{array}{r} 699.2 \\ + 3.1 \\ \hline 150 \end{array}$	$\begin{array}{r} 697.6 \\ + 1.0 \\ \hline 100 \end{array}$	$\begin{array}{r} 696.6 \\ + 0.8 \\ \hline 50 \end{array}$	$\frac{696.6}{C}$
B5+00	$\begin{array}{r} 700.3 \\ + 6.2 \\ \hline 170 \end{array}$	$\begin{array}{r} 699.2 \\ + 5.6 \\ \hline 150 \end{array}$	$\begin{array}{r} 696.7 \\ + 3.1 \\ \hline 100 \end{array}$	$\begin{array}{r} 694.6 \\ + 1.2 \\ \hline 50 \end{array}$	$\frac{93.6}{C}$
B5+50	$\begin{array}{r} 699.8 \\ + 7.1 \\ \hline 170 \end{array}$	$\begin{array}{r} 698.5 \\ + 5.5 \\ \hline 150 \end{array}$	$\begin{array}{r} 696.1 \\ + 3.2 \\ \hline 100 \end{array}$	$\begin{array}{r} 694.5 \\ + 1.2 \\ \hline 50 \end{array}$	$\frac{92.7}{C}$
B6+00	$\begin{array}{r} 699.4 \\ + 5.8 \\ \hline 170 \end{array}$	$\begin{array}{r} 697.6 \\ + 5.4 \\ \hline 150 \end{array}$	$\begin{array}{r} 697.6 \\ + 4.2 \\ \hline 100 \end{array}$	$\begin{array}{r} 695.8 \\ + 2.2 \\ \hline 50 \end{array}$	$\frac{93.6}{C}$
B6+41.6	$\begin{array}{r} 699.0 \\ + 3.4 \\ \hline 170 \end{array}$	$\begin{array}{r} 699.5 \\ + 3.2 \\ \hline 150 \end{array}$	$\begin{array}{r} 699.0 \\ + 3.4 \\ \hline 100 \end{array}$	$\begin{array}{r} 698.1 \\ + 2.5 \\ \hline 50 \end{array}$	$\frac{695.6}{C}$

Right

(10)

$\frac{-03}{212}$ 698E

$\frac{-03}{165}$ 699E

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①

Left

C 0+00	701.1 <u>8.2</u> 703.8	699.9 <u>+7.0</u> 100	695.8 <u>+2.9</u> 50	<u>692.9</u> C	
C 0+50	+8.2 <u>154.0</u> 704.8	702.4 <u>6.3</u> 100	698.8 <u>+3.2</u> 50	<u>95.6</u> C	
C 1+00	+6.2 <u>149.2</u> 704.8	703.7 <u>+5.4</u> 100	701.1 <u>+2.5</u> 50	<u>98.6</u> C	
C 1+50	710.9 <u>+8.6</u> 719.5	705.4 <u>+3.1</u> 708.5	705.0 <u>+2.3</u> 100	703.8 <u>+1.5</u> 50	<u>202.3</u> C
C 2+00	711.3 <u>+6.2</u> 117.0	705.1 <u>+1.1</u> 103.0	705.7 <u>+1.5</u> 100	705.3 <u>+1.2</u> 50	<u>04.6</u> C
C 2+50	713.0 <u>+7.2</u> 9.3	707.0 <u>+1.2</u> 10.2	706.7 <u>+1.0</u> 5.0	<u>05.8</u> C	
C 3+00	713.7 <u>+7.5</u> 82.2	707.5 <u>+1.2</u> 86.2	706.5 <u>+1.0</u> 5.0	<u>06.2</u> C	
C 3+100	713.5 <u>+7.3</u> 78.2	707.1 <u>+1.5</u> 65.5	705.5 <u>+1.0</u> 5.0	<u>06.3</u> C	

Right

(11)

$$\begin{array}{r} 7057 \\ -0.5 \\ \hline 230 \end{array}$$

$$\begin{array}{r} 7039 \\ -2.3 \\ \hline 438 \end{array}$$

$$\begin{array}{r} 703.4 \\ -2.8 \\ \hline 84 \end{array}$$

File No. 15/22

12
C3450

CL 17³²
+ 7.5
770

706²
+ 0.8
703

706⁵
+ 0.2
50

~~706~~
061
C

C4+00

715²
+ 9.8
100

709²
+ 4.8
50

054
C

C4+50

713²
+ 12.5
100

706²
+ 4.6
50

014
C

C5+00

710²
+ 10.9
100

703²
+ 4.1
50

699.8
C

C5+50

708²
+ 9.2
100

702²
+ 3.2
50

99L
C

C6+00

707⁵
+ 8
100

701⁸
+ 2
50

995
C

643²

714⁶
+ 14
150

706⁶
+ 6
100

702¹
+ 15
50

700.6
C

$$\begin{array}{r} 705\cancel{6} \\ - 0\cancel{5} \\ \hline 390 \end{array}$$

$$\begin{array}{r} 702\cancel{6} \\ - 3\cancel{5} \\ \hline 470 \end{array}$$

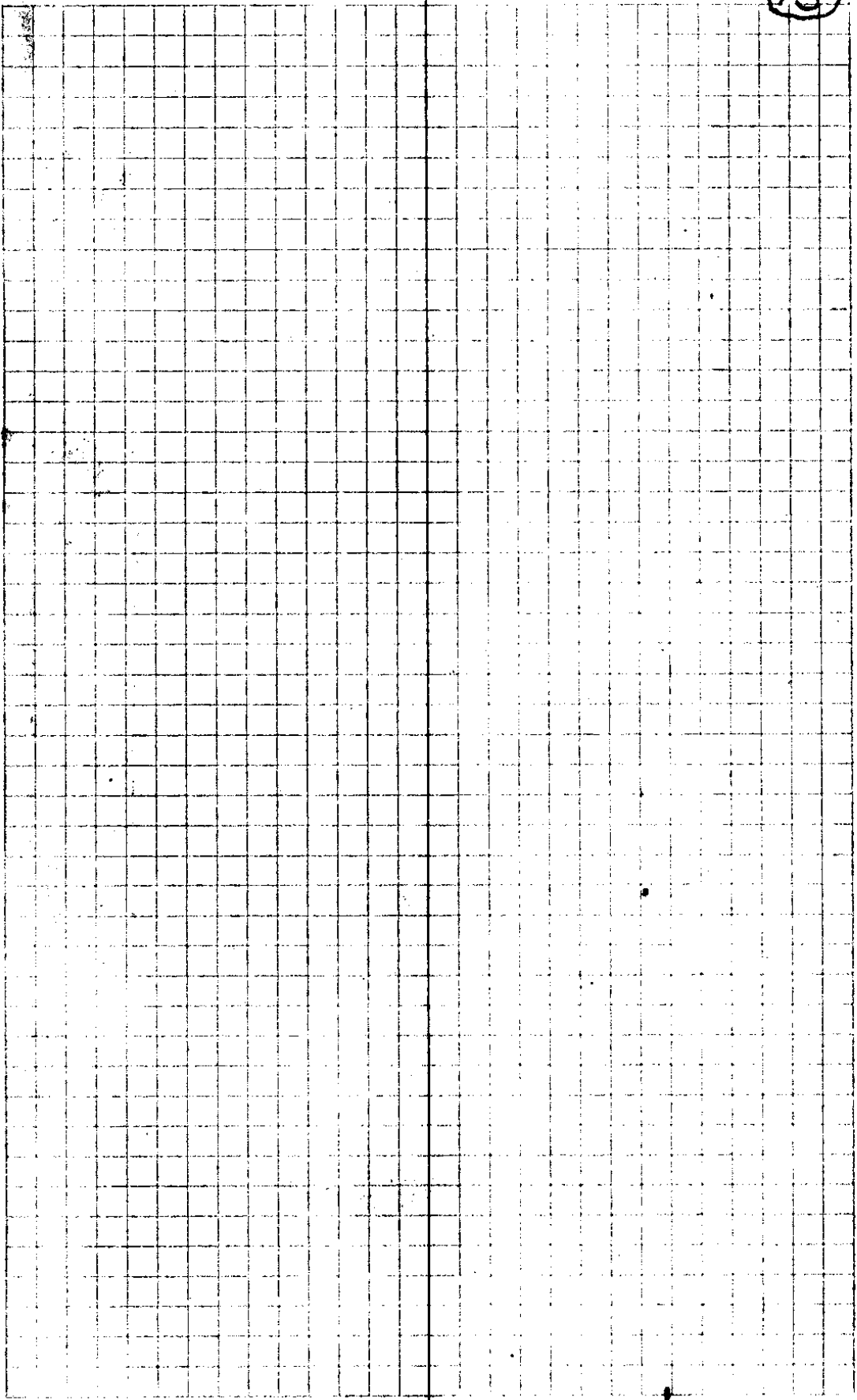
$$\begin{array}{r} 70\cancel{6} \\ - 4\cancel{8} \\ \hline 680 \end{array}$$

43

(12)

U.S. File No. 15/22

13



U. S. File No. 15/22

14

U. S. File No. 15/22

Sta	+	Δ	-	R	E.I.
B.M.	5.854	635 ⁸⁷⁶			630 ⁰²²
○			0.666		635.210 ●
	10.222	645 ⁴³²			
○			1.107		644.325 ●
	8.800	653 ¹²⁵			
○			1.188		651.937 ●
	11.616	663 ⁵⁵³			
○			1.288		662.265 ●
	12.665	674 ⁹³⁰ ✓			
B.M.			3.550	3.550	671.380
○			3.550		
	12.429	683.809			
○			11.099		672.710 ●
	1.020	673.730			
○			8.294		665.436 ●
	6.025	671.461			
○			1.365		670.096 ●
	11.653	681.749			
B.M.				7.324	674.425 ^v ●
○			0.914		680.835 ●
	12.542	693.377			
○			1.404		691.975 ●
	9.563	701.536 ^v			

(15)
N.E. Cor. Myrtle Creek Bridge
State H/W.

Top Concrete Sewer Pipe East Edge

High Point on Tyle S.W. Cor.
School Grounds

C. S. FILE No. 15/22

(16)

Sta

+

∩

-

R

701.536

B.M.

0.380

701.156

B.M.

5.640

695.896

S.W. Cor School Porch

N.W. Cor. Flag Pole on Bottom

Sta	+	$\bar{\Delta}$	-	R.	EI.
A. Line					
B.M.	12 ¹⁹	686.62			
0+00				12 ¹	674.5
+50				9 ¹	677.5
1+00				5 ⁴	681.2
+50				2 ⁰	684.6
			0 ²⁷		686.35
	10 ⁷⁷	697.12			
2+00				10 ⁴	686.7
+50				8 ²	688.9
Tree				5 ⁵	691.6
"				6 ⁷	690.4
"				4 ⁹	692.2
"				1 ⁷	695.4
"				3 ⁶	693.5
"				+1 ⁰	696.1
"				1 ⁷	695.4
"				4 ⁷	692.4
3+00				6 ¹	691.0
+06 ³				5 ⁹⁵	691.17
+50				6 ³	690.8
4+00				8 ⁷	688.4
+50				8 ¹	689.0

S.W. Cot. School Grounds

Sta $\textcircled{10}$ +	π	-	R.	EI.
		<u>727</u>		689.85
$\textcircled{10}$ 622	696.07			
5+00			<u>79</u>	688.2
+50			<u>96</u>	686.5
+90			<u>112</u>	684.9
6+00			<u>104</u>	685.7
+440			<u>77</u>	688.4

B. Line

6+416			<u>+05</u>	695.6
6+00			<u>25</u>	693.6
5+50			<u>34</u>	692.7
5+00			<u>25</u>	693.6
		<u>116</u>		694.91
$\textcircled{10}$ 1026	705.17			
4+50			<u>86</u>	696.6
4+00			<u>51</u>	700.1
3+50			<u>48</u>	700.4
3+00			<u>49</u>	700.3
2+83			<u>54</u>	699.8
2+50			<u>64</u>	698.8
2+00			<u>90</u>	696.2

Sta ⑨ + π - R E.I.

⊙ 4 50 701.09 8 58 696.59

1+50			8 <u>0</u>	693.1
1+00			10 <u>6</u>	690.5
0+50			13 <u>4</u>	687.7
0+00			16 <u>8</u>	684.3

C. Line

0+00			8 <u>2</u>	692.9
+50			5 <u>5</u>	695.6
1+00			2 <u>5</u>	698.6

⊙ 10 70 710.99 0 80 700.29

1+50			8 <u>7</u>	702.3
2+00			6 <u>4</u>	704.6
+50			5 <u>2</u>	705.8
3+00			4 <u>8</u>	706.2
+187			4 <u>8</u>	706.2
+50			4 <u>9</u>	706.1
P. Box			5 <u>17</u>	705.82
Home			4 <u>33</u>	706.66
Plate				
4+00			5 <u>6</u>	705.4

Sta	+	π	-	R	El.
		710.99			
4+50				96	701.4
5+00				112	699.8
			1051		700.48
	792	708.40			
5+50				93	699.1
6+00				89	699.5
+432				78	700.6
			103		707.37
	1104	718.41			
D. Line					
6+45				26	715.8
6+00				09	717.5
5+50				12	717.2
			039		718.02
	947	727.49			
5+00				62	721.3
4+50				34	724.1
4+00				47	722.8
3+724				55	722.0
3+50				55	722.0
			543		722.06
	080	722.86			

Sta (27) +

π

-

R

EI.

70545

Bottom
Step

490

700.55

"

488

700.57

"

592

699.53

417

701.28

⊙ 468

705.96

Floor
Gym.

305

702.91



N.E. }
Center } Facing North
N.W. }

Sta	+ (3)	π	-	R	EI.
4+00					688.4
A Line	11 <u>05</u>	699.45			
0+8 <u>8</u>				10 <u>6</u>	688.85
0+12				9 <u>0</u>	690.5
0+50				5 <u>1</u>	694.4
1+00				0 <u>8</u>	698.6
			0 <u>36</u>		699.09
	6 <u>50</u>	705.59			
1+50				6 <u>3</u>	699.3
1+80				5 <u>6</u>	700.0
2+00				4 <u>9</u>	700.7
2+50				4 <u>5</u>	701.1
3+00				4 <u>4</u>	701.2
			2 <u>80</u>		702.79
	8 <u>28</u>	711.07			
3+50				5 <u>8</u>	705.3

$$\begin{array}{r} 6887 \\ 108 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 6890 \\ 105 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 6934 \\ 61 \\ \hline 62 \end{array}$$

$$\begin{array}{r} 6983 \\ 12 \\ \hline 79 \end{array}$$

$$\begin{array}{r} 6885 \\ 107 \\ \hline 28 \end{array}$$

$$\begin{array}{r} 6895 \\ 100 \\ \hline 27 \end{array}$$

$$\begin{array}{r} 6914 \\ 81 \\ \hline 90 \end{array}$$

$$\begin{array}{r} 6924 \\ 61 \\ \hline 28 \end{array}$$

$$\begin{array}{r} 6958 \\ 31 \\ \hline 95 \end{array}$$

$$\begin{array}{r} 6965 \\ 30 \\ \hline 25 \end{array}$$

(23)

$$\begin{array}{r} 6982 \\ 69 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 6982 \\ 69 \\ \hline 194 \end{array}$$

$$\begin{array}{r} 6971 \\ 17 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 6994 \\ 58 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 6973 \\ 83 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 497002 \\ 49 \\ \hline 216 \end{array}$$

$$\begin{array}{r} 6977 \\ 79 \\ \hline 258 \end{array}$$

$$\begin{array}{r} 497002 \\ 49 \\ \hline 214 \end{array}$$

$$\begin{array}{r} 6972 \\ 79 \\ \hline 268 \end{array}$$

$$\begin{array}{r} 497002 \\ 49 \\ \hline 220 \end{array}$$

$$\begin{array}{r} 6972 \\ 79 \\ \hline 280 \end{array}$$

$$\begin{array}{r} 7075 \\ 46 \\ \hline 44 \end{array}$$

$$\begin{array}{r} 703.3 \\ 78 \\ \hline 52 \end{array}$$

$$\begin{array}{r} 702.7 \\ 84 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 702.0 \\ 91 \\ \hline 262 \end{array}$$

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Sta	+ (24)	π	-	R	El.
		711.07			
4+00				14	709.7
	⊙		035		710.72
	866	719.38			
4+50				4L	7153
	⊙		047		718.91
	839	727.30			
5+096				45	722.80

(24)

$$\begin{array}{r}
 706.9 \\
 \underline{42} \\
 209
 \end{array}$$

$$\begin{array}{r}
 707.8 \\
 \underline{33} \\
 55
 \end{array}$$

$$\begin{array}{r}
 798.8 \\
 \underline{23} \\
 85
 \end{array}$$

$$\begin{array}{r}
 798.0 \\
 \underline{31} \\
 27
 \end{array}$$

$$\begin{array}{r}
 714.2 \\
 \underline{52} \\
 20
 \end{array}$$

$$\begin{array}{r}
 714.2 \\
 \underline{52} \\
 43
 \end{array}$$

$$\begin{array}{r}
 714.9 \\
 \underline{45} \\
 109
 \end{array}$$

$$\begin{array}{r}
 714.3 \\
 \underline{51} \\
 113
 \end{array}$$

$$\begin{array}{r}
 713.9 \\
 \underline{55} \\
 209
 \end{array}$$

$$\begin{array}{r}
 714.5 \\
 \underline{49} \\
 266
 \end{array}$$

$$\begin{array}{r}
 722.3 \\
 \underline{51} \\
 209
 \end{array}$$

$$\begin{array}{r}
 722.2 \\
 \underline{51} \\
 59
 \end{array}$$

$$\begin{array}{r}
 721.8 \\
 \underline{45} \\
 108
 \end{array}$$

$$\begin{array}{r}
 722.2 \\
 \underline{51} \\
 143
 \end{array}$$

$$\begin{array}{r}
 722.9 \\
 \underline{41} \\
 225
 \end{array}$$

$$\begin{array}{r}
 724.6 \\
 \underline{33} \\
 192
 \end{array}$$

B.M.

SW Cor Gas Pump

E End Head wall Culvert

Ground 10.35 491.21

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508.770

0+50			10.50	498.27
+75			10.54	498.23
A prou			11.06	497.71
T.P.	1.96	499.68	11.05	497.72
1+00			2.10	497.68
+25			2.32	497.36
+50			2.58	497.10
+75			3.05	496.63
2+00			3.36	496.32
+25			3.73	495.95
+50			4.10	495.58
+75			4.3	495.38
? T.P.	3.61	499.29	4.00	495.68
3+00			4.25	495.04
+25			4.50	494.79
+50			4.83	494.46
+75			5.04	494.25
4+09 ⁸			5.33	493.96
4+19 ⁵			3.61	495.68
+50			3.83	495.46
+75			3.52	495.77
5+00			3.72	495.57
5+25			3.98	495.31
5+50			4.65	494.64
5+75			4.50	494.70

Gravel 2+75 to end
 Depth West end 1.5' Gravel

Grades from
 0+00 to 0+91.6

Sta	Elev	Grade	C	Other
0+00	498.81	498.71	C	0.1
+11	498.32	498.59	F	.02
+25	498.69	498.44	C	0.25
+30	498.27	498.16	C	0.11
+75	498.23	498.07	C	0.34
+91.6	497.37	497.71		0/0

Elev down
 +7.21

Grade f 4+09.8 to 5+75

Sta	Elev	Grade	C	Other
4+09.8	493.96	493.96		
+19.5	493.68	493.85	C 1.83	1' - 10"
+50	495.46	493.49	C 1.97	1' - 11 5/8"
+75	495.77	493.20	C 2.57	2' - 6 7/8"
5+00	495.57	492.91	C 2.66	2' 8"
5+25	495.31	492.62	C 2.69	2' 8 1/4"
5+50	494.64	492.32	C 2.32	2' - 3 7/8"
5+75	494.79	492.03	C 2.76	2' - 9 1/8"

Sta out stakes on
 + EAST END CULVERT
 A R.L. Elev. Rod B

10.25	501.85			
0+00		6.86	494.99	5.64
0+11		6.48	495.37	5.59
+25		6.51	495.34	5.74
+50		6.76	495.09	6.62
+75		5.83	496.02	7.37

111

Blue Top E. End Culvert

	4.84	495.34	Rod	Grade	490.50
0+75			5.66	490.68	R
+50			5.39	490.95	
+25			5.11	491.23	
0+00			4.84	491.5	

West End

	4.25	492.72	R	L	488.47
4+19 ⁵⁶			4.17	2.51	492.25
+50			3.51	3.39	489.21
+75			4.88	3.10	487.84
5+00			3.62	4.85	489.10
+25			4.09	5.06	488.63
+50			3.06	3.88	489.66
+75			3.23	5.44	489.49

Myrtle Creek Sewer
June 27-1938

U. S. File No.

15/22

Sta Dist ΔL ΔR MC. C.C.

5+35⁶

15°28' N 16¹/₄W N 16°02'W.

3+97¹

5°45'

N 32°W N 31°30'W

1+53¹⁵

0+56

0+00

N 25³/₄W

Myrtle Creek Sewer 2

June 27-1938 N. Richardson T

B. Lane Ch.

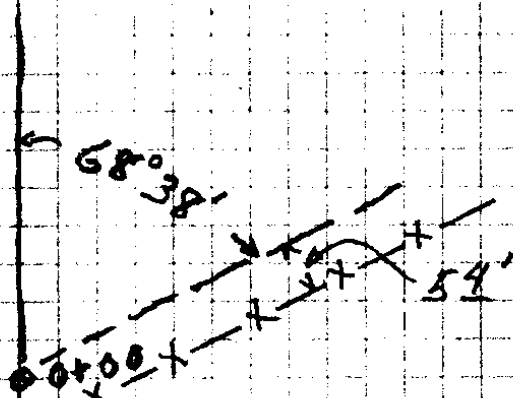
Harvey Eppstein Ch.

G. Dyer Ax.

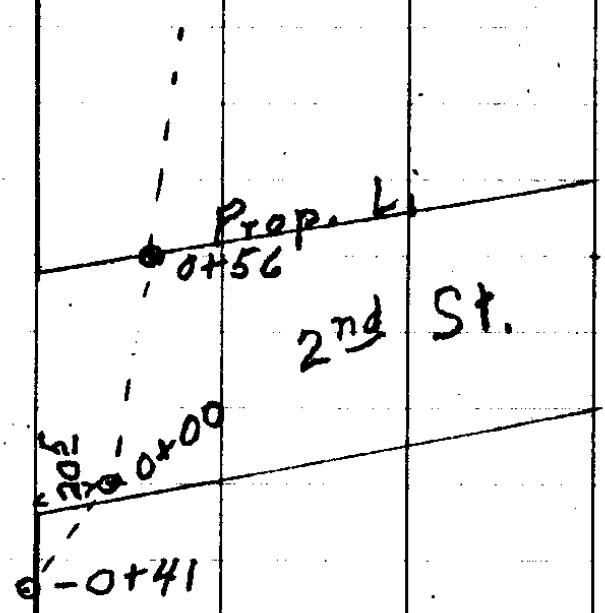
North Side W. Heard St.

Prop. Line 2nd St

Point on North Side of Tile
Catch Basin



C. S. File No. 15/22



4

The page contains a large grid of graph paper. A vertical line runs down the center of the grid, dividing it into two equal halves. The grid is composed of small squares, with the vertical line acting as a central axis.

S. File No. 15/22

Sta	+	π	-	R	EI. 5
B.M.	756	678 ⁹⁴			671.380
- J.P. - 0+41				1156	667.38
Flow - 0+41				1256	666.38
0+00				756	671.38
Flow 0+00				887	670.07
0+56				319	675.75
0+75				176	677.18
			202		676.92
	775	684 ⁶⁷			
1+00				596	678.71
+25				525	679.42
+53 ¹⁵				560	679.07
+75				391	680.76
			203		682.64
	960	692 ²⁴			
2+00				1015	682.09
+25				775	684.49
+50				431	687.93
+75				459	687.65
			033		691.91
	1209	704 ⁰⁰			
3+00				1532	688.68
+25				1433	689.67

Top Tile

10'
offset

6

6 72 672.22

3 52 675.42

2 02 676.92

7 49 677.18

6 85 677.82

4 95 679.72

2 93 682.64

8 10 684.14

3 65 688.59

2 25 689.99

0 33 691.91

10 72 693.28

9 11 694.89

i. s. File No. 15/22

Sta	+	π	-	R.	El.
		704 ⁰⁰			7
3+50				12 ⁴⁰	691.60
+75				10 ⁰⁵	693.95
+97 ^L				7 ⁰⁰	697.00
4+25				3 ²⁹	700.71
			0 ⁶²		703.38
	9 ²⁹	712 ⁶⁷			
4+50				8 ¹³	704.54
+75				6 ⁰⁷	706.60
5+35 ^b				2 ³³	710.34
Flow End Culvert				3 ⁸⁵	708.82
			5.00		
	46 ²⁹				

10' OFF Set

8

6 92 697.08

5 15 698.85

5 70 698.30

0 62 703.38

7 06 705.61

5 40 707.27

1 65 711.02

Q. & File No. 15/22

Levels From SP Station
TO O.S.H.D. BM on North East
Corner of Bridge over
MYRTLE CREEK

JUNE 30-38
HARVEY EPP
BERT LANE

⑪ sta	+	↑	-	Rod	Elev.
U.S.G.S. BM					615.512
●	4.290	619 ⁸⁰²			
			3.265		616.537
●	3.980	620 ⁵¹⁷			
			4.125		616.391
●	11.170	627 ⁵⁶²			
			3.242		624.320
●	10.715	635 ⁰³⁵			
			6.825		628.210
●	1.671	629 ⁸⁸¹			
			9.754		639.635
●	1.561	641 ¹⁹⁶			
			8.968		632.228
●	2.119	634 ³⁴⁷			
			9.206		625.141
●	2.029	627 ¹⁶⁴			
			6.024		621.140
●	5.072	626 ²¹²			
			4.241		621.971
●	8.348	630 ³¹⁹			
			0.297		630 ⁰²²
		O.S.H. BM.			